

Assessing Energy Saving Potential in Existing Buildings in Abu Dhabi through Passive Retrofitting Strategies: Case Study –Office Buildings

تقييم إمكانية توفير الطاقة في المباني القائمة في أبوظبي من خلال استر اتيجيات تحديث المباني: در اسة حالة للمباني التجارية

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ABSTRACT

The UAE as a leading country in the region has set goals to reduce CO2 emissions by 2020 in line with Copenhagen Accord. However, the challenge is considered great since the UAE has been identified as one of the highest ecological footprint in the World in 2007. The future plans in the country invest heavily on sustainability frameworks and future plans such as Abu Dhabi Plan 2030. While the sustainability codes and regulatory frameworks have been recently developed in the country, the regulations are only applicable to minor percentage of the overall building stock. In general the new buildings represent only 0.5% to 2% of the total building stock. Therefore, sustainability guidelines for existing building refurbishment are considered to be critical to reduce the energy consumption in the built environment and associated CO2 emissions.

This research has studied the existing urban development in the Emirate of Abu Dhabi, and identified the commercial buildings as a major contributor to the energy consumption in the capital, with almost one third of the total energy consumption being accounted for commercial uses. An additional 25% for governmental usage has common elements with commercial buildings, yet needs to be further detailed for their sub-categories. The paper has identified two building prototypes as representation of the existing commercial building stock for the periods from 1980-1989 and 1990-1999 and prior to the implementation of the Estidama pearl building rating system for new construction.

Computer modelling was used to assess the savings in electricity consumption, associated cooling loads, energy consumption, and CO2 emissions for the selected 1980s prototype, with an indication of the annual electricity savings for a typical floor layout for a 1990s prototype. The 1980s case study of 17 stories building was modeled in three simulation models; typical floor, roof floor, and ground and mezzanine floors. Building simulations for each of the models were conducted to assess savings due to individual elemental refurbishment and combined scenarios considering upgrades to 1 and 2pearl rating thermal properties. The potential reduction in cooling loads for the overall building varies dramatically depending on the refurbishment application. For the upgrades to 1 pearl rating standard, the savings ranged from 0.21% in the case of roof, to 5.13% and 11.90% in the case of the wall and fenestration upgrades respectively. However, for the upgrades to 2-5 pearls rating requirements, the savings were estimated at 0.22% for the roof upgrades, 5.61% and 14.67 for the wall and fenestration upgrades respectively.

The study indicated that the savings achieved through refurbishment of the roof is negligible compared to that for the replacement of glazing due to the roof area being 6.4% of the building's external envelope while the glazing forms 25.2% of the same. In this context, the glazing upgrades are considered the most efficient

solution. The study also concluded that individual elements of the building, and individual floors could be looked at for prioritized refurbishment strategy depending on the individual savings that could be achieved, easement of implementation, and economic feasibility.

Moreover, the study highlights that combined solutions achieve greater savings than when individual refurbishment applications are considered. The savings for the overall building are considered significant estimated at 18.90% and 22.12% for the 1 pearl and 2 pearls upgrades respectively.

Solar gain and external conduction gain analysis indicated that the elements behavior and specifically the external conduction gain profile varies for the various applications. As an example, the 2 pearl combined scenario has 0.0727 MWh less annual conduction gain than the sum of the individual scenarios.

The economic feasibility study indicated that the most feasible refurbishment solution for the building prototype of 1980s is for 2 pearls glazing upgrade, where 9 years payback period could achieve savings of 164.2157 MWhe of annual electricity consumption. However, it was noted that the highest savings for the combined solution in the case of 2 pearls upgrades would return its capital cost in around 16 years. The simple payback period calculations excludes the savings in government electricity cost subsidies, evaluation of building envelop performance upgrades such as humidity resistance, air tightness, aesthetical appearance, as well as future increases in the cost of electricity. It is expected that once all the benefits are quantified, the Simple Payback Period (SPP) analysis will result in reasonable timeframe for the owners to recoup their initial investment cost.

Finally, the research is concluded by extrapolating the annual reduction in electricity consumption to represent the savings across Abu Dhabi. For the 1980s, the implementation of a combined retrofitting scenario to 2 pearls rating requirements; is estimated to achieve annual reduction in electricity consumption of 18,433 MWeh/yr. Whereas, the refurbishment of the most economically feasible solution to upgrade the building glazing to 2 pearl rating standards, can achieve an overall reduction of 12,214 MWeh/yr. CO2 emissions reduction for the combined solution of 2 pearls rating is estimated at 9,530,968 KgCO2/yr.

Moreover, an indication of the typical building prototype upgrade for the period from 1990-1999 has indicated that the overall savings for Abu Dhabi for the 1990s buildings, when the glazing elements are upgraded, are 28,599 MWeH/yr and 20,152.MWeh/yr for the 2 pearls and 1 pearl rating respectively.

الملخص التنفيذى

لقد وضعت دولة الإمارات العربية المتحدة كدولة رائدة في المنطقة أهداف للحد من انبعاثات غاز ثاني أكسيد الكربون بحلول عام 2020 تماشيا مع اتفاق كوبنهاغن . ومع ذلك ، يعتبر هذا تحديا كبيرا حيث أن دولة الإمارات العربية المتحدة واحدة من أعلى دول العالم في البصمة البيئية في في عام 2007. الخطط المستقبلية في البلاد تستثمر بشكل كبير على الأطر الاستدامة و الخطط المستقبلية مثل خطة أبوظبي عام 2030. في حين أن رموز الاستدامة و الأطر التنظيمية قد وضعت مؤخرا في البلاد ، إلا أن اللوائح تنطبق على نسبة ضئيلة من الأسهم بناء الكلية فقط. بشكل عام تمثل المباني الجديدة 7.5% إلى 2 % من إجمالي الأسهم بناء . وبالتالي، تعتبر المبادئ التوجيهية تحت نظام الاستدامة والتي تنظبق فقط على المباني الجديدة 0.5% إلى 2 % من إجمالي الأسهم بناء . وبالتالي، تعتبر المبادئ التوجيهية تحت نظام الاستدامة والتي تنطبق المرتبطة بها.

وقد بحثت هذه الدراسة التنمية الحضرية الموجودة في إمارة أبوظبي ، و حددت المباني التجارية باعتبار ها مساهما رئيسيا في استهلاك الطاقة في العاصمة ، مع ما يقرب من ثلث الاستهلاك الكلي للطاقة التي تمثل الاستخدامات التجارية . بالإضافة إلى 25 ٪ إضافية للاستخدام الحكومية لديها عناصر مشتركة مع المباني التجارية ، ولكن يجب أن يكون أكثر تفصيلا للفئات الفرعية. وقد حددت الورقة نموذجين للمباني التجارية القائمة للفترتين من 1980-1989 و 1990-1999 و قبل تنفيذ نظام تصنيف المباني استدامة اللؤلؤ للبناء الجديد .

تم استخدام النمذجة الحاسوبية لتقييم التوفير في استهلاك الكهرباء و الأحمال التبريد المرتبطة بها، استهلاك الطاقة ، وانبعاثات غاز ثاني أكسيد الكربون في s1980 النموذج المحدد، مع الإشارة إلى توفير الكهرباء السنوي لنموذج s1990 . نموذج s1980 يتمثل في 17 طابق تم تمثيله على ثلاثة نماذج المحاكاة ؛ متكرر ، طابق السطح ، و الطوابق الأرضية و الميزانين . أجريت المحاكاة بناء لكل من نماذج لتقييم وتوفير بسبب تجديد عنصري الفردية والسيناريوهات مجتمعة النظر في ترقيات ل 1 و تصنيف pearl2 الخواص الحرارية . الانخفاض المحتمل في الأحمال التبريد لمبنى الكلية يختلف بشكل كبير عن تطبيق التجديد. للترقيات إلى 1 لؤلؤة تحت معيار التصنيف، تراوحت الوفورات من 0.21 % في حالة السقف ، إلى 5.13 % و 11.00 % في حالة الجدار و النوفاذ على التوالي. ومع ذلك ، للترقيات ل 2-5 لؤلؤة بحسب متطلبات تصنيف اللؤلؤ ، قدرت الوفورات عند 0.22 % لل ترقيات سقف ، 5.61 % و 14.00 للجدار و النوالي.

وأشارت الدراسة إلى أن الوفورات التي تحققت من خلال تجديد السقف لا يكاد يذكر مقارنة بما كان عليه لاستبدال الزجاج نظرا لكون المساحة الطابقية للسقف 6.4 ٪ من الغلاف الخارجي للمبنى في حين أن الزجاج يشكل 25.2٪ من مساحة الغلاف الخارجي للمبنى. وفي هذا السياق، يعتبر تجديد الزجاج الحل الأكثر كفاءة. وخلصت الدراسة أيضا إلى أن العناصر الفردية للمبنى، و الطوابق الفردية يمكن النظر في استراتيجية لإعطاء الأولوية في التجديد اعتمادا على المدخرات الفردية التي يمكن تحقيقها ، تكاليف التنفيذ، و الجدوى الاقتصادية . علاوة على ذلك، تسلط الدراسة الضوء على أن الحلول مجتمعة تحقق وفورات أكبر مما كانت عليه عندما يتم النظر في التحديد علاوة على ذلك، تسلط الدراسة الضوء على أن الحلول مجتمعة تحقق وفورات أكبر مما كانت عليه عندما يتم النظر في التطبيقات الفردية للتجديد . تعتبر مقدار الوفورات للبناء الكلي كبيرة تقدر بنحو 18.90 ٪ و 22.21 ٪ لؤلؤة 1 و 2 لؤلؤة على التوالي. وأشارت الدراسة التحليلية لمقدار الطاقة الشمسية المكتسبة و الطاقة الخارجية المكتسبة عن طريق العلاف الخارجي للمبنى, أن سلوك وأشارت الدراسة الحارجية المماسية المنورية التي يمكن تحقيق وفورات أكبر مما كانت عليه عندما يتم النظر في التطبيقات الفردية للتجديد وأشارت الدراسة التحليلية لمقدار الطاقة الشمسية المكتسبة و الطاقة الخارجية المكتسبة عن طريق الغلاف الخارجي للمبنى وأشارت الدراسة الماقة الخارجية المكتسبة عن طريق التوصيل الحراري يختلف عن حالة المبنى عندما يتم تجديده بالتطبيقات المختلفة في آن واحد. كمثال ، فإن المكاسب السنوية لسيناريو التجديد لمعايير 2 لؤلؤة لكل العناصر تقدر ب 0.0027 ميجاوات أقل من مجموع السيناريوهات

وأشارت دراسة الجدوى الاقتصادية أن الحل الأكثر جدوى لتجديد النموذج بناء s1980 هو لمعايير 2 اللؤلؤ لتجديد الزجاج الخارجي، حيث أن الفترة المقدرة ب 9 سنوات كفترة الاسترداد يمكن أن تحقق وفورات بمقدار MWhe 164.2157 من استهلاك الكهرباء السنوية. ومع ذلك ،

الفر دية.

لوحظ أن أعلى الادخار لسيناريو التجديد لكافة العناصر مجتمعة بحسب معابير 2 لؤلؤة سيعود بتكلفة رأس المال في نحو 16 عاما. ومن المهم التنويه إلى أن حسابات فترة الاسترداد بسيطة تستبعد الوفورات في تكلفة الكهرباء الناتجة عن الدعم الحكومية ، وتقبيم الأداء من حيث الاستفادة المتعددة الأخرى للتجديد مثل مقاومة الرطوبة ، وتقليل تسرب الهواء ، والمظهر الجمالي ، فضلا عن الزيادات المستقبلية في تكاليف الكهرباء. ومن المتوقع أنه إذا ما تم تقييم كافة الاستفادات، فإن فترة الاسترداد ستحقق في إطار زمني معقول لأصحاب المباني لاستقرداد التكلفة الاستثمارية. الأولية.

وأخيرا، خلص البحث عن طريق استقراء الحد السنوي في استهلاك الكهرباء لتمثيل الوفورات في أبوظبي . ل s1980، و تنفيذ سيناريو التجديد لكافة العناصر مجتمعة بحسب معايير 2 لؤلؤة تحت متطلبات تصنيف نظام الاستدامة ؛ ويقدر بتحقيق خفض سنوي في استهلاك الكهرباء بنحو MWeh 18433 / سنة . في حين، تجديد الحل الأكثر جدوى اقتصاديا لرفع مستوى الزجاج بناء على معايير تصنيف اللؤلؤ 2 ، يمكنه تحقيق خفض إجمالي بنحو 214،MWeh اسنة . ويقدر الحد من انبعاثات غاز ثاني أكسيد الكربون في حال تجديد جميع العناصر بحسب معايير 2 لؤلؤةمن تصنيف اللؤلؤ بنحو 30 KgCO2/yr

و علاوة على ذلك ، قدمت الدراسة مؤشرا على تجديد بناء النموذج الممثل للفترة من 1990-1999 للوفورات الكلية للمباني في أبوظبي إن الوفورات في مباني 1990s، عندما تتم تجديد العناصر الزجاج ، هي MWeH 28599 / سنة و MWeh. 20،152 / سنة ل اللؤلؤ 2 و تقييم اللؤلؤ على التوالي.

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CHAPTER 1: INTRODUCTION

1 INTRODUCTION

1.1 OVERVIEW

Climatic change has been globally recognized as a serious challenge. International agreements, conferences, and protocols have aimed to set mitigation measures to reduce CO2 emissions. In 2010, in a correspondence for the United Nations Framework Convention on Climatic Change, the UAE has announced their decision to being associated with the Copenhagen Accord (MoFA 2010). The accord targets reduction in CO2 emissions by 2020. However, the mitigation measures vary depending on the local sources of CO2 emissions within each of the participating countries. The source of energy and the rates in energy consumption directly related to the CO2 emissions released into the atmosphere.

Energy consumption in the built environment represents a great percentage of the total energy consumed in different sectors. The built environment is responsible for approximately 40% of primary energy consumption (Petersdorff et al 2010). It is also one of the major contributors to the greenhouse gases (GHG) emission, and heat island effect. Opportunities to conserve energy in buildings are very broad and can contribute to achieving highly efficient buildings.

In the UAE, the building construction sector has been an active and fast growing business for the past two decades. According to The UAE National Media Council (2010) the construction sector represented the second highest gross domestic product (GDP) growth in 2008. This continuous growth of the construction industry in the UAE has led to raised concerns of its impacts on the environment. The recognition of the sustainable development approach is relatively new in the Gulf region including the UAE. In this context, sustainable development is defined as "Development that provides people with a better life without sacrificing or depleting resources or causing environmental impacts that will undercut the ability of future generations to meet their needs." (Richard & Dorothy 2011, p. 655).

The new trend in sustainable construction is a natural response to mitigate the environmental impacts of the building construction industry, especially since the UAE has been identified as the country with the highest ecological footprint per person worldwide on 2007 (WWF 2010). The ecological footprint is defined as "A concept for measuring the demand placed on Earth's resources by individuals from different parts of the World, involving calculations of the natural area required to satisfy human needs." (Richard & Dorothy 2011, p. 639).

In the UAE, the governmental agencies are playing a great role to mitigate the situation through building regulations that aim in reducing the environmental impact of the built environment. The UAE's commitment to reduce CO2 emissions in the near future are reflected in the sustainability frameworks in 2020 and 2030. A recent announcement in November 2013 has been to announce the first commercial Carbon capture and storage project in the UAE. The project is led by Masdar and ADNOC, and aims to reduce the CO2 emissions related to oil industry (The National 2013). All efforts with no doubts are targeting the achievement of a sustainable living in the future. In light of such efforts, and efforts to reduce energy consumption within the built environment, it has to be noted that even if the regulatory frameworks aims at developing a net-zero CO2 emissions for the new buildings, there will remain an excessive building stock with high energy consumption hence high Carbon emissions. Although the new sustainability standards and regulations targets new buildings, the existing building stock adds up only to a total of 0.5 to 2% of the total construction. Peacock et al (2008) & Langston et al (2008). Therefore, the building stock prior to implementation of sustainability and energy efficient building standards, remain a major contributor to the CO2 emissions. The only solution to mitigate this situation is by implementing building refurbishment strategies to energy consumption and associated CO2 emissions.

Many researches have been conducted on this regard, and shared knowledge on building refurbishment supports the idea that low-cost refurbishment applications can greatly benefit the existing structure, reduce CO2 emissions, and reduce reliance on renewable energy to offset the CO2 emissions released.

1.2 BUILDING REFURBISHMENT

Energy saving strategies include both active and passive techniques, and are applicable to both new designs and existing buildings. There are many aspects that were previously investigated under this subject; they include mechanical systems, thermal comfort, GHG emissions, economic feasibility, users' behavior, social aspects, standards and regulations. The list of parameters and related topics in which energy saving strategies could be approached seem endless, and are interlinked.

Many researches were conducted to investigate the strategies in which energy savings in buildings could be achieved. Refurbishment of existing building stock is envisaged as a mean of reducing CO2 emissions in the short to medium term, which makes it a preferable option compared to pure reliance on green energy sources. Sunikka & Boon (2003). According to Lockwood (Lockwood 2009, p. 48), the US Green Building Council has identified green retrofitting as "any kind of upgrade at an existing building that is wholly or partially occupied to improve energy and environmental performance, reduce water use, and improve the comfort and quality of

the space in terms of natural light, air quality, and noise—all done in a way that it is financially beneficial to the owner. Then, the building and its equipment must be maintained to sustain these improvements over time."

With the main target of reduction in energy consumption in existing buildings, the refurbishment process is applicable to most of the existing building typologies and uses including residential, commercial, governmental, healthcare, education, etc. he outcome from the refurbishment process, specifically those targeting energy savings, are of great importance for future governmental planning of construction of new power plants, management of existing and future energy demand, reduction of CO2 emissions, and reduction of peak loads across the country. The savings also impact the planning for future infrastructure utilities, and public services. There are many refurbishment strategies that could be implemented in existing buildings. However, the applicability, feasibility, and outcome of each strategy can vary dramatically. Prior to making decisions on which refurbishment strategy is to be implemented, a pre-assessment study helps identifying the feasibility and expected outcome of the technique. For example, in an office building, an improved Heating, Ventilation, and Air Conditioning (HVAC) system can achieve great savings in energy consumption but will be a costly application. Whereas, looking at improvements through passive techniques might achieve less saving in energy consumption but will be much more feasible.

Refurbishment for office buildings has been envisaged as the next big thing by Lockwood (2009). It has also been preferred over a complete redevelopment of an office building from an economic feasibility perspective as highlighted by Addy and McCallum (2012). Another research conducted by Anderson and Mills (2002) highlighted that refurbishment of existing office buildings has a reduced environmental impact over the building's redevelopment. The study indicated that the building redevelopment has increased impact over refurbishment of an air conditioned office building by 13-14%, and 20% for naturally ventilated offices. The environmental impact estimated includes 40-50% embodied energy.

However, there are constrains that usually are considered as limitations for any refurbishment process for an office building. Rhoads (2010) has identified the unavailability of capital cost and lack of incentives as the financial related limitations to the refurbishment process. Moreover, the limitations in technologies and its implementation process applicable to building refurbishment could contribute to the restrictions of application. Another aspect related to enforcement of policies and regulatory frameworks for building refurbishment.

1.3 THE IMPACT OF PASSIVE REFURBISHEMENT

Passive design has been an integrated design approach for decades. The passive design is a regionally responsive design that responds to the climatic conditions by minimizing heat gain, heat loss, maximizing natural ventilation benefits, and natural daylight. Similar to the approach in the new buildings, passive refurbishment techniques follow the same concept for existing buildings. Passive refurbishment strategies include upgrades in thermal performance of building envelope, minimizing thermal bridging impact, maximizing benefits from shading devices, optimizing natural daylight, etc. Whereas active refurbishment strategies targets upgrades in mechanical building systems, such as upgrades in HVAC system which seems to be one of the most common active retrofitting techniques. Others include integration of Building Management Systems (BMS).

Passive refurbishment strategies aim at increasing building performance with no or minimal use of energy after installation, whereas active strategies are usually requires or produces energy. The cost associated with any of the refurbishment strategies shall be carefully selected. Prior to making decisions on which refurbishment approach is feasible, it is important to analyze the existing conditions of the building to be retrofitted. Based on the current conditions, the building can be categorized into any of the four levels of refurbishment as identified by BRE (2002) based on their actual conditions at the time of assessment. The four levels of refurbishment are categorized based on levels of interventions required, as following;

- Level 1: requires minimal intervention such as addition of internal blinds, repainting of the building interior, replacement of low-energy IT solutions
- Level 2: is an intermediate level of refurbishment beyond what is identified in the previous level. This
 level is expected to incorporate lighting and systems control integration or replacement
- Level 3: represent major refurbishment applications such as raising floors, external walls, addition of external solar applications, etc.
- Level 4: is when the building requires demolition or redevelopment due to very poor conditions.

For passive refurbishment strategies, the applications might range between any of the three intervention levels. However, the reduction of environmental impact of the building is considerable. For example, upgrading thermal insulation of the building envelope can reduce cooling loads by 26% as highlighted by a study conducted by Hiroshi et al (2006) in Shanghai. Another study on office buildings in Malaysia, has indicated that

a strategy as simple as increasing the air conditioning temperature set point is a costless strategy that can achieve up to 24% savings if the set point in increased by 4° C compared to the base case of 22° C (Saidur 2009). Another study in the UAE highlighted that upgrades in thermal performance of building envelope and glazing in residential villas can achieve up to 37.2% reduction in cooling loads. (AlNaqabi *et* al 2012).

1.4 SUSTAINABLITY STANDARDS FOR EXISTING BUILDINGS

Countries around the World have already established sustainability rating systems that aim to reduce the environmental impact of the buildings. Such rating systems like Leadership in Energy and Environmental Design (LEED), Building Research Establishment Environmental Assessment Method (BREEAM), and Green Star are used as tools to assess the sustainability aspects of the building during the design and construction stages. However, recently emphasis has been to minimize environmental impact of existing buildings during operation stages. For example, LEED Existing Buildings +n Operation and Maintenance (LEED EB+OM) sustainability rating system has been introduced by the US Green Building Council as a rating system that addresses the operation and maintenance of the existing buildings. LEED stands for Leadership in Energy and Environmental Design, the rating systems established by USGBC set measures to design, construct, and operate a sustainable development both on building scale and urban development scale (USGBC 2013).

The UAE as a young country, however, has only introduced green building regulations recently. The Emirate of Abu Dhabi introduced the Estidama Pearl Rating System; which is a green building rating system; and enforced mandatory requirements on all new buildings since 2010. Estidama provides three sustainability tools targeting the villas, building, and large developments. The Pearl systems corresponding to these three tools are Pearl Villa Rating system, Pearl Building Rating System, and Pearl Community Rating System. The Pearl Building System is used for several building uses i.e. offices, multi-residential, retail, school, and mixed use buildings. The Pearl Rating System is used to rate the developments from 1 to 5 pearls, where 1 pearl rating is mandatory for all developments, and 2 pearls are mandatory for all governmental buildings. This research will use the Pearl rating system standards.

Although the green building regulations were made mandatory, such regulations target new buildings only, whereas the larger stock is represented in the existing buildings. The lack of policies and sustainability standards for existing buildings in the UAE, and the limited research addressing energy savings through building refurbishment, have triggered this research.

1.5 AIMS AND OBJECTIVES

The study primarily focus on identifying existing building typologies of commercial buildings in Abu Dhabi, which represent the development in construction methods, material use, architectural style which influence the behavior of the building in terms of energy consumption and thermal performance parameters.

The building prototype shall be assessed against several retrofitting scenarios to investigate an effective yet economically feasible strategy to upgrade the existing building stock to reduce energy consumption. The research investigates the upgrades in thermal performance of building envelope.

AIM

The purpose of the study is to explore the potential of energy savings by retrofitting existing buildings in Abu Dhabi Metropolitan through passive design techniques with main focus on commercial buildings.

OBJECTIVES

The objectives identified for the study include the following:

- To assess the energy consumption in the existing commercial buildings in Abu Dhabi
- To identify sample building typologies corresponding to the evolution of construction practices and building regulations in 1980s & 1990s
- To understand the chronological development in building construction and its relation to energy consumption and CO2 emissions
- To explore the impact of retrofitting existing buildings through passive techniques on energy savings and CO2 emissions reduction. The passive techniques include;
 - Upgrade of thermal insulation for the external walls, for two different wall sections U-value
 - Upgrade of the thermal insulation for the roof, for two different roof sections U-value
 - Replacement of the glazing materials, for two different glazing solar heat gain coefficient and Uvalue
 - Combined Solutions

- To assess the feasibility and economic viability of the retrofitting process through simple payback applications
- To assess the refurbishment impact on the total existing building stock represented by the studied typology. This aims to allow for policy makers to understand the estimated energy savings on a large scale.

1.6 RESEARCH OUTLINE

This research is presented in six main chapters, supported by 5 appendices. The following is a brief description of the content for each of the chapters.

The first chapter:

This chapter is an introductory chapter that provides an overview of the major topics addressed in the research in general terms. The chapter is concluded by listing the research aims and objectives.as well as outlining the research paper.

The second chapter:

The literature review provides detailed study of the previous researches conducted to assess potential of energy savings in existing buildings through buildings refurbishment. The chapter also identifies the energy consumption pattern in the UAE, then identifies the major sectors within the built environment which highly contributes to the energy consumption in the country. The chapter then reviews the existing building stock in Abu Dhabi, and analyze the construction development to identify representative prototypes for commercial buildings in the 1980s and 1990s.

The third chapter:

This chapter identifies the various research methods related to this topic, and compares the method to identify the most relevant research method within the context of this study. The chapter then presents the preferred research methodology and discusses the relevant tools. The chapter also presents a comparison between building simulation tools, and provides a validation of the selected tool. A summary of the research methodology for this study is then concluded. The fourth chapter:

The fourth chapter presents the case study, the simulation data input, and the simulation method. The chapter also provides an identification of the user validation for the case study, The simulation scenarios are also presented in details.

The fifth chapter:

This chapter presents the results concluded from the research and provides a critical discussion of the results. The chapter highlights the results for cooling loads energy, and CO2 emissions of the studied models. It also highlights the solar gain and external conduction gains associated with each of the scenarios. The chapter then presents an economic feasibility study of the refurbishment solutions, and then is concluded by magnifying the result on a larger scale to represent the saving in Abu Dhabi.

The sixth chapter:

This chapter is considered the final chapter within the research, which presents the conclusion of this study and recommendations for future studies.

CHAPTER 2: LITERATURE REVIEW

2 LITERATURE REVIEW

2.1 OVERVIEW

Energy consumption in the built environment represents a great percentage of the total energy consumed in different sectors. The built environment is responsible for approximately 40% of primary energy consumption (Petersdorff *et* al 2010). It is also one of the major contributors to the greenhouse gases (GHG) emission, and heat island effect. Opportunities to conserve energy in buildings are very broad and can contribute to achieving highly efficient buildings.

Many researches were conducted to investigate the strategies in which energy savings in buildings could be achieved. Energy saving strategies include both active and passive techniques, and are applicable to both new designs and existing buildings. There are many aspects that were previously investigated under this subject; they include mechanical systems, thermal comfort, GHG emissions, economic feasibility, users' behavior, social aspects, standards and regulations. The list of parameters and related topics in which energy saving strategies could be approached seem endless, and are interlinked.

This chapter presents the literature review and collected data which leads to the identification of the existing gap and highlights the opportunities for investigations in this field. First, the chapter discusses previous researches conducted to estimate energy savings through various refurbishment strategies with focus on passive techniques over active strategies. Then, the chapter presents the current status in the UAE and primarily in Abu Dhabi to identify the existing building stock, building typologies, and construction methods. The chapter is concluded by identification of the problem statement and setting the aims and objectives of this research in light of the collected data.

The following section highlights the outcome of previous studies conducted in this field to investigate potential energy savings through building refurbishment techniques. The studies cover different climatic conditions, different building typologies, and both direct and passive retrofitting techniques.

2.2 ASSESSMENT OF REFURBISHMENT STRATEGIES THROUGH PREVIOUS STUDIES

There are many refurbishment strategies that could be implemented in existing buildings. However, the applicability, feasibility, and outcome of each strategy can vary dramatically. Prior to making decisions on which refurbishment strategy is to be implemented, a pre-assessment study helps identifying the feasibility and expected outcome of the technique. For example, in an office building, an improved Heating, Ventilation, and Air Conditioning (HVAC) system can achieve great savings in energy consumption but will be a costly application. Whereas, looking at improvements through passive techniques might achieve less saving in energy consumption but will be much more feasible.

Following is a summary of selected previous studies conducted to assess potential of energy savings in existing buildings. The studies cover building typologies ranging from low-rise residential buildings to office buildings and high rise commercial buildings. The selected studies mainly focus on cooling strategies; however few addressed the implications during heating days. The literature review below categorizes the reviewed studies according to the refurbishment systems investigated being passive techniques or active techniques.

2.2.1 PASSIVE STRATEGIES

Passive design strategies can be used to reduce energy consumption not only during the early design stages, but also can be employed to achieve energy savings in existing buildings. Techniques such as upgrading building glazing, thermal performance for walls and roof, using shading devises, using various window typologies, the use of natural ventilation, and many other strategies have been tested by researchers for various building typologies, and different climatic conditions.

A study conducted by Gugliermetti & Bisegna (2007) investigated the potential energy savings in residential buildings and small office buildings in five different cities in Italy, representing the Mediterranean climate, due to the integration of reversible windows. The study highlighted that previous studies undertaken on the same topic did not take into consideration the occupants' thermal comfort and the cooling loads in summer. Another aspect of the study is considering overheating effects in winter due to heat gains through the reversed window system. Previous studies were conducted for different building properties in relation to winter overheating, but those did not explore the reversed window system specifically.

The reversed window system suggested in the study has one clear pane, and another reflective one, and the system allows the window to be closed on both ways. The study investigated the impact of thermal properties and the reflectance of different glazing materials and systems. In order to estimate the energy savings using the reversed window system, the paper defines several scenarios of heating, cooling, and glare control strategies in which occupants contribute to the control system such as openings. The strategies include natural ventilation, shading devices (external shutters and internal curtains), forced ventilation, and mechanical HVAC systems.

The results of this study have highlighted that reversible windows system can contribute to energy savings in the residential buildings and small offices located in Mediterranean climatic conditions. The reflective pane is always facing the warmer environment, in other words the reflective coat is external in summer, and internal in winter. The potential for energy savings depend on the techniques used to mitigate the overheating that occurs in winter. While energy savings are less in buildings located in colder winters due to use of natural ventilation to overcome winter overheating problem, the mechanical ventilation reduces the savings in warmer winters. Also, it has been indicated that both the reversed window system utilized for both east and west facades increases the energy saving by 10%-15% compared to the south facing windows.

Another study was conducted on a case study of a conventional design of a residential building in Spain where the study investigated energy savings through passive strategies. Ruiz & Romero (2011) recommended several passive strategies for both reducing heating and cooling levels. Energy savings of a combined solution has been estimated to be 13% of the original building design.

The paper has analyzed the context of the building and listed its characteristics and features. Then simulated two groups of passive strategies, the first group included the heating strategies running one simulation for each strategy same has been performed for the cooling strategy.

All results were compared to the basic model which reflects the conventional design

Final model has been recommended using the most appropriate at all strategies, those were changing building orientations to south, increasing glazing area to 20% at both the north and south facades

Adding a 35 cm framings to the windows and adding a 2 cm XPS CO2 expendable polystyrene insulation to the external walls. The cost analysis has indicated that minimal costs are added to the conventional design to achieve the energy savings of 13%.

On a different level, a study was conducted to assess the potential of energy savings on a large development scale, under an initiative by the US Environmental Protection Agency (EPA), which was launched to measure the contribution of the heat island reduction (HIR) techniques. This initiative led to the conduction of a pioneer project named the Urban Heat Island Pilot Project (UHIPP) taking into consideration five cities within the United States. The project realized the urbanization's great role in the increase of carbon emissions and the heat island effect. This study, conducted by Akbari & Konopacki (2005), is perceived as a continuation of the previous studies, and expanding the HIR strategies assessment to include all the states.

The study identified building prototypes for residential, office, and retail buildings both for the pre 1980s buildings, and post 1980s taking into consideration both electricity and gas systems. The study assessed energy saving potential through considering three sets of strategies;

- Direct HIR strategies, i.e. reflective roofs, and trees for shading;
- Indirect HIR strategy which consider the urban setting in terms of the use of reflective materials in paving and buildings, as well as increase in vegetated surfaces; and
- A scenario considering a combination of indirect and direct HIR strategies
 Energy savings were presented in relation to the heating-degree-days, and cooling-degree-days (HDD, and CDD).

The results of the study have indicated that the direct HIR strategies contribute to more than three quarters of the energy savings for all buildings. They also indicate that the highest potential for energy savings in a gasheated building is in residential typology with a maximum of 25% savings for pre 1980s, and 20% for post 1980s. The highest savings in peak electricity demand is in the office buildings typology which is estimated to be a maximum of 1.0 kW/1000 sq.ft for pre-1980s buildings, whereas both the residential and office buildings has a maximum savings of 0.4 kW/1000 sq.ft for post-1980s buildings.

2.2.2 COMBINED PASSIVE AND ACTIVE STRATEGIES

Another research addressed an office building typology, with focus on passive strategies to achieve reduction in energy consumption. In Malaysia, Saidur (2009) conducted a study to assess the potential of energy savings in office buildings by calculating energy intensity, global warming gas emissions, and economic viability of the

suggested energy saving strategies. The strategies include: upgrading building insulation, improved glazing system, use of compact fluorescent lamps (CFL), adjusting the temperature set point for the air conditioning system to a higher temperature, as well as savings by higher efficiency electric motors. It has to be noted here that energy savings and emissions have been calculated for high-efficiency motors (HEM), and the variable speed drives (VSD) at different operational loads. The economic viability has also been estimated through calculating the expected payback periods of the strategies. The study used extensive database provided by the Malaysian Energy Center (PTM) collected through energy auditing for 68 office buildings.

As part of the study, the results have been compared to other countries where several researchers have conducted similar studies. This is perceived not only as comparison of the energy consumption and emissions, but also it is a validation to the research methodology conducted since the results were similar to those from Thailand which has similar climatic characteristics.

The results of the study have indicated that air conditioning is the highest energy consumer among building appliances and equipment, followed by lighting system, lifts and pumps, and others which are represented by the following percentages respectively: 59%, 19%, 18%, and 6%. Also, it has been indicated that both the CFL fixtures, and upgrading building insulation are cost effective measures with an estimated payback period of less than 33% of the product life span. A strategy such as increasing the air conditioning temperature set point is a costless strategy that can achieve up to 24% savings if the set point in increased by 4° C compared to the base case of 22° C. Moreover, the study concluded that the utilization of the HEM and VSD are considered economically viable.

Another study conducted on an auditorium building typology highlighted the potential of reducing cooling loads up to 70% of the building's original status. The study, conducted by Flores *et* al (2008), investigated the integration of passive design strategies to achieve a better thermal performance hence reduction in energy consumption with minimal addition to the conventional building costs. It was conducted on an existing auditorium building in Santa Rosa, Argentina. Based on this study, an improved design of the same building is to be constructed in a different location in Argentina. The new design is to consider several passive solar strategies for energy savings while maintaining minimal additional costs. A comparison between the original design and the modified one is conducted. In order to validate the results on the ground, field measurements were taken. A study was conducted on the first project - an auditorium building in Santa Rosa- in winter to understand the thermal behavior of the building. The building heating and cooling strategies included building insulation, double glazed openings, heating system with controls for heating degree-days, natural ventilation, glazing areas, and thermal capacity for cooling season. The researchers measured the outdoor climatic conditions, and the dry bulb temperature inside the building through field measurements.

The assessment on the first model was based on building parameters and data including; outdoor temperature, solar irradiance on horizontal surface, building parameters and properties, site, building materials, and building orientation. The results indicated general thermal satisfaction except where great differences in temperature between the coldest and warmest spaces within the auditorium occur, as it gets colder in higher levels. The study recommended to reduce the heating loads required through passive techniques while avoiding the overheating effect in summer.

Based on the first project, another auditorium building is to be designed in a different city – General Picowhich has a warmer winter but has higher cooling loads in summer. The base model is simulated exactly as the first project built in Santa Rosa, but then was modified to reduce energy consumption for both heating and cooling loads. For heating, the modified design used both solar air collectors and glazing areas for solar heat gains. The model indicated overheating in Summer, therefore, cooling strategies were incorporated. Those include natural ventilation, shading, insulation, paint color, and vegetation, as well as a cooling system. The simulation indicated 70% reduction in cooling loads.

After the second project was built and in order to validate and compare the results, the field measurements were taken for the modified design after construction. The measurements were taken in winter –unoccupied buildingand summer –fully occupied building. The measurements indicated a success in terms of reducing the vertical differences in temperature to only 1°C within the building. In summer, the average temperature is about 23°C which is within the comfort zone. The cooling system is required to perform in the extremely hot summer days. The new design achieved around 50% reduction in heating loads due to improved envelope insulation, direct and indirect solar heat gain, and air collectors. Another 70% reduction in cooling loads was achieved during summer time. A study by Ehsan *et* al (2012) investigated the provision of an optimized solution for retrofitting buildings in terms of cost efficiency and energy savings. The authors recognize the complicated inter-linked nature of the problem where multi aspects contribute to the overall performance of the building. The researchers reviewed several optimization solutions including cost-benefit analysis, multi-criteria analysis, multi-objective optimization, and energy rating systems, and therefore decided to approach the problem by applying a multi-objective optimization model. The problem was approached by presenting the multi-objective optimization model, then applying the model to an existing residential building in Portugal constructed in 1945. A list of building refurbishment strategies have been presented comparing the implementation costs vs. the energy savings obtained.

The study has taken into consideration four variables for retrofitting strategies which are different solar collectors, alternative insulation of building materials for walls and roof, and alternative window properties. The calculations have considered each strategy separately for simplification of equations. It has to be noted also that the equations used to calculate energy consumption for heating purposes took into consideration 26 parameters, while 6 were considered for cooling, and 5 for domestic hot water. Thermal performance and energy consumption of the base case model before applying the retrofitting strategies has been calculated using the Portuguese building thermal model (RCCTE) which did not take into consideration energy consumption by lighting systems.

The results of the study have emphasized that the application of a multi-objective optimization model on a residential building in Portugal has a non-linear relationship, where it is critical to study the deviation of implementation costs vs. energy savings for the various retrofitting actions, i.e. the cheapest implementation cost presented in the study was around 1791 €with about 15,263 kWh/year energy savings, whereas a one level advanced retrofitting strategy would cost about 1834 €with about 20,229 kWh/year savings.

Such a study provides decision makers with a good insight to establish a criterion for selection of an optimized building retrofitting scenario without compromising the cost efficiency of the solution.

The study has also recommended a further development to similar optimization model that would take into consideration other factors related to indoor environment such as thermal comfort, and air quality.

On a different aspect, a research was conducted to evaluate efficiency of design strategies in energy savings for different climatic zones, with focus on comparison on thermal performance in temperate-humid and hot-dry

climate. Similar to the studies conducted by Gugliermetti & Bisegna (2007) and Ehsan et al (2012), the study addressed thermal performance of the building envelope. Building envelope is one of the major building elements which contribute to energy consumption due to heat transfer. The study indicated that a one level upgrade in refurbishment solutions although of around 2.5% increased cost would result in 32% additional annual energy savings.

Another study conducted by Yilmaz (2007) investigated the thermal behavior of the building envelope in terms of the walls U-value and thermal storage characteristics. In order to emphasize the importance of considering both parameters, the study considers two different climatic zones which are the hot-dry, and the temperate-humid climates. A typical living room in a residential building with same orientation has been selected in two different cities in Turkey, one in Istanbul which has temperate-humid climate, the other in Mardin which has hot-dry climate. Three different wall compositions have been analyzed, wall 1 and 2 has the same U-value, whereas wall 3 has almost three times higher U-value but is a thick masonry wall.

The calculations indicate that although the U-value is the same in wall 1 and 2, their thermal behavior is different. What is more important to note is that the traditional masonry wall which has higher U-value is more suitable for hot-dry climate because of its high thermal mass property.

The researcher also addressed the problem in two case studies in Mandrin using experimental method. Field measurements were taken for two rooms in each of the two residential buildings. One building is a traditional 17th century building –Mungan house, the other is a modern building –Demir House 1990- that applied the Turkish Standards TS 825, Heating Energy Conservation Standard for Building in Turkey.

The field measurements were taken hourly for rooms of same orientation, and measured the temperature in several points. The first set of measurements showed the differences in temperature in the rooms for the traditional and the modern houses, as well as the overheating problem in summer for the modern house.

A second set of measurements were taken hourly for a third room, which measured the air temperature, wall surface temperature, and humidity level. The purpose of this study is to study of the contribution of thermal mass in the design. The results indicated that the indoor temperature is almost even throughout the day and night due to the high thermal capacity of the traditional wall.

As a final step, a questionnaire was conducted for the residents in both traditional houses and modern houses in the city to study their perception in terms of thermal, visual and air quality aspects. The survey included 68
traditional houses, and 32 modern ones. The questionnaire consisted of 36 questions with answered scaled in five points from being cold to being hot. The results of the survey supported the results of the experimental study.

In conclusion, the paper indicated the importance of thermal mass concept over the U-value characteristics in hot-dry climate. As well as highlighting that although the degree-day concept specified both Istanbul and Madrin within the same climatic zones, the cities do not have the same climatic characteristics. Therefore, the application of the TS 825 standards for both cities is not the best decision for energy conservation.

Further to the studies highlighted above, another study was conducted in China addressing upgrading of building insulation as one of the effective solutions to reduce energy in existing buildings. A combination of active and passive strategies, however, has proven to be efficient and achieve reductions in annual load up to 40% and 67% in Beijing and Shanghai respectively. The study conducted by Hiroshi *et* al (2006) addressed the thermal quality of the indoor environment in the urban areas within the residential sector. A three layered study approach was developed which included a questionnaire survey, experimental method, and mathematical method. Both the questionnaire and the field measurements were conducted for 8 cities in China representing the different climatic zones in china. The cities included: Harbin, Urumqi, Beijing, Xian, Shanghai, Changsha, Chongqing, Kunming, and Hong Kong. The survey period ranges from 1998 till 2004, included a total of 810 houses for questionnaire survey, and 76 for field measurements.

The questionnaire was based on a questionnaire model previously developed for a study in Japan. The survey meant to collect data related to building characteristics, heating periods, operation time for heating/ cooling systems, clothing types, and so on. The questionnaire was distributed to different social classes in the different cities, including pupils and their families, middle class families, and high class families. Along with the questionnaire, the families were provided with two liquid crystal thermometers, and were asked to measure the temperature in the living room and the bedroom, for five days, three times a day. Another set of field measurements were conducted to measure indoor and outdoor temperature, as well as humidity levels.

The results were discussed for winter and summer seasons based on the conducted survey. The results were summarized for eight parameters including buildings year of construction, building height, floor area, heating/cooling systems, operation periods of heating/cooling systems, peak heating/cooling periods,

temperature differences between the outdoor and indoor living room and bedroom temperatures, and the relation between the clothing factor and the room temperature.

The results of the experimental study was summarized for the eight cities indicating the thermal comfort levels using the psychrometric chart compared to the ASHRAE thermal comfort definition. The results were also summarized to indicate the variation in indoor temperatures and humidity levels for three cities in winter: Urumqi, Changsha, and Chongqing, and for Shanghai and Hong Kong in summer.

Based on the data collected from the questionnaire survey, and the field measurement, as well as weather data previously developed by ZHANG, mathematical calculations were used to estimate the heating and cooling loads for a model apartment both in Shanghai, and Beijing. The calculations were conducted for a base case model for both cities, and then developed cases 2 to 11 with several energy saving techniques including building insulation, increased ventilation, and shading by a balcony element, as well as a combination of several cases. In Beijing, the thermal insulation contributes to a maximum of 26% reduction in annual loads, whereas the reduction of air exchange rate contributes to a maximum of 28.4% savings. The shading through balconies was not an effective strategy. The combination of the best strategies contributes to total savings of 40% in heating and cooling loads. In Shanghai, thermal insulation tends to increase the cooling loads, whereas reduction of air exchange rate contributes to a maximum of 13.1% reduction in annual loads. With regards to shading by balcony, higher savings occur in summer but the overall annual reduction is estimated to be 1%. The combination of the strategies contributes to about 67% reduction in annual loads.

2.2.3 ACTIVE SYSTEMS

A research conducted in Hong Kong to assess potential of energy savings in existing high rise commercial buildings representing 15% of the total building stock. The study indicated that this sector contributes to around 60% of total energy consumption in buildings, and that the Mechanical Ventilation and Air Conditioning (MVAC) system is the major contributor of the energy consumption. This research conducted by Philip & Chow (2007) addressed the direct refurbishment techniques to improve building energy efficiency. The strategies included the following areas: enhancements in chillers, mechanical ventilation system, fresh air delivery, optimization of airside systems, increasing temperature by 2° C, integration of interior shading, and

Geothermal Heat Pump (GHP) system. With regards to the active systems, the findings of the research were positive as it concluded that major reduction in energy consumption within existing high rise commercial buildings could be achieved as following; The low-temperature air distribution system reduces the MVAC electricity consumption by 27%; GHP system reduces the total energy consumption of the building by 17% compared to the baseline model, at the same time the reduction of 31-41% of the peak MVAC load and peak building demand can be dropped by 31-41% respectively.

In conclusion, the study investigated the different heating and cooling systems within the eight cities for residential buildings. It also investigated the users' contribution to the thermal environment, whether it was by opening the windows for cooling, the pattern in which they operate the mechanical systems if existed, their clothing patter, and so on. Also, the study suggested economical energy saving strategies applicable for residential apartments in Beijing and Shanghai.

In addition to the research conducted globally to assess the potential of energy savings in existing buildings through refurbishment strategies and their economic feasibility. The following section aims at investigating the case of the Emirate of Abu Dhabi, the energy consumption in the built environment, Abu Dhabi's existing building stock, applicable building codes and regulations through the history, and identifying building prototypes based on chronological development of construction methods, architectural style, materials use, and building performance.

2.3 ENERGY CONSUMPTION IN THE UAE

After the discovery of oil in the UAE in 1960s, and the formation of the United Arab Emirates in 1971, the UAE witnessed a rapid development in all sectors. The energy consumption increased dramatically, which mainly is due to growth in population, economy, and urbanization. According to Kazim (2007) the population has doubled every 5 years since 1980 to reach around 3.25 million capita by year 2000. During this duration the UAE continued to have the highest energy consumption per capita compared to average rates in Europe, Middle East, the United States, and the World as shown in Figure 1. The peak energy consumption per capita in this duration has occurred in the 1990s, where it has gradually started to reduce towards 2000s. Similarly, Al-Iriani (2005) indicates that the electricity consumption average annual growth rate in UAE for the period from 1980 to 2000 is around 10% which is much higher than the world average growth rate of 3%.



Figure 1 UAE's energy consumption per capita compared to other regions from 1980 to 2003. (Kazim 2007, p. 434)

2.3.1 ENERGY CONSUMPTION PROFILE IN THE EMIRATE OF ABU DHABI

According to the recent release of Abu Dhabi Census Center (SCAD 2012), electricity consumption profile witnessed constant increase since 1972. However, there has been slight fluctuation in certain periods which can be best explained in the economical, industrial, and building construction development in the Emirate.

The data collected from the Abu Dhabi Statistics Center, Appendix A Table A1, the data stipulates the electricity consumption in MWH in the three regions of the Emirate: Abu Dhabi, Al Ain, and Al Gharbeia. It is with no doubt that Abu Dhabi witnessed the highest consumption of all time due to its status among the three regions in terms of economic development and political importance.

Based on the collected data, the following line chart -Figure 2- has been developed to illustrate the chronological increase in electricity consumption on a cumulative yearly basis. It compares all three regions together with the total consumption in the Emirate as a whole.





2.3.2 SECTORAL ENERGY CONSUMPTION

It is important to understand the energy consumption per building sector in the UAE in order to identify the most critical areas where refurbishment opportunities have the greatest impact in energy savings.

Building Sectors in the UAE can be grouped under the following sectors based on the building uses;

- Residential Sector
- Commercial Sector Offices, Retail, etc.
- Governmental Sector Community facilities, and other governmental buildings
- Industrial Sector
- Agriculture Sector
- Others

The above sectors are based on the land use categories specified by the Abu Dhabi Urban Planning Council, which is the legislative body which controls and regulates Abu Dhabi urban development.

UPC (2013) states the guidelines for development review process applicable to both master planning urban scale projects as well as single building projects.

Table 1 lists both main land use categories and sub-categories of each sector.

| Table 1 | General | Land | Use Ty | pe in i | the I | Emirate | of A | bu l | Dhabi. (| UPC | 2013, | p.2) | |
|---------|---------|------|--------|---------|--------------|----------------|------|------|----------|-----|-------|--------------|--|
| | | | | | | | | | | | | | |

| General Land Use Types | Specific Land Use Types | General Land Use Types | Specific Land Use Types |
|------------------------|---|------------------------|---|
| Residential | Single unit household Two to four households Multi households Institutional living Employee housing (permanent) Employee housing (temporary) Guest worker housing (permanent) Guest worker housing (temporary) Palace residential | Infrastructure | Transportation Utilities |
| Commercial | Automobile/vehicle sales, leasing & rental Business services Personal services Restaurants, cafes and fast-food Retail sales Convenience Retail Shopping Complex Office Commercial recreation Hotel | Community Services | Governmental services Police Civil defence Community centre Cultural institutions Petrol Station Mosque Other religions Post secondary education Private school Public school |

| | Conference/Convention/Exhibition Centre Other sales and service (walk in) | | Public health care Other |
|--------------|---|-------------------------|---|
| Industrial | General Industrial Heavy Industrial City serving industrial Research and Development | Open Space & recreation | Developed open space Natural open space Archeological |
| Agricultural | Farm Other | | |

According to the categories mentioned previously, Abu Dhabi Statistics Center (SCAD) 2011c has identified the electricity usage percentage per sector in the Emirate of Abu Dhabi since 2008. The data acquired from both Abu Dhabi Distribution Company, and Al Ain Distribution Company was presented in the SCAD (2011c) publication regarding energy and environmental statistics.

Table 2 shows the percentage of electricity consumed per sector in the emirate of Abu Dhabi for the period from 2008 until 2011.

Table 2 Percentage of Electricity Consumption Per Sector. (SCAD (2011c), p.6)

| Sector | 2008 | 2009 | 2010 | 2011 |
|-----------------|------|------|------|-------|
| Total | 100 | 100 | 100 | 100 |
| Domestic Sector | 39.6 | 37.7 | 35.9 | 30.7 |
| Commercial | 30.8 | 31.7 | 32.1 | 28.8 |
| Government | 16.9 | 16.2 | 16.1 | 25.1* |
| Agriculture | 9.1 | 9.2 | 8.2 | 7.0 |
| Industry | 2.4 | 3.7 | 7.2 | 8.0 |
| Other Sectors | 1.2 | 1.4 | 0.6 | 0.4 |

Source: Abu Dhabi Distribution Company, Al Ain Distribution Company

*Note: New meters were installed from 2008 and the cumulative reading of those meter were billed in 2011 for Al Garbia (Al Marfa)

The latest figures for the year 2011 indicates nearly an equal percentage of electricity consumption in the residential and commercial sector; both contributing to almost 60% of overall electricity consumption in the Emirate.

However, Radhi (2009) has indicated that the energy consumption for the residential sector in Al Ain for year 2005 accounts for the nearly 46% of its energy consumption. The industrial sector is the second highest consumer of energy among all sectors which accounts for nearly 25% of the consumed energy in 2005. Figures 3 & 4 highlight the sectoral energy consumption in year 2005 and 2011 for Al Ain and Emirate of Abu Dhabi respectively.



Figure 3 Sectoral Energy Consumption in Al Ain 2005. (Radhi 2009)



Figure 4 Sectoral Energy consumption in the Emirate of Abu Dhabi 2011 (Source: SCAD 2011c and Author)

Since this study focuses on the buildings prior to Estidama Pearl Rating implementation and the endorsement of the International Building Code tailor fir for the Emirate of Abu Dhabi, it is important to have an insight to the building stock prior to 2000s. According to Kazim (2007), in 1998, commercial sector in the UAE was responsible for 15.1% of its energy consumption, whereas 16.2% was caused by the residential sector. Again, this confirms that the energy consumption of both residential and commercial sector is almost equal. This trend has been almost consistent in the capital city of Abu Dhabi. However the residential sector contributes highly to energy consumption in other cities such as Al Ain. This is mainly due to Abu Dhabi having established a central business district (CBD) in an early stage during its development contrary to a city like Al AinSince the existing data indicates high energy consumption within the built environment in the UAE, and in light of the efforts internationally which highlights the potential of energy savings in existing buildings, the following section highlights the gap in refurbishment studies in the UAE.

2.4 THE GAP IN REFURBISHMENT STUDIES IN THE UAE

In the UAE, there has been limited research addressing energy savings through building refurbishment. In the past decade, there has been an increased awareness towards the need for implementing sustainable design approaches in new buildings which lead to establishing sustainability rating system in Abu Dhabi. However, there are no policies strictly addressing the energy saving aspect in existing building retrofitting. Unlike other countries which already implement sustainability ratings specifically designed for existing buildings, the UAE has not yet enforced any regulations in this area. The US Green Building Council, for example, has already set guidelines as part of the optional LEED rating system for existing buildings. LEED stands for Leadership in Energy and Environmental Design, the rating systems established by USGBC set measures to design, construct, and operate a sustainable development both on building scale and urban development scale (USGBC 2013).

However, a group of researchers in the UAE has launched a research project to assess the potential of energy saving in existing buildings in five of the Emirates; Abu Dhabi, Dubai, Sharjah, Ajman, and Ras Al Khaimah (AlNaqabi *et* al., 2012 and Alawadi *et* al., 2013). First, the research aimed at identifying the existing building stock in all five emirates in order to identify typologies for the second phase of analysis. However, due to lack of data at the time of research, especially in Abu Dhabi, the study focused on federal housing built by the Ministry of Public Works (MoPW). The first phase identified four prototypes responsive to the construction in 1974-1979, 1980-1989, 1990-1999, and 2000-2012. The first stage concluded that in a 1991 villa typology, approximately 37.2% reduction in annual cooling loads could be achieved if thermal insulation is upgraded to the requirements of 1 Pearl Rating based on the Abu Dhabi Urban Planning Council, Estidama requirements (UPC 2013b).

The second phase of the research was more detailed, where five villa typologies were simulated through IES-VE virtual environment software tool. The five prototypes represented the periods from 1970s, 1980s, 1990s, 2000s, and 2010s. the study conducted at minimum three simulations for each prototype; a base case, upgrade to 1 pearl rating, and upgrade to 2 pearl rating. The upgrade targeted thermal insulation for external walls, and roof, and glazing solar heat gain coefficient and u-value. The total reduction in annual cooling loads ranged from 27.5% to 29.8% in the case of upgrading to 1 pearl requirement, and from 28.5% to 30.8% in the case of upgrades to 2 pearl rating requirements. The study, however, recommended upgrading the houses to 1 pearl rating as the additional savings were minimal in the case of upgrading to 2 pearl. Based on the pioneer research project highlighted above, a significant gap in available validated information in the field of building refurbishment and energy savings in existing buildings has been identified. Also, as noted earlier, the lack of data to enable such studies has been identified. Therefore, it is essential to bridge this gap and further investigate the potential of energy savings in existing building stock through applications of refurbishment strategies. As one of the research contributors to the previously conducted research project, the author is aiming to investigate the potential in energy savings in existing buildings in Abu Dhabi through building retrofitting strategies. However, this study aims to focus on commercial building typologies rather than residential buildings.

The following section investigate the history of urban development in Abu Dhabi, this is to identify the existing settlements and the relevant periods of which the existing building stock is referred to, which also identifies the existing commercial building stick.

2.5 DEVELOPMENT HISTORY IN ABU DHABI

The Emirate of Abu Dhabi is considered one of the growing Emirates in the country and the region. It has notably been developed in the past decade. This development was a natural response to the increase of population. The Statistics Center – Abu Dhabi (SCAD 2011a) has indicated that the growth of Abu Dhabi population in 2010 is estimated to be nine times compared to 1975, with a growth rate of 4.5% from 2001 to 2005. This growth is directly linked to increasing land development and building construction industry.

In order to understand the status of the existing building stock in Abu Dhabi, and due to lack of data on existing building stock, an insight of the urban development of the Emirate is essential within the economic and urban growth context. The Emirate of Abu Dhabi pre-1960 and oil discovery was an organic vernacular settlement, which grew according to the needs of the residents. The settlements were mostly nearby the coast; since the residents were reliant on fishery and pearl collection from the Gulf Sea.

Pre-1960s the buildings were mostly two storeys buildings as seen in the following Figure 5



Figure 5 "Ariel View Showing Residential Neighborhoods in the 1950s in Al Bahya Town." (Abu Dhabi Municipality & Town Planning Department 2003, cited in AlKaabi 2011, p. 123)

According to AlKaabi (2011), the first master plan prepared for Abu Dhabi Island was proposed in 1962 and later updated in 1966. In 1968, settlement in Abu Dhabi was still around the north-west along the cost, as shown in Figure 6. These master plans produced after the discovery of oil from Abu Dhabi have to be assessed in conjunction with the economic and political developments which occurred during the late 1960s and early 1970s; as economic and political development had great impact on the status of both Abu Dhabi and Dubai.

The United Arab Emirates was announced as a state in 2nd of December 1971. That is also happened to be after the first exports of oil both in Dubai and Abu Dhabi in 1962 and 1969 respectively. (National Media Council 2008). Parallel to those events, the Municipality of Abu Dhabi was founded in 1962. At first, the municipality was named as "Department of Abu Dhabi Municipality and Town Planning". Later, the need for a well-planned city had led to the issuance of a royal decree in 1969 to appoint the first municipal board. (ADM 2013).



Figure 6 Ariel View of Abu Dhabi in 1968. (Abu Dhabi Municipality & Town Planning Department 2003, cited in AlKaabi 2011, p. 134)

Similar to the recordings of AlKaabi (2011), in conference the 17th ICOMOS General Assembly (2011), researchers from Abu Dhabi Authority of Culture and Heritage (ADACH) explained that the initial master plans proposed for Abu Dhabi city early 1960s have been put into implementation later in the decade.

From that point onwards, Abu Dhabi city witness a transformable urban development, introducing various land uses including residential developments and supportive infrastructure and community facilities.

The initial implementation phase of the master plan was planned between 1962 and 1968. Later stage was proposed by 1974. During that stage, the Department of City Planning in Abu Dhabi was chaired by Dr. Abdul Rahman Hassanein Makhlouf. (Abu Dhabi awards 2013).

As noticed in Figure 7, the city is based on a grid-system urban morphology. The majority of the urban development occurred in the northern-east part of the island. The residential and mixed-use developments were mainly between the streets currently known as Corniche Street, and Electra Street North-South and Salam Street to the East until the Old Souq area to the west. The industrial zone was further down towards the south-east of Electra St.



Figure 7 Part of Abu Dhabi in 1974. (ADSIC 2009, p.4)

2.5.1 FIRST BUILDING DEMOLITION MOVEMENT

As the Department of City Planning in Abu Dhabi became functional, the implementation of the planned urban development took place. Unfortunately, and according to Chabbi & Mahdy in conference The 17th ICOMOS General Assembly (2011), p.77;

"The design and construction of the buildings had often been of inferior quality because the demand was so high and quality control mechanisms were not fully in place, therefore in the following decade, a wave of "reconstruction" was undertaken to replace this stock of buildings."

It is obvious that the population growth that started in 1970s has led to great transformation in the urban development in the Emirate of Abu Dhabi. But what is also clear, is that the building construction which took place as the expatriates movement towards the country increased, has been of poor quality that many of the buildings had to be deconstructed later on. Another reason why building demolition took place at that point in time, is that the low-rise horizontal city development was moving towards vertical developments where new building heights were allowed. Of course this led to more and more structures being reconstructed to allow for higher buildings.

2.5.2 ABU DHABI AFTER 1980s

Contrary to the situation during 1970s, the urban development in the Emirate was more organized and controlled since 1980s. That is basically due to the earlier formation of the Department of City Planning, and the efforts that took place as the city developed. This, if anything, indicates that the majority of the existing building stock in the Emirate of Abu Dhabi, and within the Island in particular, has been developed in the 1980s onwards.

Although, great efforts have been made after the establishment of the department of City Planning in Abu Dhabi; it wasn't until 2007 when the Abu Dhabi Urban Planning Council (UPC) was formed by the law 23 of 2007. (UPC 2011). The Urban Planning Council has developed the 2030 vision of the Emirate and published the Urban Framework Plans for the Emirate of Abu Dhabi. This vision aimed at a well-planned sustainable built environment in the Emirate of Abu Dhabi including plans for the Western Region, Abu Dhabi, and Al Ain.

2.6 BUILDING STOCK IN ABU DHABI

This section aims at identifying the geographic boundaries of the study within th Emirate of Abu Dhabi, as well as understanding the existing building stock. The section first explains the jurisdiction of the Emirate of Abu Dhabi and identifying the major cities then narrows down to the area of the study. This is followed by the analysis of the existing settlement and the understanding of the existing building stock.

2.6.1 DEFINING GEOGRAPHIC BOUNDARIES

The Emirate of Abu Dhabi which accommodated nearly 2.0 million residents in 2010, consists of three regions: Abu Dhabi, Al Ain, and the Western Region as well as the Emirates Islands. (SCAD 2011a).

A recent survey by the General Census of Population, Housing and Establishment, 2005 (SCAD 2012b) has indicated that Abu Dhabi Region is the first contributor to the provision of housing units in the Emirate with 137,857 housing units, followed by Al Ain with 83,528 housing units. While the Western region contributed to only 20,002 units of a grand total of 243,251 housing units in the Emirate in 2005.

Both Abu Dhabi and Al Ain regions are the most inhabited and developed regions within the Emirate of Abu Dhabi. And since Abu Dhabi region contributes to 85% of completed buildings within the Emirate (SCAD 2011b); the research project has considered Abu Dhabi region to be the focus of the study.

In order to understand the chronological order of building construction in Abu Dhabi in a geographical context, analysis of the settlement growth and expansion of urban development is essential. The analysis is required, to develop a detailed understanding of the urban settlement in Abu Dhabi City and Abu Dhabi Metropolitan in particular.

Abu Dhabi Metropolitan includes Abu Dhabi City and the sub-urban and rural settlements outside the Island. Abu Dhabi Island is the core settlement where the major development has taken place for the past forty or more years. Other recent developments such as Mohammad Bin Zayed City, Khalifa A City, Khalifa B City, Masdar City, Al Raha Beach Development, And other future cities are all developments located outside the Island. There are also other sub-urban and rural settlements outside the Island within Abu Dhabi Metropolitan which are relatively old and includes low density housing projects such as Al Rahba, Al Shamkha, Al Bahia, Al Wathba, Al Samha, and others which were developed mainly with prototypes of extended family housing.

Figure 8 illustrates the precincts of Abu Dhabi Metropolitan based on Plan Abu Dhabi 2030 as part of the urban structure framework plan.



Figure 8 Precincts map of Plan Abu Dhabi 2030. (UPC 2010, p. 85)

2.6.2 URBAN DENSITY - AN INDICATION OF CHRONOLOGICAL SETTLEMENT

It is understood that areas with higher densities are the areas where the urban development first started to expand, which does not necessarily imply that existing buildings in those areas are the oldest but could be for the most part.

The following map –Figure 9- illustrates the population density in Abu Dhabi Island in 2005. It shows that the northern central and northern eastern part of the Island has the highest densities, which happens to be also the part where the relatively older buildings exist. This has been also highlighted by Dr. Essam Saleh – from the town planning department of the Abu Dhabi Municipality- during an interview on June 28th, 2012.

The same has been concluded in the previous section 2.5, where the urban development after discovery of oil all through the formation of the town planning department in the Abu Dhabi Municipality and later after the formation of Abu Dhabi Urban Planning Council has been explained. The chronological urban development reflects the existing building stock in each of the timeframes.



Figure 9 Population density by sector on Abu Dhabi Island matching DPE census data and building points with DMA sector boundaries. (Abu Dhabi Spatial Data Infrastructure 2012, p.1).

As highlighted earlier, this research mainly focuses on the commercial buildings inclusive of mixed-use and office buildings in Abu Dhabi. Therefore, the industrial zone located outside the Island which is Mussafah Industrial City will be beyond the scope of this study.

Having set the research project physical boundaries based on population and building densities as well as land use structure, it is critical to analyze the building construction development in this context based on the various land uses throughout the intended timeframe scope of the study.

2.6.3 EXISTING BUILDING STOCK DATA

As explained earlier, building construction in Abu Dhabi has started after the discovery of oil in the 1960s. The earliest census data obtained from the Census Center – Abu Dhabi is dated back to 1975 with 10 years' time interval for data collected. Other data was available from official publications in Abu Dhabi which mainly covers the years from 2001 to 2010. The data collected is combined and presented in Table 3.

| Voor/Type of Building | | 1975 | 1985 | 1995 | 2001 | 2005 | 2010 |
|-----------------------|---|-------------|-------------|-------------|--------------|-------------|---------|
| fear/ | Type of Building | Number | Number | Number | Number | Number | Number |
| | Villa | 1,601 | 4,741 | 7,194 | 5,289 | 10,803 | |
| | Apartment/multistorey | 4,468 | 29,235 | 47,925 | 15,095 | 3,632 | |
| | Deluxe Apartment | 0 | 0 | 617 | 160 | 0 | |
| Residential* | Arabic House | 13,450 | 1,475 | 230 | 0 | 0 | N/A |
| | Popular/ low-cost House | 6,386 | 7,871 | 6,987 | 11,644 | 13,434 | |
| | Single Storey Building | 0 | 0 | 1,206 | 5,413 | 4,602 | |
| | Others | 8,742 | 20,506 | 23,679 | 27,427 | 7,537 | |
| | Total | 34,647 | 63,828 | 87,838 | 65,028 | 40,008 | 270,428 |
| | Hospitals (all) | N/A | N/A | N/A | N/A | 33 | 33 |
| | Health Centers (all) | N/A | N/A | N/A | N/A | 435 | 435 |
| Healthcare Facilities | Clinics (all) | N/A | N/A | N/A | N/A | 239 | 239 |
| | Government Hospitals | 2 | 10 | 13 | 12 | 13 | 12 |
| | Government Clinics - Centers | N/A | N/A | N/A | N/A | 48 | 48 |
| | Private Schools | 12 | 54 | 149 | 178 | 201 | 184 |
| Caluaration. | IGovernmental Schools | 77 | 159 | 246 | 316 | 322 | |
| Education | Universities (all) | N/A | N/A | N/A | N/A | | 9 |
| | Colleges and Institutes (all) | N/A | N/A | N/A | N/A | Γ | 20 |
| Hotels | | 10 | 19 | 39 | 49 | 55 | 115 |
| Commercial** | | 13,736 | 55,635 | 76,419 | 98,917 | 117,254 | 165,072 |
| | | | | | | | |
| Sources | SCAD (2010): Abu Dhabi in Fig | gures: 2010 |). | | | | |
| | SCAD (2011a): Abu Dhabi in F | igures: 201 | L1. | | | | |
| | SCAD (2011b): Building Comp | letion Stat | istics: Mar | ch Quarter | 2011. | | |
| | SCAD (2012): Abu Dhabi: Dev | elopment | Statistics: | 1960-2010. | | | |
| | SCAD Census Data for Abu Dh | abi from 1 | 975 to 2005 | obtained | directly fro | om the Stat | tistics |
| | Center of Abu Dhabi | | | | | | |
| | | | | | | | |
| | Notes: | | | | | | |
| | * For Residential units, data r | eflects the | units with | iin Abu Dha | abi only. H | owever the | e total |
| | number of units for Year 2005 includes residential units in the Emirate inclusive of Al Ain | | | | | | |
| | and the Western Region | | | | | | |
| | ** Commercial category is as | sumed to r | eflect the | building st | ock catego | orized unde | er |
| | "Buildings" as per SCAD (2012 |) data. | | | | | |

| Table 3 Summary | of Abu Dhab | i Existing Building | Stock (Statistics | Center – Abu Dhabi) |
|-----------------|-------------|---------------------|-------------------|---------------------|
|-----------------|-------------|---------------------|-------------------|---------------------|

The data collected from Abu Dhabi Statistics Center (SCAD 20120) - represented in Appendix A Table A2- is summarized in the chart representation of the data provided in Figure 10. The chart indicates that the building stock in the Emirate of Abu Dhabi gradually increased from 1968 to late 1970s. The years 1978-1980 witnessed a great increase in the number of buildings constructed with almost 22,600 new units were constructed. The increase in the total number of new buildings constructed in Abu Dhabi continued until 1986 were the existing building stock started to decrease gradually. However, the construction industry picked up again and the building stock was increasing steadily from 1993 onwards with minor fluctuations.



Figure 10 Key Statistics of Construction Activity in The Emirate of Abu Dhabi. (SCAD 2012)

Data collected from the Statistics Center – Abu Dhabi included a breakdown of different building land uses in terms of building permits numbers, mostly for years from 2005 to 2010. The land uses include:

| Residential | Public Utilities | Temporary |
|-------------|----------------------------|-------------------------|
| Commercial | Agricultural | Annex of low cost house |
| Industrial | Residential and Commercial | Others |

Also, the various types of building permits were obtained for the same period. This includes total number of permits for the following categories: New, Refurbishment, Temporary, Demolition, and Others.

Based on the data collected, and as indicated in Table 4, both the Residential use and Temporary buildings have the highest number of building permits from year 2005 to 2009, followed by the industrial and public utilities uses. Total number of building demolished for years 2009 & 2010 combined in Abu Dhabi is 371 permits.

| | | Number of Permits | | | | | |
|----------------------------|--------------------------------------|-------------------|------------|-------------|--------------|--------------|--------------|
| | | 2010* (AD) | 2009* * | 2008 (AD | 2007 (AD+ | 2006 (AD+ | 2005 (AD+ |
| Permit Category | Permit sub-category | | (AD) | +WK) | WK) | WK) | WK) |
| New | New Buildings | 2,066 | 1,429 | | | | |
| | Permits for Renewal or amendments | 642 | 655 | | | | |
| Refurbishment | Additions | 1,872 | 2,609 | | | | |
| | Improvements and decorations | 2,028 | 22 | | | | |
| Demolition | Demolition | 107 | 264 | | | | |
| Others | Others types of permits | 274 | 211 | | | | |
| Residential | | 4,473 | 3,718 | 1,401 | 852 | 907 | 705 |
| Commercial | | 968 | 388 | 222 | 134 | 67 | 67 |
| Industrial | | 638 | 338 | 229 | 252 | 192 | 169 |
| Public Utilities | | 3 | 424 | 335 | 240 | 250 | 278 |
| Agricultural | | 80 | 0 | 0 | 0 | 0 | 0 |
| Residential and Commercial | | 6 | 296 | 0 | 0 | 0 | 0 |
| Temporary | | 279 | 3,629 | 1,768 | 949 | 3,682 | 3,162 |
| Annex of low cost house | | | | 174 | 889 | 957 | 1,566 |
| Others | | 821 | 26 | 0 | 0 | 0 | 0 |
| Total | | 7,268 | 8,819 | 4,129 | 3,316 | 6,055 | 5,947 |
| | Sources: | | | | | | |
| | * SCAD (2011a) | | | | | | |
| | ** SCAD (2010) | | | | | | |
| | Notes: Years 2005-2008 includes perm | its for Abu | ı Dhabi an | d the West | tern Regio | n | |

As concluded from the above statistics and data, commercial buildings are one of the major contributors to energy consumption in Abu Dhabi. Therefore, it is vital to further study and analyze the status of the existing commercial building stock to identify the best typologies representing the buildings in Abu Dhabi. Also, it is important to investigate the total Gross Floor Area (GFA) of the commercial buildings. This will allow identifying the impact of the refurbishment strategies –topic of this study- on a large scale covering the overall existing commercial building stock.

The following section addressed the statistics and data regarding the existing commercial building stock.

2.6.4 EXISTING COMMERCIAL BUILDING STOCK

As indicated in the chronological development in the city of Abu Dhabi, and through the construction and demolition stages that affected the existing building stock in the Island, it is noted that the majority of the existing commercial building stock from mid-1980s is located in the northern east part of the island -namely, the developments between the streets currently known as Corniche Street, and Electra Street North-South and Salam Street to the East until the Old Souq area to the west. This zone includes the Central Business District (CBD) in Abu Dhabi.

From mid-1990s onwards, the development in Abu Dhabi island extended towards Al Muroor Street and Airport Road to the south, and towards Al Bateen and the west side on the Corniche. In the recent years, the mixed use developments reached out to the Grand Mosque District starting. The following Figure 11 indicates the units per building within the northern part of the island, and Figure 12 provides an indicative breakdown of the existing uses within the island of Abu Dhabi. Both figures representing units densities and land use breakdown supports the data provided earlier, and defines clear separation between three decades of existing mixed-use development;

- 1. 1980s 1990s
- 2. 1990s 2000s
- 3. 2000s 2010s



Figure 11 ADCP Properties Units by Sector in Abu Dhabi Island. (ADSIC 2009, p.5)



Figure 12 Abu Dhabi Land Use Allocation Tracking. (ADSIC 2009, p.9)

Besides the analysis conducted on the urban development and master planning level development in Abu Dhabi to understand the existing building stock and commercial building stock; and due to the lack of data and information; interviews with contemporary architects and engineers were conducted. Interviews with Arch. Munir Kosnik and Eng. Elias Shahin on The 2nd of April 2013 and The 25th of August 2013 respectively concluded that the leasable spaces in the island of Abu Dhabi were considered as commercial uses, and that the buildings designed since 1980s were considered for either office or residential uses. Therefore majority of the existing commercial building stock are residential conversion of the buildings, especially for the buildings constructed from 1980s to mid-1990s.

A recent publication by the Abu Dhabi Urban Planning Council included an assessment of the existing office market (UPC 2010b). The study highlighted that the existing building stock as of 2009 is of poor quality office space, and that residential conversion contributes to a good portion of the available office space.

The study gave a ranking of four levels A to D; A being the best quality office space based on international quality and professionally managed space to D being the worst quality.

- Grade A offices represent less than 17% of the existing building stock majority of which are built recently (after 2005) for governmental or semi-governmental entities such as Abu Dhabi Investment Authority, Al Mamoura Building, AlDar HQ, etc.
- Grade D offices represent residential conversions with the poorest quality of office spaces.

The following chart -Figure 13- provides a percentage breakdown of an overall 1.8 million square meters of office space as of 2009 in Abu Dhabi.



Figure 13 Percentage breakdown of the existing office space in Abu Dhabi as of 2009. (UPC 2010b, Author)

According to the study, around 800,000 square meters of office space is provided within the Central Business District. Whereas around 550,000 square meters of grades B and C office spaces are provided along Al Muroor road and Abu Dhabi road. Most of the other office supplies within the island of Abu Dhabi are also of Grades B and C. Around 200,000 square meters of Grade A office spaces are provided outside the island within the Abu Dhabi Metropolitan. (UPC 2010b).

The total office space in Abu Dhabi in 2007 was indicated at 1.4 million square meters (UPC 2010a). And since the Grade A office buildings represent around 300,000 square meters and has just recently been developed, 200,000 square meters of which were developed outside the island, then it is assumed that at least 93% of the 1.4 million square meters office space as of 2007 are grades B,C and D.

Moreover, and based on the previous data, it is concluded that Grade D office space of 160,000 square meters are those who were built in early to mid-1980s, and within the CBD area. It is also concluded that the Grade B and C buildings within the Almuroor and Airport roads represent the building stock in 1990s.

For this study, and based on the above, the following figures in Table 5 will be considered;

| Period | Location | Grade | Office Space – GLA* | Office Space – |
|-----------|------------------|--------------------|---------------------|---------------------|
| | | | (Square Meters) | GFA*(Square Meters) |
| 1980-1985 | CBD | D | 160,000 | 200,000 |
| 1986-1989 | CBD | C (44% of 800,000) | 280,000 | 350,000 |
| 1990-1999 | CBD | B (30% of 800,000) | 360,000 | 450,000 |
| 1990-1999 | Muroor – Airport | C (60% of 550,000) | 330,000 | 412,500 |
| | Roads | | | |
| 1990-1999 | Muroor – Airport | B (40% of 550,000) | 220,000 | 275,000 |
| | Roads | | | |

Table 5 Summary of Office Building Survey from 1980-1999. (UPC 2010a, UPC 2010b, Author)

Note: * GLA = 0.8 * GFA (Gross Floor Area) (Source: UPC 2010b).

It has to be noted that the office space available per capita as of 2009 is much lower than the international standards representing only 1.9 square meters per person. (UPC 2010b).

According to the data provided in the previous sections, the following is concluded;

- Commercial buildings as well as residential buildings are the major contributors to energy consumption within the existing building stock in Abu Dhabi city.
- Commercial buildings with reference to statistics collected under the category of Buildings- witnessed a boom in construction late 1970s to mid-1980s. From 1986-1993 the existing stock decreased. After 1993, building stock increased gradually till 2010.
- Around 3% of total permits issued on 2009 in Abu Dhabi were demolition permits. However, 4.5% were the permits given for new commercial building construction.

The following section provides an insight to the different building regulations that governed the building design and construction in Abu Dhabi.

2.7 BUILDING REGULATIONS IN ABU DHABI

Buildings codes and regulations are usually set by the government to regulate building performance and building design parameters. In Abu Dhabi, the Municipality of Abu Dhabi (ADM) is the regulatory authority which sets the building codes, review the building applications, and issue the building permit. The Municipality of Abu Dhabi (ADM) was found in 1962. It was called "Department of Abu Dhabi and Town Planning". However, the need for a well-established municipal board was recognized. In 1969, the first municipal board was appointed by the issuance of a royal decree (ADM 2013).

The first local order (1) of 1976 was issued related to building regulations. These regulations were followed by the issuance of Decree (4) of 1983 related to building construction regulations, followed by an amendment concluded by Decree (4) of 1985. Administrative law (20/94) of 1994 was later issued related to executive list of the previous building regulations. The issued regulations did not set a specific criteria or requirements for building performance related to energy savings such as building envelope thermal performance. However, recommendations were stipulated under Article (43) of 1983 - Chapter 2 Architecture and Design Building Regulations. The recommendations included the following (ADM 1983);

Building orientation and use of shading elements in relation to prevailing wind

- The use of thick walls and insulated walls
- The use of thermal insulation and water proofing for the roof. As well as using shading devices for the roof such as pergolas
- Provide windows to floor ratio that do not exceed 1:6. It is recommended to use shading devices for the windows
- For glazing, reflective glazing is recommended. Where direct solar gain is anticipated, double glazed reflective glazing is recommended
- The selection of windows framing with minimal infiltration
- For exterior building finishing, paints selection of white and light colors is recommended.

While all the above relate to building thermal performance, these recommendations were not set as regulations and were never enforced on any building development.

It was not until 2009 that the Department of Municipal Affairs (DMA) –Higher committee of Abu Dhabi Building Codes has issued the 2009 International Building Code for Abu Dhabi. However, the building code has not been made mandatory as yet. (DMA 2013).

In 2010, Estidama Pearl Rating Systems minimum requirements were made mandatory by the Executive Council Order of May 2010. For all new buildings, at least 1 pearl rating must be met, whereas governmental buildings are required to meet a minimum of 2 pearls under the Pearl Building Rating System. (UPC 2013b). Estidama is the Arabic word of sustainability. Estidama team has been formed in 2007 as part of the Abu Dhabi Urban Planning Council. Estidama issued three different rating systems including;

- Pearl Building Rating System (PBRS)
- Pearl Community Rating System (PCRS)
- Pearl Villa Rating System (PVRS)

As highlighted above, all buildings subject to this study fall within the timeframe where no specific regulations were enforced relevant to building performance and energy savings. However, it has been noted that after the building demolition which occurred in 1970s, many international consultancy firms moved to establish new business in the UAE. Also, many professionals and contractors were inspired by the international trends and best practices in building design and construction. This trend influenced the quality of the building design and construction, therefore many of the buildings designed late 1980s onwards started to use thermally insulated walls and double glazing windows providing a better building envelope performance than that specified in the concurrent regulations at that time. Interviews conducted with Arch. Munir Kosnik, Eng. Elias Shahin, Arch. Azza Al Sayed who worked in Abu Dhabi during that time all confirmed the same.

The following section presents the different trends in building design and construction in Abu Dhabi with regards to commercial buildings. The section identifies representative building typologies for existing buildings subject to this study for the timeframe from 1980-1989 and 1989-1999.

2.8 DEFINING BUILDING TYPOLOGIES

As highlighted in the previous sections, the existing building stock in Abu Dhabi mostly refers back to mid-1980s. However, there were no regulations set to control building performance in terms of energy efficiency and thermal performance of the building envelope. It wasn't until 2010 that Estidama pearl rating systems were made mandatory. Therefore, in terms of regulatory framework, the existing building stock should have been treated the same with regards to energy and thermal performance. However, as noted earlier, this wasn't the case since the buildings designed in the late 1980s were of better design and construction quality. This section will further investigate the identified timeframes for this study being 1980-1989 and 1990-1999. In order to identify the building typologies, the architectural character and construction materials of each period have to be identified. Besides the background research conducted earlier, the lack of available data and information has been bridged through the following;

- Review of data collected through EMPORIS database which provides buildings related information globally (EMPORIS 2013)
- Personal interviews with Architects and Engineers who have worked in the construction industry in the UAE since 1970s.
- Field observation in Abu Dhabi

The building database collected and provided by EMPORIS online is presented in a comparative format in Appendix B. A total of 217 buildings are provided with information related to their height, year of construction, architectural style, location, visual image representation, consultants, etc.

The analysis of the data collected indicates that the majority of the buildings go back to 1980s with few exceptions which are hotel establishments, or iconic buildings such as Etisalat tower, and other few residential buildings which were constructed early 1980s and late 1970s.

The buildings from mid-1980s until 2010s range from 15-25 storeys in height with low to high rise buildings category. The higher the building the recent it was constructed. Also, it is noted that the majority of buildings pre-1990s were of postmodern architectural style and with concrete structures. Steel was introduced late 1990s, and more complex structures after 2010 as taller buildings and skyscrapers were constructed. Modern architectural style was introduced from mid-1990s onwards, and it was more evident after year 2000.

Furthermore, personal interview with Eng. Elias Shahin on 25th of August 2013 –who has been working in Abu Dhabi since 1970s- highlighted the following;

- Buildings in 1970s were low-rise buildings from 3-5 storeys usually ground floor, mezzanine floor, and two typical floors. In 1970s there was no building review process similar to what is existing nowadays, however the building design was reviewed as part of the review process run by Sheikh Khalifa Committee, which was a governmental department responsible for providing loans for Emirati residents to build their houses. There was also the social services and commercial buildings department. Very few of those buildings still exist, and mostly around what is known as Electra and Jawazat streets
- Buildings in 1980s and 1990s were on average around 20 stories height.
- The buildings in 1980s were mainly conventional window design, single glazing, solid concrete structure with plaster or paint finishing. Stone cladding was introduced at a later stage in the same period. Majority of the buildings used no wall insulation (hollow block) and were poor in terms of thermal performance.
- Towards the end of 1980s, the buildings started using wall insulation and double glazing. Also curtain walls and aluminum cladding started to appear in some of the buildings designed late 1980s and early 1990s.
- There is a change in the AC system used between pre-1990s and post-1990s. The majority of the buildings used window type air conditioning units before 1990s with few exceptions of iconic buildings. It was later that the central AC system was used for provision of cooling systems within the buildings.
- It has also been noted that the majority of the existing building stock from the 1980s is around whats is known as Tourist club area, Hamdan Street, and Khalifa Street.
- Office buildings were defined under what was called commercial building. The buildings were designed to suite residential units, offices, and ground floor retail spaces.
- Integration of external shading was not given attention at any time because the building regulations did not allow for any extrusions beyond the plot line, and the building owners wanted the maximum built area to be used for profitability.

Another interview conducted with Architect Munir Kosnik on 2nd of April 2013 – who has been working in the UAE since late 1980s- highlighted the following;

- In late 1980s and 1990s any leasable space was called under commercial space. In other words, whether the building is designed for a residential apartment or for offices both were accommodated under commercial building terminology
- It is difficult to identify existing stand-alone office buildings which go back to 1980s.
- Buildings in 1980s followed a conventional design approach with concrete buildings.
- A mix of glazing and solid external cladding was used still used in late 1980s and early 1990s.
- Building insulation and double glazing were in use in 1989 onwards.

An interview with Architect Azza Al Sayed on 5th January 2012 – who has been working in Abu Dhabi since 1970s- highlighted the following;

- There were no specific requirements for building performance in terms of energy consumption and thermal performance. International Building Code however was made available in 2009 but was not mandatory; however some consultants were guided by the draft code.
- Sheikh Khalifa Committee -which was a part of the Abu Dhabi Municipality and is no longer availablehad in position all buildings drawings and specifications pre and during 1980s; as they were approving the grants for Emirati people.
- There were main consultants and contractors who had influenced the market and provided a better quality product based on best practices. Some of which are still working till date.

Based on the data provided above, the interviews, and personal walk-throughs and observatory analysis of the existing building stock in Abu Dhabi, the following summary of the existing commercial building typologies is concluded –presented in Table 6.

| Comparison Criterion | Buildings from 1980 to 1989 | Buildings from 1990 to 1999 | | |
|-------------------------|-----------------------------------|-----------------------------------|--|--|
| Building use | Mixed use- offices as residential | Mixed use- offices as residential | | |
| | conversion | conversion. | | |
| | | Stand-alone office buildings | | |
| Building Height | 15-20 floors | 20-25 floors | | |
| Architectural Style | Post-modern | Post-modern and Modern | | |
| Construction Material | Concrete | Concrete and Steel structures | | |
| Cladding Type | Block wall with plaster or paint | Curtain wall type. | | |
| | finishing. | Aluminum cladding. | | |
| | Stone cladding introduced later. | Stone Cladding | | |
| Wall Insulation | No wall insulation | Thermal insulation provided | | |
| Glazing type | Single glazing | Double glazing | | |
| Shading | Not prioritized | Not prioritized | | |
| Air Conditioning System | Window type unit | Central AC system | | |

Table 6 Comparison Summary of Existing Commercial Building Typologies in Abu Dhabi from the period from 1980 to 2000. (Author)

Based on the literature review and background research presented earlier, the identification of the research problem, and the research aims and objectives have been developed. The following section presents the problem identification, followed by the aims and objectives.

2.9 PROBLEM STATEMENT

Since the discovery of oil in 1960s, the UAE has been rapidly developing. The construction industry has negatively impacted the environment on many levels, one of which is related to the huge consumption of energy in the built environment which contributed to nearly two-fifth the total energy consumption. Recently, the country became effectively involved in global environmental initiatives such as Montreal Protocol in 2013. Such involvement reflects the growing awareness of the country towards protecting the environment and saving the natural resources.

The efforts of the Abu Dhabi Urban Planning Council through mandating minimum requirements for building, villa, and community developments through the enforcement of the Estidama Pearl Rating Systems, is considered a step towards achieving the goals set for the country to reduce energy consumption, use of alternative clean energy resources, and many others. The environmental initiatives, regulations, and requirements adopted in the UAE are applicable and targeting new buildings only. However, in Abu Dhabi the existing building stock, which contributes to more than 70% of the existing building stock as of 2005 to 2010 statistics, lacked any enforcement of sustainable building regulations.

In the Emirate of Abu Dhabi, around 85% of the existing building stock is accommodated in Abu Dhabi city. In 2011, the energy consumption of commercial buildings and residential buildings evenly contributed to nearly 60% of the total energy consumption of the built environment. Moreover, additional 25% was identified as the energy consumed by governmental buildings, which also included governmental offices and facilities.

Having mentioned the above, it is essential to investigate the means to reduce energy consumption in the existing building stock in Abu Dhabi, specifically for office buildings which together with the governmental buildings contributes to around 55% of total energy consumption in the built environment. In this context, and due to lack of validated information, this research aims to investigate the energy savings potential in refurbishing existing buildings in Abu Dhabi through passive strategies. The study focuses on commercial buildings in the Abu Dhabi Metropolitan, and it covers the buildings built pre-1970s to 2010 with focus on two case studies of one building built in 1980s and another in 1990s. A financial feasibility study will be conducted to weigh the passive strategies proposed within the refurbishment process in terms of its cost versus its efficiency in achieving higher energy savings.

CHAPTER 3: METHODOLOGY

3 METHODOLOGY

3.1 METHOD SELECTION

Selection of an appropriate research method is essential to enable the study being conducted within the applicable limitations of the studied program. A full understanding of the applicable research method used to assess the energy savings in existing buildings is important prior to initiating the study. Also, a comprehensive understanding of the limitations of the preferred methodology is required to assist in the applicability to the research timeframe. Such limitations include research resources, time, applicability to the research problem, validity of the research method, and economic feasibility.

3.2 COMPARISON OF RESEARCH METHODS APPLICABLE TO THE RESEARCH

The assessment of the contribution of passive design strategies in energy savings in existing buildings could be investigated through the following four research methods, i.e. laboratory approach, modeling approach, field measurement approach, and literature review approach. Each of those approaches has its limitations when applied to this research, as discussed in this section.

In general, there are two approaches mostly applied by the researchers in this field which are modeling and field measurement approaches.

3.2.1 LABORATORY APPROACH

The laboratory approach is an experimental type of research methods. It involves a controlled environment in a physical lab, where controlled variables are standardized forming a baseline to enable the investigation related to the effect of an independent variable throughout the study. The results of the study will be seen through the dependent variables or the outcomes in comparison to the standardized (baseline) scenario (Ross & Morrison, 2012).

Within the context of this particular research, the application of this approach to the designed research problem is quite limited. Not only this approach would be expensive and requires a lot of time to perform, it also is complicated to structure due to requirements of research instruments, and the means to control the research environment. Researchers in this field do not tend to apply this approach to their studies. And for the purpose of this study, it is also not preferred.

3.2.2 MODELING APPROACH

The modeling approach is another type of experimental research method defined by Ross & Morrison (2012). Typically, a representative physical model of the experiment is developed to clone the actual conditions and context from reality to a different scale controlled environment in order to facilitate conducting the experiment.

The application of the modeling approach to this study could be translated through a digital model instead of a smaller scale physical model. That is to simulate the exact conditions from real life through simulation software and digital tools. This application of the modeling approach is less time and resource consuming. It is also widely applied by the researchers in this field.

3.2.3 MODELLING APPROACH THROUGH SIMULATION MODEL

The simulation tools can provide the best assessment and flexibility when it comes to assessing and comparing several strategies in terms of thermal and energy performance. It is a cheaper method compared to experimental method, and does not require extensive human and physical resources.

The validation process is a key element when it comes to utilizing a simulation method. If the model was not validates, the results could not be validated as well.

The errors in simulation tools are related to the users input. i.e. weather data.

The limitations of this method include the assessments of aspects such as social and users behavior which are best approached in the survey method.

Energy modeling and building simulation has become a widely popular and reliable tool used by researcher and designers in the past few decades. Designers tend to use such tools prior to building construction to ensure a highly efficient building performance. On the other hand, researches utilize these tools in conducting studies and investigations on the built environment in timely manner, minimal human and financial resources. Building

simulation has proven to be reliable research method with several software packages available both on commercial and academic scales. Building simulation software are capable of conducting CFD analysis, thermal modeling, energy simulation, daylight analysis, and many other parameters. Software such as Energy Plus (Ruiz & Romero 2011, Fumo et al. 2010), DOE-2 (Akbari & Konopacki 2005, Cho & Haberl 2010, Lam et al. 2010), eQUEST (Ke et al. 2013), EOTECT (Raia et al. 2011, Saadah & AbuHijleh 2010), IES Virtual Environment (Azhar et al. 2010, Al-Masri & Abu-Hijleh 2012, AlNaqabi 2012, Alawadi 2013) have been utilized for researches to assess energy consumption and thermal comfort.

Moreover, some researches were conducted on simulation tools specifically developed for the academic research, or for specific purposes. Examples of such tools were used by Philip & Chow (2007), who used PRISM CO simulation tool for cooling and heating load estimations, and used TRACE 600 for energy simulation. However, Gugliermetti & Bisegna (2007) used TMY, and WINDOWS 4.1 for thermal simulation but were not validated but only referred to previous papers who used same tools. IENUS a research-only energy simulation tool was utilized, and was validated through comparison with the results of a small office building with same Mediterranean climatic conditions.

Another research by Ruiz & Romero (2011) used Energy Plus TM tool for thermal simulation, that was developed by the US Department of Energy. Also employed LIDERIT software tool for assessing compliance with the Codigo Technico de La Edification regulations. Another tool that was employed for assessing environmental impact of the modified model vs. the original model is CALENDER.

3.2.4 FIELD MONITORING APPROACH

Field monitoring approach is a type of observational research method (Research Methodology c. 2005). Typically, the study is directly related to the actual physical environment where the variables are measured through adequate instruments, and then extract the recorded data for analysis.

In this study, field monitoring approach could be applied to monitor several variables within the existing buildings. This includes measurements of Lux levels, thermal heat gain of the building elements, and other variables needed for the study. The field monitoring approach requires field measurement equipment, human
resources, and a well-designed methodology to where and when the field measurements are taken and the existing building is monitored.

Many researchers use this approach to explore the existing conditions and then study the impact of a specific independent variable after implementation such as the study undertaken by Flores et al (2008) where two physical buildings were monitored including an original building, and another modified design.

Limitations of this approach are reflected through the time constraints limiting the study, as well as the requirements for various field measurement equipment that would offset the cost of the study to higher levels as more detailed data is required.

Also, it has to be noted that within the context of this study, the passive strategies will have to be implemented in order to be tested. Therefore the application of this approach is deemed incompatible for this study.

3.2.5 EXPERIMENTAL FIELD RESEARCH

The experimental research method is best used for studying thermal comfort levels for existing buildings when discussing parameters such as dry-bulb temperature, humidity levels, daylighting. The calibration of the measurement tools is a critical issue, unfortunately none of the papers discussed have mentioned the equipment calibration process, instead have mentioned the types of equipment, and their specific location and function.

The field measurement method is found appropriate only when the study is considering certain parameters as mentioned previously, and when the time of the study is not limited. It has to be noted that the equipment might be expensive which adds to the research project costs.

It has to be noted here that none of the papers discussed under this group had employed the field measurement method as the only research method employed. The results were usually compared to questionnaire survey results, or results obtained through simulation tools.

3.2.6 LITERETURE REVIEW APPROACH

Literature review approach is typically used as a research method when extensive database of previous studies have been conducted on a specific topic. Basically, the new study reviews the existing data available through previous researches, and applies analytical studies to explore a proposed problem of a study.

In this study, the previous studies in the same field in UAE are limited. Therefore the literature review approach could be applied only through comparing the proposed problem to other studies conducted in the same region with similar climatic conditions stating the similarities and limitations of the study, in other words a case study approach. This usually gives indicative figures to how much passive techniques are able or not to reduce energy consumption in existing buildings.

3.2.7 MATHMATICAL CALCULATION APPROACH

The mathematical calculation research method is heavily dependent on other supporting methods for data collection which is basically utilized in the mathematical analysis of the problem. Therefore, the validation of the results are usually more complicated, and might require other methodologies for validation, such as field measurements, case studies, or comparison with literature review.

There are several mathematical analysis methods including linear and non-linear calculations. The greater the number of parameters considered, the more complexity levels are present in applying the mathematical method. An example of the level of complexity is found in the study conducted by Saidur (2009) where a multi-objective optimization model was developed and had to utilize programming softwares to present the results. This method has also been utilized by Ehsan *et* al (2012) and Ibrahim (2002) supported by other research methods. However, the calculation method is useful to employ this methodology for economical and feasibility studies.

3.3 PREFERRED RESEARCH METHOD

Having briefly discussed alternative research approaches above, and through further assessment and understanding of the pros and cons of each method, the preference has been given to the modeling approach to conduct this particular study. This judgment has taken into consideration the limitations in the research timeframe, the human resources required, the instruments/ equipment needed to conduct the research and other aspects such as cost of the study.

Computer modeling is a time efficient research method, it allows the researcher to study multi dependent and independent factors, and it is most suitable to compare several energy saving strategies prior to implementation for the specific context, geographic location, and climatic characteristics of a building–unlike the measurement field method.

Following is a brief of each of the limitations considered during the process of the research method selection for this study.

3.3.1 RESEARCH TIME DURATION

Among the research methods highlighted earlier, the literature review would require the minimal timing since no experiments are required and that it is purely based on previous studies. Second least time consuming is the modeling approach since it requires more time modeling the sample buildings and performing the simulation, as well as the time required for training to learn the energy simulation software selected for the study. Similarly, the laboratory approach will require more time to structure and prepare the experiment, and will require more observation time throughout the study. Moreover, the field monitoring approach will consume the longest time duration since the study aims to study the existing buildings all year round including summer and winter energy consumption, and peak times. Therefore, a minimum estimate for collecting this data will be minimum one year.

3.3.2 RESARCH RESOURCES

Here again literature review will only require the efforts of the researcher himself/herself, while extensive database of previous studies required to be available. Similarly, the modeling approach will require the same human resources, but more research facilities such as an IT Lab, and energy simulation software.

On the other hand, both the laboratory and the field measurements approaches will require additional resources including research assistants, research instruments and equipment. And in the case of laboratory approach, there should be a physical research facility available to conduct the experiment.

3.3.3 FINANCIAL COSTS

With regard to the overall cost of the research, the least research expenses will be where less research resources are required. Therefore literature review approach will not require high financial costs, whereas modeling approach will require additional costs of the simulation software and training. Higher costs are estimated for both laboratory and field monitoring approaches due to additional human resources, and research instruments requirements.

3.3.4 MODELLING APPROACH SELECTION

Having mentioned the above factors, it is noted that although literature review approach is the most efficient in time, cost, and resources it will be insufficient for this study due to technical data requirements and limited previous studies conducted in UAE in this field.

Also, it is noted that the laboratory approach requires high research resources, time duration, and financial costs. In addition, it is not a common research method in this field.

Field measurements approach is one of the research methods best applicable to this type of study, it will provide sufficient technical data, but will require more time and cost compared to the modeling approach. Therefore, the field monitoring approach has been eliminated for this particular study.

The modeling approach is deemed sufficient for this study since it is considered feasible in time, cost, and resources requirements. Moreover, it provides the tools necessary to study the interdependent relation between many variables at the same time, which is critical in this study that requires assessment of alternative scenarios of passive design retrofitting techniques prior to implementation.

3.4 SELECTION OF SIMULATION TOOL

There are several building modeling softwares available that could be employed for this study. Many available softwares have been verified by different agencies and have the capability to perform highly accurate energy simulation of the model.

Those softwares could be grouped into two categories;

- a whole building energy simulation, which analyze the total energy consumption of the building; and
- a detailed simulation tool, which considers a particular aspect of the building such as thermal bridging, natural ventilation, etc. (Hirsch et al 2011)

For the purpose of this study a detailed energy simulation is required to identify the potential of energy savings due to integrating passive retrofitting techniques.

A research conducted by Crawley *et* al (2005) analyzed twenty simulation softwares, their capabilities in thermal modeling, CFD analysis, solar insulation, building envelope, and other capabilities. The compared simulation softwares included BLAST, BSim, DeST, DOE-2.1E, ECOTECT, Ener-Win, Energy Express, Energy-10, EnergyPlus, eQUEST, ESP-r, HAP, HEED, IDA ICE, IES <VE>, PowerDomus, SUNREL, Tas, TRACE, and TRNSYS.

The research stipulated the pros and cons of each of the computer modeling softwares. Appendix A includes an extract of the summary comparison of the 20 computer modeling softwares (Tables A3 - A7). The tables indicated that IES VE, EnergyPlus, and TRANSYS tools are capable of conducting most of the solar analysis and insolation analysis requirements. However, for advanced fenestration analysis, other software tools are deemed sufficient such as IDA ICE.

For this study, building envelope calculations is considered critical. The study highlighted that calculations for outside surface convection were based on ASHRAE requirements in the case of IES VE software. It also highlighted that IES VE is the only software that is capable of conducting general building envelope calculations related to inside radiation view factors, radiation-to-air component separate from the exterior detailed convection, and air emissivity/ radiation coupling.

However, other studies have utilized other computer modeling tools. As highlighted earlier, Gugliermetti & Bisegna (2007) has conducted a study using a research-only software (IENUS) as a main tool for energy

simulation. Although the study has mentioned that the software allowed for adjustments to include several parameters, the author did not validate the model employed for his study.

Another study conducted by Ruiz & Romero (2011), successfully estimated the energy savings through Energy Plus. However, it was not clear what were the heating and cooling systems used in the conventional design studied, and whether parameters such as infiltration has been considered through the building thermal simulation.

A more complex study conducted by Akbari &Konopacki (2005) analyzed data which included both statistical analysis and energy simulation. The paper discussed the data collected and the parameters that were used as an input for the simulation tool. The data did not only include the building characteristics, but it also included the weather data. A clear classification of the climatic zones were identified and discussed as it was utilized throughout the study to obtain the results.

Since this paper is a continuation of previous studies by the same authors, the verification of the DOE-2 simulation tool has been referenced to their previous work. And the methodology is also validated by referencing to the project of the US Environmental Policy Act (EPA) which is the Urban Heat Island Pilot Project (UHIPP).

Another study has utilized several software tools. A study conducted by Philip & Chow (2007), highlighted in the previous chapter, have used the simulation through PRISM CO which utilized data from energy audit. The PRISM CO model, and even the further developed models mostly were used for a single variable/ parameter. The models ignored the electricity consumption used for lighting. With regard to the energy simulation software TRACE600, few variables were still under the uncertainty zone such as people load.

For this study, IES VE has been used as an energy modeling tool to assess energy savings and reductions in cooling loads for the building prototype. In a comparison with 20 commonly used energy simulation software, IES VE provided various interlinked parameters and assessment options including building envelope, daylight and solar variables which are important for this study (Crawley *et* al. 2008). IES has proven high reliability and accuracy of its results with advanced features.

3.5 IES VIRTUAL ENVIRONMENTN SOFTWARE VALIDATION

As highlighted previously, many researchers have been using IES VE for energy simulation and thermal modeling. The software, which was compared with another 19 computer modeling tools was proven to be of high capabilities and reliability, especially for this type of research and analysis. (Crawley *et al.* 2008). This simulation software has also been used for the previous research project, of which this study is a continuation for. The study has assessed energy consumption of five housing typologies and analyzed annual cooling load savings through IES VE 6.4. (AlNaqabi *et al.*, 2012 and Alawadi *et al.*, 2013).

It is important through to validate the software within the context of the study. A study conducted by AlNaqabi (2013) have validated the software by modeling an existing villa as a case study and comparing the results with the actual total energy consumption. The researcher has also contributed to the previous study (AlNaqabi *et* al. 2012) which adopted IES software for the research.

The software validation case study was selected from the Emirate of Sharjah, and is presented in the following Table 7 and Figure 14 below. The IES model indicated similar trend in total monthly energy consumption, with minor deviations in the monthly energy consumption for the months from May to August. AlNaqabi (2013) explained that the deviation is justified due to the building typology which is a school, in which the occupancy profile varies in the summer months due to minimal occupancy of the building facilities where students are mostly off during Summer.

| Fable 7 Validation | model results. | (AlNaqabi | (2013), pp. (| 50) |
|---------------------------|----------------|-----------|---------------|-------------|
|---------------------------|----------------|-----------|---------------|-------------|

| Month | Actual | Simulated |
|-----------|--------------------|--------------------|
| | Energy Consumption | Energy Consumption |
| | (MWh) | (MWh) |
| January | 4.29 | 2.63 |
| February | 4.22 | 4.10 |
| March | 6.74 | 6.33 |
| April | 7.24 | 10.07 |
| May | 12.56 | 14.78 |
| June | 11.82 | 16.67 |
| July | 18.34 | 18.97 |
| August | 14.71 | 19.28 |
| September | 16.74 | 16.70 |
| October | 12.49 | 12.92 |
| November | 9.80 | 7.99 |
| December | 7.22 | 3.93 |



Figure 14 Comparison of tested villa actual and simulated energy consumption. AlNaqabi (2013), pp. 60)

As a conclusion of the validation case study an average annual energy consumption deviation of 6% from the actual results was identified. However, the deviation is much less for the months where the building is fully occupied.

3.6 SUMMARY RESEARCH METHODOLOGY

The research methodology which best applies to this particular study is the modeling approach, in which data collected will be analyzed through a quantitative, qualitative, and graphical quantitative analysis, as well as interpretations of interviews and observations.

3.6.1 LITERATURE REVIEW, DATA COLLECTION AND ANALYSIS

The study requires investigation to identify the existing building typologies which represents the total stock of buildings in Abu Dhabi Metropolitan. The data collected should reflect the total number of buildings in each category as well as building Gross Floor Area (GFA). The data collected should be analyzed to identify the common design and construction building typology of commercial buildings in 1980s and 1990s. An understanding of existing and previous building regulations is also essential.

The data collected is presented within the literature review section of this study, and further analysis will be curried on in relevant chapters as required.

3.6.2 BUILDING MODELING AND SIMULATION

The study will conduct two sets of building simulation using IES Virtual Environment 6.4 software;

- The first set will model and analyze the existing buildings as they are currently with no modifications
- The second set will model and analyze the modified buildings assessing the various proposed passive retrofitting techniques by conducting several simulation runs independently.

The following passive retrofitting techniques will be explored:

- Thermal insulation for external walls
- Thermal insulation for roof
- Glazing materials for external openings

The following parameters will be assessed using the software;

- Room cooling plant sensible load

- Chiller energy
- Auxiliary chiller energy
- Heat rejection fan/ pump energy
- Total system energy
- Total equipment energy
- Total energy
- Sensible heat balance
- Sensible internal gains breakdown
- Total Carbon emissions

The details of the simulation models and scenarios will be further discussed in the following chapter.

3.6.3 SIMPLE PAYBACK PERIOD COST ANALYSIS AND STATISTICAL ANALYSIS

A simple payback period cost analysis will be conducted to assess the financial feasibility of the building refurbishment process. The analysis will be conducted based on simple payback period, similar to what have been implemented in the previous research project conducted by AlNaqabi *et* al (2012) and Alawadi *et* al (2013). The analysis will be based on market based prices of the proposed retrofitting applications.

3.6.4 ANALYSIS METHOD

- Analysis of data collected regarding stock of existing buildings in Abu Dhabi Metropolitan to identify two case studies representing commercial buildings in 1980s and 1990s.
- Analysis and assessment of energy savings of refurbishment strategies for the selected case studies in comparison with the baseline as built model.
- Cost analysis of retrofitting strategies and comparing energy savings achieved with reference to expenses.

The following Chapter identifies the simulation models, scenarios, input parameters, and output parameters addressed in the study.

CHAPTER 4: SIMULATION MODELS

4 SIMULATION MODELS

4.1 INTRODUCTION

In order to initiate the computer modeling and simulation for the studied case, it is important to identify the simulation scenarios, simulation input data, and any associated assumptions. Since the research addresses building typologies from earlier decades, it is deemed necessary to understand the simulation input parameters to reflect the exact conditions and not using the software default values and assumptions.

The research targets to conduct energy simulation and thermal modeling for 9 simulation models including the baseline model, and 8 refurbished building scenarios. The first section explains the parameters of the case study, followed by an explanation of the general input data for the baseline model. Then the chapter presents the simulation input for the 8 refurbishment scenarios besides the trial scenarios explanation. The chapter also presents a summary of the simulation variables which concludes the simulation input parameters to be assessed through the computer modeling and simulation for the 9 scenarios.

4.2 THE CASE STUDY

The case study building is a mixed-use building typology located in Abu Dhabi in Electra Street. The building is located on a 50 x 80 square feet plot. The building represents a typical prototype of the 1980s in Abu Dhabi. It is a concrete structure building, single glazed, with no walls insulation. The building consists of 15 typical floors each of 3.4 meters height, and a mezzanine and ground floor building with a total height of 7.4 meters. Figure 15 is a photo of the case study building.

The building is designed as a mixed-use building following the norms in Abu Dhabi during the time of design and construction. The typical floor was designed to either be utilized for office spaces or accommodate a four two bedrooms residential units. However, the ground floor has been allocated for retail-office spaces, and the mezzanine was allocated for office spaces.



Figure 15 Real time case study building photo.

4.2.1 TYPICAL FLOOR

The typical floor covers an area of 447.1 square meters. The external walls surface area is 289.68 square meters, and a net external glazing area of 93.84 square meters. The following Figure 16 and Figure 17 are extracted from the simulation model of the typical floor which represents the typical floor plan and an external perspective image of the model.

4.2.2 MEZZANINE FLOOR

The mezzanine floor covers an area of 344.1 square meters. The external walls surface area is 269 square meters, and a net external glazing area of 73.68 square meters. The following Figure 16, Figure 17 and Figure 18 are extracted from the simulation model which represents the mezzanine floor plan and an external perspective image of the model.

4.2.3 GROUND FLOOR

The ground floor covers an area of 344.1 square meters. The external walls surface area is 132.64 square meters, and a net external glazing area of 270.56 square meters. Figure 16, Figure 17 and Figure 18 are extracted from the simulation model of the ground floor which represents the floor plan and an external perspective image of the model.



Figure 16 Typical floor plans of the IES-VE model.



Figure 17 Typical floor three dimensional image of the IES-VE model.



Figure 18 Three dimensional image of the IES-VE model for ground and mezzanine floor.

4.3 BASELINE MODEL INPUT

4.3.1 GEOGRAPHICAL LOCATION AND WEATHER DATA

The case study building is located in Abu Dhabi City in Electra Street. The building is oriented approximately 45 degrees East-North. In order to set the weather data file and geographic setting of the building, the computer model used the IES-VE tool of APLocate. Thorough this tool, the identified location data was linked to the the software built-in data related to Abu Dhabi Intl Airport, United Arab Emirates. Daylight adjustments have been set to zero. Following are the location data and site data input used for APLocate tool;

Location Data:

- Longitude: 54.65° E
- Latitude: 24.43° N
- Altitude: 27m meters above sea level
- Time Zone (hours ahead of GMT): 4 hours

Site Data

- Ground reflectance: 0.20
- Terrain Type: City
- Wind exposure (CIBSE heating loads): Normal

4.3.2 ABU DHABI'S CLIMATIC CONDITIONS

The United Arab Emirates is characterized by its hot arid desert climatic, whereas the main characteristics are known to be the high temperature, and the low rainfall levels (The UAE National Media Council. 2010). The outside maximum dry bulb temperature can reach to 46.5°C. The weather data design file is based on ASHRAE Standards; however, the weather data file selected was AbuDhabiIWEC.fwt which is generated by IES-VE. The following Table 8 provides more details of the assumption. The table is a generated report from the baseline model.

Table 8 Location and Site Data. (Source: IES-VE APLocate)

Location & Site Data

| Location | Abu Dhabi Intl Airport |
|--|------------------------|
| Region | United Arab Emirates |
| Latitude | 24.43 N |
| Longitude | 54.65 E |
| Altitude | 27.0m |
| Time zone | 4.0 hours |
| Hours ahead of GMT | |
| Daylight Saving Time | |
| Time adjustment | 0.0 hours |
| From | |
| Through | |
| Adjustment for other months | 0.0 hours |
| Site Data | |
| Ground reflectance | 0.2 |
| Terrain type | City |
| Wind exposure | Normal |
| (CIBSE Heating Loads) | |
| | |
| Weather Simulation Data | |
| ApacheSim File | AbuDhabilWEC.fwt |
| · | |
| | |

Design Weather Data

| Design Weather Data Source & Statistics | |
|---|--|
| Source of Design Weather ASH | RAE design weather database |
| ASHRAE weather location Abu | Dhabi Intl Airport, United Arab Emirates |
| Monthly percentile for Heating Loads design weather 99.6 | % |
| Monthly percentile for Cooling Loads design weather 0.4 9 | , 0 |
| Heating Loads Weather Data | |
| Outdoor Winter Design Temperature 11.5 | C |
| Cooling Loads Weather Data | |
| Max. Outside Dry-Bulb 46.5 | C |
| Max. Outside Wet-Bulb 23.6 | C |

Weather model data

| | Tempe | Humidity | Solar | |
|-----|----------------|-------------------------------|-------|------------------------------|
| | Dry bulb T Min | Dry bulb T Min Dry bulb T Max | | Linke Turbidity Factor |
| | (°C) | (°C) | (°C) | |
| Jan | 19.50 | 29.50 | 18.00 | 2.31 |
| Feb | 23.40 | 33.80 | 17.80 | 2.37 |
| Mar | 26.70 | 38.00 | 18.90 | 2.56 |
| Apr | 28.60 | 41.80 | 20.30 | 2.85 |
| May | 29.60 | 44.10 | 21.10 | 3.06 |
| Jun | 31.00 | 45.20 | 21.90 | 3.22 |
| Jul | 33.80 | 46.10 | 23.60 | 3.29 |
| Aug | 34.00 | 46.50 | 23.30 | 3.13 |
| Sep | 30.40 | 43.10 | 23.10 | 2.84 |
| Oct | 30.20 | 43.10 | 21.60 | 2.65 |
| Nov | 23.50 | 35.00 | 19.80 | 2.44 |
| Dec | 20.70 | 31.20 | 18.80 | 2.38 |

4.3.3 THERMAL CONDITIONS

This section stipulates the simulation input and assumptions used to generate the thermal properties of the baseline model. It has to be noted that many of the parameters deviate from the default software tools settings due to the nature of the project as an old dated building design and systems.

4.3.3.1 ROOM CONDITIONS

All rooms are set to the same profile as following;

- Heating: heating profile is set off continuously
- District Hot Water System (DHW): is set to zero consumption
- Cooling: Cooling profile is set working between 8:00am to 6:00pm with constant profile. The cooling set point is set to 23 °C based on comfort zone set by ASHRAE. UCLA Energy Design Tools Group (2011).
- Plant Auxiliary System: the auxiliary system is set on between 8:00am to 6:00pm
- Model Setting: model settings are set to defaults; with solar reflected fraction of 0.05, and furniture mass factor of 1
- Humidity Control: humidity is set within 30% to 70% relative humidity based on thermal comfort guidelines of ASHRAE. UCLA Energy Design Tools Group (2011).

4.3.3.2 SYSTEM

The main system utilized is a cooling only system, where low efficient air conditioning systems were used. The COP was assumed to be 2.2 based on the ASHRAE 90-1975 effective in 1980.

4.3.3.3 INTERNAL GAINS

The building zoning was divided into five zones based on functionality and relevant thermal conditions. The detailed report of the thermal conditions input of all zones has been generated through IES-VE tools and is provided in Appendix C, Table C1.

 Corridor: Corridor internal gains include Fluorescent lighting is assigned to maximum power consumption of 13W/m2

- Kitchen: Kitchen internal gains include Fluorescent lighting is assigned to maximum power consumption of 9W/m2, and cooking assigned to maximum power consumption of 10W/m2
- Lobby: internal gains include Fluorescent lighting is assigned to maximum power consumption of 12W/m2, and miscellaneous lift assigned to a maximum power consumption of 5W/m2. Based on Abu Dhabi building code which was in use in 1980s, Article (55) regarding provision of elevators states that for buildings over 15 storeys minimum three elevators should be provided of minimum capacity of 6 people each (ADM 1983). However the estimated consumption of 5W/m2 is assigned to the maximum power consumption in the simulation model based on the KONE energy calculator (KONE 2013).
- Office: Office internal gains include computers set at 20W/m2 for maximum sensible gain and maximum power consumption, and is set to a profile from 8:00am to 6:00pm.

The default setting is also similar to what has been used in a study conducted by Hammad & Abu-Hijleh (2010) which is conducted for a typical office space in Abu Dhabi. The study assumed occupancy of two computer desks per 32 square meters, where the computer uses 370W. When the same is calculated based on the total office area of the simulated building the average power consumption for computers would be 22W/m2 which is close to the default setting.

Use of fluorescent lighting was selected for internal heat gain based on illuminance level of 500 lux for office spaces based on IESNA requirements (Block 2000), accordingly maximum power consumption is assumed 11W/m2.

For people occupancy, the assumption is to dedicate 12 square meters per person. Although the average office space in Abu Dhabi as per UPC (2010b) was 1.9 square meters per person, this is not considered a representative ratio for this type of buildings, since the building prototype is typically designed for either residential or office uses. According to Hammad & Abu-Hijleh (2010), a typical office space in Abu Dhabi provides 16 square meters per person. However, based on the layout of this building an average of 36 people could be accommodated, therefore the habitable space dedicate to each person is around 12 square meters. Based on these assumptions, the occupancy density for the building simulation is assigned to 12 m2/person with maximum sensible gain of 90W/person, and latent sensible gain of 60/person.

 Washroom: washroom internal gains include fluorescent lighting set at 9 W/m2 for maximum sensible gain and maximum power consumption.

4.3.3.4 AIR EXCHANGES

- All rooms are set to an infiltration rate of 0.25 air change per hour.
- Auxiliary ventilation is set to a maximum of 2 air change per hour, and a variation profile set from 8:00 am to 6:00pm.

4.4 SIMULATION MODELS

4.4.1 TEST SIMULATION MODELS

Prior to starting the final simulation of the studied scenarios, and due to complexity of the simulation for highrise building model, it is necessary to run test simulations to minimize modeling errors to minimal. Therefore, the author conducted several test simulations on a typical floor of the studied building. The test model was tested to identify the following parameters are within the expected range;

4.4.1.1 AIR TEMPURATRE

The model thermal conditions for cooling set point was defined as 23° C and the cooling profile is set to a daily profile from 8:00 am to 6:00 pm. Therefore, a successful simulation model shall reflect a flat line of 23°C where the cooling system is operational. Figure 19 present the output of annual air temperature profile in one sample room within the typical floor. As noticed in the figure, the air temperature profile is responsive to the outdoor air temperature profile where the cooling is off, and is represented in a constant formula –flat line- where the cooling is operational.



Figure 19 Annual air temperature profile for room identified Living-01. (IES VE Tool)

4.4.1.2 RELATIVE HUMIDITY

The relative humidity has been set within the recommended range as per ASHRAE thermal comfort parameters which are in the range between 30% and 70%. Figure 20 present the output of annual relative humidity profile in one sample room within the typical floor. The figure highlights that the annual relative humidity profile is responsive to the limits set for relative humidity with maximum value of 70% and minimum value of 30%. Where the cooling system is off –outside the occupancy profile settings- the relative humidity profile represents the actual outdoor conditions.



Figure 20 Annual relative humidity profile for room identified Living-01. (IES VE Tool)

4.4.1.3 ROOM CO2 CONCENTRATION

An important indication of whether the modeling is representatives of the as-built conditions, is the room CO2 concentration. CO2 concentration is one parameter that indicates a habitable space and is directly linked to the cooling loads. High room CO2 concentration could be identified where reductions in cooling loads beyond the actual conditions occur. According to ASHRAE the room CO2 concentration shall be less than 1000 ppm. Figure 21 present the output of annual room CO2 concentration profile in one sample room within the typical

floor. The figure highlights that the maximum CO2 concentration level is around 595 ppm where the cooling is off. However, it is further reduced to around 360 ppm when the cooling system is operational.



Figure 21 Annual room CO2 concentration profile for room identified Living-01. (IES VE Tool)

4.4.1.4 COOLING PLANT SENSIBLE LOAD

Similar to the air temperature profile, the annual cooling plant sensible load is an indication of the model behavior compared to the actual conditions. Since the cooling system is set to a daily profile from 8:00 am to 6:00 pm; the simulation results shall reflect the same. Figure 22 present the output of annual cooling plant sensible load profile in one sample room within the typical floor. The figure highlights that the annual cooling load profile is responsive to the outdoor conditions; i.e. during the Summer months, the cooling load is at peak, where it is reduced during Winter Months. Also, it is noticed that the cooling load is zero when the cooling system is off.



Figure 22 Annual cooling plant sensible loads profile for room identified Living-01. (IES VE Tool)

4.4.1.5 THERMAL ZONING

Moreover, a trial simulation was conducted for the typical floor with the internal partitions, and without the internal partitions. The comparison of sensible cooling loads for both models is used to identify whether the internal zoning will have impact on the study. Based on this comparison, the final model for the overall structure is defined. Figure 23 indicates the typical floor models as-built, and with connected spaces. The model to the left defines the rooms as different zones, which typically consumes more time for analysis. To the right, a modified model has considered the IES ModelIT function to connect spaces. The function was used for the office spaces only, and was selected with removal of partitions.



Figure 23 Typical plan IES model. To the left is the model as-built conditions, to the right is the model with connected spaces.

The results highlighted an overall difference of 5% on the total room cooling sensible load. The differences range from 3.4% to 5.2% on the monthly cooling loads. Table 9 stipulates the monthly and yearly room cooling plant sensible loads in MWh for the typical floor based on a simulation model for the as-built conditions of separate spaces, and a simulated model with connected spaces for office spaces. Figure 24 summarizes the difference in cooling load profile of the two models graphically. It is noticed that the difference during the Summer from May to September witness the greatest deviation in the results.

Based on the comparison highlighted above, the author decided to simulate the building on the basis of as-built conditions to minimize the modeling errors.

 Table 9 Comparison on room cooling plant sensible loads between connected spaces model and as built model.

Room cooling plant sens. load (MWh)

| Date | Typical Floor as built | Typical Floor with connected spaces |
|--------------|------------------------|-------------------------------------|
| Jan 01-31 | 0.9059 | 0.8651 |
| Feb 01-28 | 1.8522 | 1.7698 |
| Mar 01-31 | 4.8052 | 4.5588 |
| Apr 01-30 | 9.6783 | 9.1826 |
| May 01-31 | 14.0266 | 13.314 |
| Jun 01-30 | 17.2003 | 16.3085 |
| Jul 01-31 | 18.6062 | 17.694 |
| Aug 01-31 | 19.5397 | 18.5494 |
| Sep 01-30 | 16.8354 | 15.961 |
| Oct 01-31 | 11.9635 | 11.3382 |
| Nov 01-30 | 7.5186 | 7.1125 |
| Dec 01-31 | 2.5366 | 2.3937 |
| Summed total | 125.4686 | 119.0477 |



Figure 24 Typical floor space zoning comparison.

4.4.2 SIMULATION SCENARIOS

The simulations scenarios are set to analyze the thermal parameters of the building envelope, and the impact of the upgrades for the external wall insulation, roof insulation, and external glazing. This research will use the minimum requirements for the 1 pearl rating for the building envelope upgrades, that will be based on the requirements stipulated under the Estidama U-value calculator for the 1 pearl rating and 2-5 pearl rating. Where the 2-5 pearl rating standards are used, the research will refer to the standards as 2 pearl scenario.

The first set of simulation is the baseline scenario for the as-built conditions. The second set targets the thermal insulation upgrades for the external walls to the requirements of the Abu Dhabi Urban Planning Council Estidama requirements as stipulated in the Pearl Rating System set for Abu Dhabi. This set includes two scenarios; the first is the upgrade to 1 Pearl rating with the requirements for wall U-value of 0.32 (W/m2.K), the second is for 2Pearls rating with the requirements of 0.29 (W/m2.K).

The third set consists of two scenarios for upgrades of glazing properties to 1 Pearls rating requirement for glazing U-value of 2.2 (W/m2.K) and glazing SHGC value of 0.4. The second scenario improves the performance for 2 Pearl rating to 1.9 (W/m2.K) and 0.3 respectively.

The fourth set consists of upgrades of the roof thermal insulation in two scenarios similar to the above. The 1 pearl rating scenario requires roof u-value of 0.14 (W/m2.K), whereas the second scenario for 2 pearl rating requires roof u-value of 0.12 (W/m2.K).

The fifth and final set of model is a scenario of all combined solutions of 1 pearl, and 2- pearls requirements. Table 10 provides a summary of the minimum requirements in compliance with 1 Pearl rating, and the advanced requirements to achieve the optional credit 2 Pearls (Abu Dhabi Urban Planning Council 2010). Table 10 Summary of thermal performance requirements in compliance with 1 pearl & 2-5 pearls rating.

| Element | Baseline Model | 1 Pearl RE-R1 Required Target Value | | 2-5 Pe RE-2 (| arls Optional Target Value |
|-----------------------|----------------|---|---------------------|------------------|-------------------------------|
| Infiltration | 2.000 ach | 0.350 | ach | 0.200 | ach |
| Wall (U-value) | 1.600 W/m2.K | 0.320 | W/m ² .K | 0.290 | W/m ² .K |
| Floor (U-value) | 0.25 W/m2.K | 0.150 | W/m ² .K | 0.140 | W/m ² .K |
| Roof (U-value) | 0.505 W/m2.K | 0.140 | W/m ² .K | 0.120 | W/m ² .K |
| Glazing (U- value) | 5.811 W/m2.K | 2.200 | W/m ² .K | 1.900 | W/m ² .K |
| Glazing (SHGC) | 81 % | 40 | % | 30 | % |

Table 11 summarizes the scenarios based on different simulation input variables which were used for the case study. For easy comparison the table uses two different symbols for the baseline and the modified parameter. The symbol O is used where the baseline value is used, and the symbol X is used where an upgrade is proposed and evaluated.

| Scenario | | | Baseline | Wall | Wall | Glazing | Glazing | Roof | Roof | Combined | Combined |
|-----------|---------------------|-------------|----------|------------|---------------|---------|---------------|------------|---------------|----------|------------|
| Variables | U-value (W/m2.K) | SHGC (%) | Model | 1 Pearl | 2-5 Pearls | 1 Pearl | 2-5 Pearls | 1 Pearl | 2-5 Pearls | 1 Pearl | 2-5 Pearls |
| External | Baseline | n.a. | 0 | - | - | 0 | 0 | 0 | 0 | - | - |
| Walls | 0.320 | n.a. | - | Х | - | - | - | - | - | Х | - |
| | 0.290 | n.a. | - | - | Х | - | - | - | - | - | Х |
| Glazing | Baseline | Baseline | 0 | 0 | 0 | - | - | 0 | 0 | - | - |
| | 2.200 | 0.4 | - | - | - | Х | - | - | - | Х | - |
| | 1.900 | 0.3 | - | - | - | - | Х | - | - | - | Х |
| Roof | Baseline | n.a. | 0 | 0 | 0 | 0 | 0 | - | - | - | - |
| | 0.140 | n.a. | - | - | - | - | - | Х | - | Х | - |
| | 0.120 | n.a. | - | - | - | - | - | - | Х | - | Х |

Table 11 Summary of IES model simulation input variables

Notes:

O: the baseline value is applied

X : an upgrade is applied

n.a.: not applicable

4.5 SIMULATION PROCESS

The case study building consists of a total 17 floors with 15 typical floors, mezzanine and ground floors. Therefore, the simulation processing through IES-VE is likely to be interrupted by model complexity and its requirements for advanced IT systems. In order to minimize any unwanted IT related errors and delays, the researcher decided to split the simulation into three different models.

The simulation process begins with identifying the breakdown of the building structure for easy analysis and arrangement of the results. The building has been divided into three models as following;

- Typical floor simulation model
- Ground floor and mezzanine floor simulation model
- Roof floor simulation model

The simulation and the study will be conducted separately for each of the models. For each of the models the 8 scenarios will be generated, as described in the earlier section. A total of 23 simulations shall be conducted inclusive of;

- 7 simulations for the typical floor model
- 7 simulations for the ground and mezzanine floors model
- 9 simulations for the roof floor model

All results from the models will be presented statistically and imported into a table form using MS Office – Excel program. The results from the typical floor model will be multiplied by 14 to represent the overall results for all typical floors except for the roof floor. The results will be added to the ground and mezzanine floors results as well as the roof floor model results.

Although the roof floor is represented architectural in the same manner as the typical floor, it has been identified as a separate IES model since the roof is exposed directly to the external atmosphere, which shall increase the solar gain and energy consumption for this floor in particular.

The final step shall be presenting the overall results for the whole structure in the coming sections of this paper.

CHAPTER 5: RESULTS AND DISCUSSION

5 RESULTS AND DISCUSSION

5.1 INTRODUCTION

This chapter will include the results of this research and discuss the savings that are achieved through various refurbishment strategies. This section will also discuss the economic feasibility of the proposed scenarios to nominate the most feasible option which achieves the greatest energy savings within an economically viable solution context. The study presented in this chapter will also evaluate the overall savings of the existing building stock in Abu Dhabi which is represented by the studies typology.

Comprehensive and critical analysis of the results is required to understand the potential of energy savings by employing thermal envelope upgrades. The results will be presented for the room cooling plant sensible loads, the system energy, the auxiliary system energy, the total electricity consumption. It is also essential to understand the sensible heat balance which includes the conduction gain in the external building envelope elements. It has to be noted that during the studies conducted for the previous research project –refer to Chapter 2- that the behavior of the cooling load profile and related energy savings when combined refurbishment solutions are employed, has to be explained through the elemental heat gain, and overall envelope sensible heat balance.

The chapter will first present the outcome of the refurbishment solutions for thermal insulation upgrades for external walls, followed by glazing upgrades, thermal insulation upgrades for the roof, and the combined refurbishment solutions. A discussion around the building envelope performance in terms of solar gain and external conduction gain will be presented to support and justify the results of combined versus individual refurbishment scenarios. The chapter will then provide an economic feasibility assessment section. The chapter will be concluded by assessing the potential of energy saving for the total GFA of the existing building stock in Abu Dhabi, which is represented by the case study.

5.2 EXTERNAL WALLS INSULATION REFURBISHMENT

The refurbishment application for the external walls of the building focuses on upgrading the thermal performance of the walls. Therefore, the refurbishment technique proposed is addition of thermal insulation.

There are two types of thermal insulation upgrades to the existing buildings, which are locally common. These include thermal insulation boards of different thicknesses, thermal properties, and material properties, and the application of a curtain wall which could be externally fixed to the existing structure.

This section will present and discuss the results of two different scenarios to upgrade the thermal performance of the external walls. The scenarios selected are the upgrades to U-value of 0.32 W/m2.K and 0.29 W/m2.K; which are based on the Estidama Pearl Rating System requirements for 1 pearl, and 2-5 pearls rating.

5.2.1 TYPICAL FLOOR

The results for the typical floor –presented in Table 12- indicated cooling loads savings of around 5.67% for the 1 pearl wall upgrade, and 5.80% for the 2 wall pearl upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 5.14% and 5.26% for the 1 pearl and 2 pearls scenarios respectively. The savings in the annual energy consumption were 3.54% and 3.63% for the 1 pearl scenarios and 2 pearl scenario respectively.

Annual reductions in electricity consumption for the 1 pearl wall upgrades is estimated at 3.752 MWeh/yr, and 3.840 MWeh/yr for the 2 pearls wall. Also, the annual reduction in CO2 emissions are estimated at 1,940 KgCO2 and 1,985 KgCO2 for the 1 pearl and 2 pearls upgrades respectively. CO2 emissions were estimated based on the IES Vista Analysis results of Total Carbon Emissions CE including carbon emissions from the building and its systems and based on type of fuel used to generate electricity in Abu Dhabi excluding any contribution from renewable energy.

For a monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.

| | | | Wall- 1 | | Wall-2 |
|---|-----------|-----------|---------|-----------|---------|
| | | | Pearl | | Pearl |
| | | Wall- 1 | Savings | Wall-2 | Savings |
| Output | Baseline | Pearl | (%) | Pearl | (%) |
| Room cooling plant sens. load (MWh) | 125.4686 | 118.3528 | 5.67% | 118.1854 | 5.80% |
| Chillers energy (MWh) | 56.1426 | 53.2564 | 5.14% | 53.1885 | 5.26% |
| Ap Sys chillers energy (MWh) | 56.1426 | 53.2564 | 5.14% | 53.1885 | 5.26% |
| Ap Sys heat rej fans/pumps energy (MWh) | 16.8428 | 15.9769 | 5.14% | 15.9566 | 5.26% |
| Total system energy (MWh) | 83.2134 | 79.4628 | 4.51% | 79.3745 | 4.61% |
| Total electricity (MWh) | 105.8156 | 102.0636 | 3.55% | 101.9753 | 3.63% |
| Total energy (MWh) | 105.897 | 102.1464 | 3.54% | 102.0581 | 3.63% |
| Total CO2 Emissions ((kgCO2) | 54,723.00 | 52,783.00 | 3.55% | 52,738.00 | 3.63% |

Table 12 Load, Energy and Carbon results of external wall upgrades for typical floor model.

It is noticed that the additional savings beyond the 1 pearl rating upgrades and minimal for external wall upgrades in the typical floor, with a range of 0.08% to 0.13%. Also, it is noticed that the overall savings in the case of 1 pearl upgrade from the baseline case is still modest. This is explained due to the fairly good thermal performance of the external wall section which is calculated to have a U-value of 1.6 W/m2.K. The construction of the external wall as-built, although has no thermal insulation application, it was designed with air gap between two high density concrete blocks. This explains the modest reductions in cooling loads, energy consumption, and CO2 emissions.

5.2.2 ROOF FLOOR

The results for the roof floor –presented in Table 13- indicated cooling loads savings of around 5.94% for the 1 pearl wall upgrade, and 6.09% for the 2 wall pearl upgrade. This is slightly greater than the results shown for the typical floor, and that is mainly due to the external building envelope in case of the roof floor includes the roof element which is almost three times of better insulation than the baseline wall section. This means that the overall building envelope in case of the roof floor. The results also indicate a reduction in annual chillers energy and related auxiliary chiller system and heat rejection system, estimated at 5.39% and 5.52% for the 1 pearl and 2 pearls scenarios respectively. The savings in the annual energy consumption were 3.73% and 3.82% for the 1 pearl scenarios and 2 pearl scenario respectively.

Annual reductions in electricity consumption for the 1 pearl wall upgrades is estimated at 3.9896 MWeh/yr, and 4.0848 MWeh/yr for the 2 pearls wall. Also, the annual reduction in CO2 emissions are estimated at 2,062 KgCO2 and 2,112 KgCO2 for the 1 pearl and 2 pearls upgrades respectively. For a monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.

| | | | Wall- 1 | | Wall-2 |
|---|-----------|-----------|---------|-----------|---------|
| | | | Pearl | | Pearl |
| | | Wall- 1 | Savings | Wall-2 | Savings |
| Output | Baseline | Pearl | (%) | Pearl | (%) |
| Room cooling plant sens. load (MWh) | 127.3355 | 119.7668 | 5.94% | 119.5863 | 6.09% |
| Chillers energy (MWh) | 56.8844 | 53.8155 | 5.39% | 53.7423 | 5.52% |
| Ap Sys chillers energy (MWh) | 56.8844 | 53.8155 | 5.39% | 53.7423 | 5.52% |
| Ap Sys heat rej fans/pumps energy (MWh) | 17.0653 | 16.1447 | 5.39% | 16.1227 | 5.52% |
| Total system energy (MWh) | 84.1811 | 80.1926 | 4.74% | 80.0975 | 4.85% |
| Total electricity (MWh) | 106.78 | 102.7904 | 3.74% | 102.6952 | 3.83% |
| Total energy (MWh) | 106.8647 | 102.8762 | 3.73% | 102.781 | 3.82% |
| Total CO2 Emissions ((kgCO2) | 55,222.00 | 53,160.00 | 3.73% | 53,110.00 | 3.82% |

 Table 13 Load, Energy and Carbon results of external wall upgrades for roof floor model.

Similar to the typical floor, the additional savings beyond the 1 pearl rating upgrade were minimal, estimated to be within a range of 0.09% to 0.14%. Generally, the savings in cooling loads, energy consumption, and CO2 emissions are greater than the typical floor, which has been explained earlier.

5.2.3 GROUND AND MEZZANINE FLOORS

The results for the ground and mezzanine floors –presented in Table 14- indicated cooling loads savings of around 3.88% for the 1 pearl wall upgrade, and 3.98% for the 2 wall pearl upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 3.58% and 3.67% for the 1 pearl and 2 pearls scenarios respectively. The savings in the annual energy consumption were 2.53% and 2.59% for the 1 pearl scenarios and 2 pearl scenario respectively.

Annual reductions in electricity consumption for the 1 pearl wall upgrades is estimated at 5.0284 MWeh/yr, and 5.1512 MWeh/yr for the 2- pearls wall. Also, the annual reduction in CO2 emissions are estimated at 2,600 KgCO2 and 2,663 KgCO2 for the 1 pearl and 2 pearls upgrades respectively. For a monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.

| | | | Wall- 1 Pearl | | Wall-2 Pearl |
|---|------------|------------------|------------------|-----------------|-----------------|
| Output | Basalina | Wall- 1 Poorl | Savings | Wall-2 Poorl | Savings |
| Room cooling plant sens. load (MWh) | 245.7228 | 236.1836 | 3.88% | 235.9506 | 3.98% |
| Chillers energy (MWh) | 107.9103 | 104.0423 | 3.58% | 103.9478 | 3.67% |
| Ap Sys chillers energy (MWh) | 107.9103 | 104.0423 | 3.58% | 103.9478 | 3.67% |
| Ap Sys heat rej fans/pumps energy (MWh) | 32.3731 | 31.2127 | 3.58% | 31.1843 | 3.67% |
| Total system energy (MWh) | 155.2918 | 150.2647 | 3.24% | 150.142 | 3.32% |
| Total electricity (MWh) | 198.4932 | 193.4648 | 2.53% | 193.342 | 2.60% |
| Total energy (MWh) | 198.6329 | 193.6059 | 2.53% | 193.4831 | 2.59% |
| Total CO2 Emissions ((kgCO2) | 102,649.00 | 100,049.00 | 2.53% | 99,986.00 | 2.59% |

Table 14 Load, Energy and Carbon results of external wall upgrades for GF and Mezz floor model.

The results indicate higher energy consumption for the ground and mezzanine floors compared to the typical and roof floors. That is due to the high ratio of glazing in the ground floor level which is used for retail and office spaces. The additional savings beyond the 1 pearl rating upgrades were minimal and even less than the previous two models for the typical and roof floors. The additional savings ranges between 0.06% and 0.09%.

5.2.4 ALL BUILDING

The results for the building consist of 14 typical floors, roof floor, and ground and mezzanine floors. The results –presented in Table 15- indicated cooling loads savings of around 5.13% for the 1 pearl wall upgrade, and 5.61% for the 2 wall pearl upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 4.98% and 5.10% for the 1 pearl and 2 pearls scenarios respectively. The savings in the annual energy consumption were 3.44% and 3.52% for the 1 pearl scenarios and 2 pearl scenarios respectively.

Annual reductions in electricity consumption for the 1 pearl wall upgrades is estimated at 61.5460 MWeh/yr, and 63.0002 MWeh/yr for the 2 pearls wall. Also, the annual reduction in CO2 emissions are estimated at 29,760 KgCO2 and 32,565 KgCO2 for the 1 pearl and 2 pearls upgrades respectively.

| | | | Wall- 1 | | Wall-2 |
|---|------------|------------------|----------------|-----------------|----------------|
| Output | Baseline | Wall- 1 Pearl | Savings (%) | Wall-2 Pearl | Savings (%) |
| Room cooling plant sens. load (MWh) | 2129.6187 | 2020.4583 | 5.13% | 2010.1325 | 5.61% |
| Chillers energy (MWh) | 950.7911 | 903.4474 | 4.98% | 902.3291 | 5.10% |
| Ap Sys chillers energy (MWh) | 950.7911 | 903.4474 | 4.98% | 902.3291 | 5.10% |
| Ap Sys heat rej fans/pumps energy (MWh) | 285.2376 | 271.034 | 4.98% | 270.6994 | 5.10% |
| Total system energy (MWh) | 1404.4605 | 1342.9365 | 4.38% | 1341.4825 | 4.48% |
| Total electricity (MWh) | 1786.6916 | 1725.1456 | 3.44% | 1723.6914 | 3.53% |
| Total energy (MWh) | 1788.0556 | 1726.5317 | 3.44% | 1725.0775 | 3.52% |
| Total CO2 Emissions ((kgCO2) | 923,993.00 | 894,233.00 | 3.22% | 891,428.00 | 3.52% |

Table 15 Load, Energy and Carbon results of external wall upgrades for the building.

The annual cooling load profile for the three scenarios i.e. baseline, Wall 1 Pearl and Wall 2 Pearls; are presented in Figure 25. It is noticed that the upgrades positively impacted the building performance in terms of cooling loads reduction. The greatest reductions are noticed during the summer months from June to September. For monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.



Figure 25 Comparison for Monthly Room Cooling Plant Sens. Load (MWh) for Wall Upgrades.
5.3 BUILDING FENESTRATION REFURBISHMENT

The refurbishment application for the building fenestration focuses on upgrading the thermal performance of the glazing. The external glazing could be replaced with higher performance of thermal resistance, and improved solar heat gain coefficient (SHGC). This section will present and discuss the results of two different scenarios to upgrade the thermal performance of the building fenestration. The scenarios selected are the upgrades to U-value of 2.2 W/m2.K and 1.9 W/m2.K; and SHGC of 0.4 and 0.3; which are based on the Estidama Pearl Rating System requirements for 1 pearl, and 2-5 pearls rating.

5.3.1 TYPICAL FLOOR

The results for the typical floor –presented in Table 16- indicated cooling loads savings of around 11.02% for the 1 pearl glazing upgrade, and 13.50% for the 2 glazing pearl upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 9.96% and 12.20% for the 1 pearl and 2 pearls scenarios respectively. The savings in the annual energy consumption were 6.87% and 8.41% for the 1 pearl scenarios and 2- pearl scenario respectively.

Annual reductions in electricity consumption for the 1 pearl glazing upgrades is estimated at 7.271 MWeh/yr, and 8.901 MWeh/yr for the 2 pearls glazing. Also, the annual reduction in CO2 emissions are estimated at 3,760 KgCO2 and 4,603 KgCO2 for the 1 pearl and 2 pearls upgrades respectively. For a monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.

| | | | Glazing - 1 Pearl | | Glazing -2 Pearl |
|---|-----------|---------------------|----------------------|---------------------|---------------------|
| Output | Baseline | Glazing- 1 Pearl | Savings (%) | Glazing -2 Pearl | Savings (%) |
| Room cooling plant sens. load (MWh) | 125.4686 | 111.6365 | 11.02% | 108.5303 | 13.50% |
| Chillers energy (MWh) | 56.1426 | 50.5493 | 9.96% | 49.2955 | 12.20% |
| Ap Sys chillers energy (MWh) | 56.1426 | 50.5493 | 9.96% | 49.2955 | 12.20% |
| Ap Sys heat rej fans/pumps energy (MWh) | 16.8428 | 15.1648 | 9.96% | 14.7887 | 12.20% |
| Total system energy (MWh) | 83.2134 | 75.9404 | 8.74% | 74.3098 | 10.70% |
| Total electricity (MWh) | 105.8156 | 98.5444 | 6.87% | 96.9144 | 8.41% |
| Total energy (MWh) | 105.897 | 98.624 | 6.87% | 96.9934 | 8.41% |
| Total CO2 Emissions ((kgCO2) | 54,723.00 | 50,963.00 | 6.87% | 50,120.00 | 8.41% |

| Table | 16 Load. | Energy a | nd Carbon | results of | external | glazing | upgrades | for typical | floor mod | del. |
|-------|----------|----------|-----------|------------|----------|---------|----------|--------------|-----------|------|
| | | | | 1000000 | | 88 | -P8-uuos | -or of prom- | | |

It is noticed that the additional savings beyond the 1 pearl rating upgrades are greater than that achieved through external wall upgrades in the typical floor. The savings in the case of fenestration upgrades ranges from 1.54% to 2.48% which is almost 19 times greater than the case of wall upgrades. Also, it is noticed that the overall savings in the case of 1 pearl upgrade from the baseline case is significant. This is explained due to the significant difference between the thermal performance of the external glazing as-built conditions; which is a clear single glazed window panels; and the proposed upgrades.

5.3.2 ROOF FLOOR

The results for the roof floor –presented in Table 17- indicated cooling loads savings of around 11.57% for the 1 pearl glazing upgrade, and 14.20% for the 2-5 glazing pearl upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 10.48% and 12.86% for the 1 pearl and 2-5 pearls scenarios respectively. The savings in the annual energy consumption were 7.25% and 8.90% for the 1 pearl scenarios and 2-5 pearl scenario respectively.

Annual reductions in electricity consumption for the 1 pearl glazing upgrades is estimated at 7.7473

MWeh/yr, and 9.5098 MWeh/yr for the 2-5 pearls glazing. Also, the annual reduction in CO2 emissions are estimated at 4,006 KgCO2 and 4,917 KgCO2 for the 1 pearl and 2-5 pearls upgrades respectively. For a monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.

| | | | Glazing - 1 Pearl | | Glazing -2 Pearl |
|---|-----------|----------------------|----------------------|---------------------|---------------------|
| Output | Baseline | Glazing - 1 Pearl | Savings (%) | Glazing -2 Pearl | Savings (%) |
| Room cooling plant sens. load (MWh) | 127.3355 | 112.6073 | 11.57% | 109.2521 | 14.20% |
| Chillers energy (MWh) | 56.8844 | 50.925 | 10.48% | 49.5692 | 12.86% |
| Ap Sys chillers energy (MWh) | 56.8844 | 50.925 | 10.48% | 49.5692 | 12.86% |
| Ap Sys heat rej fans/pumps energy (MWh) | 17.0653 | 15.2775 | 10.48% | 14.8708 | 12.86% |
| Total system energy (MWh) | 84.1811 | 76.4326 | 9.20% | 74.6696 | 11.30% |
| Total electricity (MWh) | 106.78 | 99.0327 | 7.26% | 97.2702 | 8.91% |
| Total energy (MWh) | 106.8647 | 99.1162 | 7.25% | 97.3532 | 8.90% |
| Total CO2 Emissions ((kgCO2) | 55,222.00 | 51,216.00 | 7.25% | 50,305.00 | 8.90% |

Table 17 Load, Energy and Carbon results of external glazing upgrades for roof floor model.

Similar to the typical floor, the additional savings beyond the 1 pearl rating upgrades are greater than that achieved through external wall upgrades in the typical floor. The savings in the case of fenestration upgrades

ranges from 1.35% to 2.63% which is almost 15 to 19 times greater than the case of wall upgrades. Also, it is noticed that the overall savings in the case of 1 pearl upgrade from the baseline case is still significant, similar to the case in the typical floor. However, it is slightly reduced than the savings in the typical floor since the contribution of the glazing to the overall exposed envelope is less in the case of the roof. The glazing to the exposed surface area of the building envelope in the case of the roof floor is 12.7%, whereas in the typical floor it is 32.3%.

5.3.3 GROUND AND MEZZANINE FLOORS

The results for the ground and mezzanine floors –presented in Table 18- indicated cooling loads savings of around 18.32% for the 1 pearl glazing upgrade, and 23.27% for the 2 wall glazing upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 16.89% and 21.45% for the 1 pearl and 2 pearls scenarios respectively. The savings in the annual energy consumption were 11.93% and 15.16% for the 1 pearl scenarios and 2- pearl scenario respectively.

Annual reductions in electricity consumption for the 1 pearl glazing upgrades is estimated at 23.6931

MWeh/yr, and 30.0891MWeh/yr for the 2-5 pearls glazing. Also, the annual reduction in CO2 emissions are estimated at 12,250 KgCO2 and 15,557 KgCO2 for the 1 pearl and 2 pearls upgrades respectively. For a monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.

| | | | Glazing - 1 Pearl | | Glazing -2 Pearl |
|---|------------|----------------------|----------------------|---------------------|---------------------|
| Output | Baseline | Glazing - 1 Pearl | Savings (%) | Glazing -2 Pearl | Savings (%) |
| Room cooling plant sens. load (MWh) | 245.7228 | 200.7012 | 18.32% | 188.5416 | 23.27% |
| Chillers energy (MWh) | 107.9103 | 89.6848 | 16.89% | 84.7648 | 21.45% |
| Ap Sys chillers energy (MWh) | 107.9103 | 89.6848 | 16.89% | 84.7648 | 21.45% |
| Ap Sys heat rej fans/pumps energy (MWh) | 32.3731 | 26.9054 | 16.89% | 25.4294 | 21.45% |
| Total system energy (MWh) | 155.2918 | 131.5977 | 15.26% | 125.201 | 19.38% |
| Total electricity (MWh) | 198.4932 | 174.8001 | 11.94% | 168.4041 | 15.16% |
| Total energy (MWh) | 198.6329 | 174.9389 | 11.93% | 168.5421 | 15.15% |
| Total CO2 Emissions ((kgCO2) | 102,649.00 | 90,399.00 | 11.93% | 87,092.00 | 15.16% |

Table 18 Load, Energy and Carbon results of external glazing upgrades for GF and Mezz floor model.

The results indicate significantly higher energy savings for the ground and mezzanine floors compared to the typical and roof floors, when the building fenestration is upgraded. That is due to the high ratio of glazing in the

ground floor level which is used for retail and office spaces; which is 2 times greater than solid external walls area where window to wall ratio is around 67%. The additional savings beyond the 1 pearl rating upgrades were considerably greater than the previous two models for the typical and roof floors with approximately 5% additional reduction in cooling loads.

Generally, the additional savings range from 3.22% to 4.95%; which is 53 to 55 times greater than the additional savings in the case of wall upgrades from 1 to 2 pearl rating. This is one of the significant notes, where great emphasis shall be given on glazing upgrades for similar buildings over wall upgrades. However, the economic feasibility will be addressed at a later section to understand the financial viability of such refurbishment application.

5.3.4 ALL BUILDING

The results for the building consist of 14 typical floors, roof floor, and ground and mezzanine floors. The results –presented in Table 19- indicated cooling loads savings of around 11.90% for the 1 pearl glazing upgrade, and 14.67% for the 2 pearl glazing upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 10.78% and 13.29% for the 1 pearl and 2 pearls scenarios respectively. The savings in the annual energy consumption were 7.45% and 9.19% for the 1 pearl scenarios and 2 pearl scenario respectively.

Annual reductions in electricity consumption for the 1 pearl glazing upgrades is estimated at 133.2372 MWeh/yr, and 164.2157 MWeh/yr for the 2 pearls glazing. Also, the annual reduction in CO2 emissions are estimated at 68,896 KgCO2 and 84,916 KgCO2 for the 1 pearl and 2 pearls upgrades respectively.

| | | | Glazing - 1 Pearl | | Glazing -2 Pearl |
|---|------------|----------------------|----------------------|---------------------|---------------------|
| Output | Baseline | Glazing - 1 Pearl | Savings (%) | Glazing -2 Pearl | Savings (%) |
| Room cooling plant sens. load (MWh) | 2129.6187 | 1876.2195 | 11.90% | 1817.2179 | 14.67% |
| Chillers energy (MWh) | 950.7911 | 848.3 | 10.78% | 824.471 | 13.29% |
| Ap Sys chillers energy (MWh) | 950.7911 | 848.3 | 10.78% | 824.471 | 13.29% |
| Ap Sys heat rej fans/pumps energy (MWh) | 285.2376 | 254.4901 | 10.78% | 247.342 | 13.29% |
| Total system energy (MWh) | 1404.4605 | 1271.1959 | 9.49% | 1240.2078 | 11.70% |
| Total electricity (MWh) | 1786.6916 | 1653.4544 | 7.46% | 1622.4759 | 9.19% |
| Total energy (MWh) | 1788.0556 | 1654.7911 | 7.45% | 1623.8029 | 9.19% |
| Total CO2 Emissions ((kgCO2) | 923,993.00 | 855,097.00 | 7.46% | 839,077.00 | 9.19% |

Table 19 Load, Energy and Carbon results of external glazing upgrades for the building.

The results indicate significant energy savings which is closer to the percentage identified in the typical floor. The additional savings beyond the 1 pearl rating upgrades were considerably greater than the previous case for wall upgrades. The additional savings estimated at 2.77% for the cooling loads, compared to a 0.48% for the wall upgrade.

Generally, the additional savings range from 2.73% to 2.77%; which is 5 times greater than the additional savings in the case of wall upgrades from 1 to 2 pearl rating. However, the 1 pearl refurbishment for the building fenestration is estimated to save 2.3 times greater cooling loads than for the wall refurbishment application. The economic feasibility study will emphasize on the viability of the solution.

The annual cooling load profile for the three scenarios i.e. baseline, Glazing 1 Pearl and Glazing 2 Pearls; are presented in Figure 26. Similar to the wall upgrades, the glazing upgrades positively impacted the building performance in terms of cooling loads reduction. The greatest reductions are noticed during the summer months from June to September. For monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.



Figure 26 Comparison for Monthly Room Cooling Plant Sens. Load (MWh) for Glazing Upgrades.

5.4 EXTERNAL ROOF INSULATION REFURBISHMENT

The refurbishment application for the building's roof implies upgrading the thermal performance of the externally exposed element of the roof. Therefore, the refurbishment technique proposed is addition of thermal insulation. This section will present and discuss the results of two different scenarios to upgrade the thermal performance of the roof. The scenarios selected are the upgrades to U-value of 0.14 W/m2.K and 0.12 W/m2.K; which are based on the Estidama Pearl Rating System requirements for 1 pearl, and 2-5 pearls rating. Since the roof insulation upgrade is only applicable on the roof floor; the results presented in this section will be specifically for the roof floor model, and the overall building.

5.4.1 ROOF FLOOR

The results for the roof floor –presented in Table 20- indicated cooling loads savings of around 3.44% for the 1 pearl roof upgrade, and 3.64% for the 2-5 roof pearl upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 3.12% and 3.30% for the 1 pearl and 2 pearls scenarios respectively. The savings in the annual energy consumption were 2.16% and 2.28% for the 1 pearl scenarios and 2 pearl scenario respectively. It is noticed that the savings are generally the lowest when compared to wall or glazing upgrades, that is mainly because the roof area is only around 6.4% of the overall building envelope.

Annual reductions in electricity consumption for the 1 pearl roof upgrades is estimated at 2.3083 MWeh/yr, and 2.4396 MWeh/yr for the 2 pearls roof. Also, the annual reduction in CO2 emissions are estimated at 1,193 KgCO2 and 1,261 KgCO2 for the 1 pearl and 2 pearls upgrades respectively. For a monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.

| | | | Roof - 1 Boord | | Roof -2 |
|---|-----------|------------------|-------------------|-----------------|---------|
| Output | Baseline | Roof- 1 Pearl | Savings | Roof-2 Pearl | Savings |
| Room cooling plant sens. load (MWh) | 127.3355 | 122.9523 | 3.44% | 122.7032 | 3.64% |
| Chillers energy (MWh) | 56.8844 | 55.1088 | 3.12% | 55.0079 | 3.30% |
| Ap Sys chillers energy (MWh) | 56.8844 | 55.1088 | 3.12% | 55.0079 | 3.30% |
| Ap Sys heat rej fans/pumps energy (MWh) | 17.0653 | 16.5326 | 3.12% | 16.5024 | 3.30% |
| Total system energy (MWh) | 84.1811 | 81.8729 | 2.74% | 81.7417 | 2.90% |
| Total electricity (MWh) | 106.78 | 104.4717 | 2.16% | 104.3404 | 2.28% |
| Total energy (MWh) | 106.8647 | 104.5565 | 2.16% | 104.4252 | 2.28% |
| Total CO2 Emissions ((kgCO2) | 55,222.00 | 54,029.00 | 2.16% | 53,961.00 | 2.28% |

Table 20 Load, Energy and Carbon results of roof upgrades for roof floor model.

It is noticed that roof insulation upgrades are less effective than wall and glazing elements refurbishment. The results for roof insulation upgrades for 1 pearl rating indicated 2.5% less savings in annual cooling loads compared to wall insulation for the same rating level. Moreover, the additional savings for the upgrades from 1 pearl rating to 2 pearl rating for roof u-value is minimal, which ranges between 0.08% and 0.20%. Generally, the cooling loads, energy consumption, and CO2 emissions for the baseline model are greater than that for the typical floor. However, the savings are not greater due to the existing insulation for the roof compared to the walls with no thermal insulation application for the existing conditions.

5.4.2 ALL BUILDING

The results for the building consist of 14 typical floors, roof floor, and ground and mezzanine floors. The results –presented in Table 21- indicated cooling loads savings of around 0.21% for the 1 pearl roof upgrade, and 0.22% for the 2-5 roof pearl upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 0.19% and 0.20% for the 1 pearl and 2-5 pearls scenarios respectively. The savings in the annual energy consumption were 0.13% and 0.14% for the 1 pearl scenarios and 2-5 pearl scenario respectively.

As mentioned in the previous section, the nominal savings are the same as achieved for the single floor of the roof. Annual reductions in electricity consumption for the 1 pearl roof upgrades is estimated at 2.3083 MWeh/yr, and 2.4396 MWeh/yr for the 2-5 pearls roof. Also, the annual reduction in CO2 emissions are

estimated at 1,193 KgCO2 and 1,261 KgCO2 for the 1 pearl and 2-5 pearls upgrades respectively. For a monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.

| | | | Roof - 1 Pearl | | Roof -2 Pearl |
|---|------------|-------------------|-------------------|------------------|------------------|
| Output | Baseline | Roof - 1 Pearl | Savings | Roof -2 Pearl | Savings |
| Room cooling plant sens. load (MWh) | 2129.6187 | 2125.2355 | 0.21% | 2124.9864 | 0.22% |
| Chillers energy (MWh) | 950.7911 | 949.0155 | 0.19% | 948.9146 | 0.20% |
| Ap Sys chillers energy (MWh) | 950.7911 | 949.0155 | 0.19% | 948.9146 | 0.20% |
| Ap Sys heat rej fans/pumps energy (MWh) | 285.2376 | 284.7049 | 0.19% | 284.6747 | 0.20% |
| Total system energy (MWh) | 1404.4605 | 1402.1523 | 0.16% | 1402.0211 | 0.17% |
| Total electricity (MWh) | 1786.6916 | 1784.3833 | 0.13% | 1784.252 | 0.14% |
| Total energy (MWh) | 1788.0556 | 1785.7474 | 0.13% | 1785.6161 | 0.14% |
| Total CO2 Emissions ((kgCO2) | 923,993.00 | 922,800.00 | 0.13% | 922,732.00 | 0.14% |

Table 21 Load, Energy and Carbon results of roof upgrades for the building.

Contrary to the refurbishment applications for the glazing and external walls, the refurbishment of the building roof has minimal if not negligible contribution to the reduction in the overall building's cooling load, energy and electricity consumption. For example, the external wall upgrades to 1 pearl rating contributes to electricity saving 26 times higher than that for the roof upgrade for the same rating level.

The annual cooling load profile for the three scenarios i.e. baseline, Roof 1 Pearl and Roof 2 Pearls; are presented in Figure 27. Similar to the wall & glazing upgrades, the roof upgrades positively impacted the building performance in terms of cooling loads reduction. The greatest reductions are noticed during the summer months from June to September. However, it has to be noted that the annual cooling loads exceed 300 MWh for the 1 & 2 pearls upgrade in July and August unlike the results shown for the wall and glazing. That is mainly due to the minimal impact of the roof upgrades in the case of tall buildings as explained earlier. For monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.



Figure 27 Comparison for Monthly Room Cooling Plant Sens. Load (MWh) for Roof Upgrades.

5.5 COMBINED REFURBISHMENT SOLUTION

The combined refurbishment solution investigates the savings that could be achieved if all above three scenarios are applied all together. This section presents the results for the individual models for the typical floor, roof floor, ground and mezzanine floors, and the overall building; in which the combined solution refers to refurbishment for the external wall and glazing in the typical floor, ground and mezzanine floors. However, combined refurbishment solution for the overall building and the roof floor model implies the refurbishment for the external walls, glazing, and roof.

This section will present and discuss the results of two different scenarios for each of the models. The scenarios selected are the upgrades of the u-values for the external envelope, and glazing upgrades that responds to the requirements stipulated to achieve Estidama Pearl Rating System requirements for 1 pearl, and 2 pearls rating.

5.5.1 TYPICAL FLOOR

The results for the typical floor –presented in Table 22- indicated cooling loads savings of around 17.93% for the 1 pearl upgrade, and 20.82% for the 2-5 wall upgrades. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 16.22% and 18.82% for the 1 pearl and 2 pearls scenarios respectively. The savings in the annual energy consumption were 11.18% and 12.98% for the 1 pearl scenarios and 2 pearl scenario respectively.

Annual reductions in electricity consumption for the 1 pearl upgrade is estimated at 11.8381 MWeh/yr, and 13.7393 MWeh/yr for the 2 pearls upgrade. Also, the annual reduction in CO2 emissions are estimated at 6,121 KgCO2 and 7,104 KgCO2 for the 1 pearl and 2 pearls upgrades respectively. For a monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.

| | | | Combined - | | Combined - |
|---|-----------|-----------|------------|------------|------------|
| | | | 1 Pearl | | 2 Pearl |
| | | Combined- | Savings | Combined - | Savings |
| Output | Baseline | 1 Pearl | (%) | 2 Pearl | (%) |
| Room cooling plant sens. load (MWh) | 125.4686 | 102.9726 | 17.93% | 99.3509 | 20.82% |
| Chillers energy (MWh) | 56.1426 | 47.0364 | 16.22% | 45.5739 | 18.82% |
| Ap Sys chillers energy (MWh) | 56.1426 | 47.0364 | 16.22% | 45.5739 | 18.82% |
| Ap Sys heat rej fans/pumps energy (MWh) | 16.8428 | 14.1109 | 16.22% | 13.6722 | 18.82% |
| Total system energy (MWh) | 83.2134 | 71.3749 | 14.23% | 69.4731 | 16.51% |
| Total electricity (MWh) | 105.8156 | 93.9775 | 11.19% | 92.0763 | 12.98% |
| Total energy (MWh) | 105.897 | 94.0586 | 11.18% | 92.1567 | 12.98% |
| Total CO2 Emissions ((kgCO2) | 54,723.00 | 48,602.00 | 11.19% | 47,619.00 | 12.98% |

Table 22 Load, Energy and Carbon results of combined upgrades solution for typical floor model.

It is noticed that the additional savings beyond the 1 pearl rating upgrades are greater than in the individual elements upgrades scenarios. This is explained through the difference in the solar gain and external conduction profiles for the external envelope; further investigations has been conducted and presented later in this chapter. The results indicated additional savings that ranges from of 1.80% to 2.98%. Also, it is noticed that the overall savings in the case of 1 pearl upgrade from the baseline case is considerable. The total of the individual savings for the glazing and external walls in the typical floor model add up to 16.70%. This is less than the savings in the cooling load when both upgrades are implemented simultaneously; which results in 17.93% savings.

5.5.2 ROOF FLOOR

The results for the roof floor –presented in Table 23- indicated cooling loads savings of around 23.62% for the 1 pearl upgrade, and 27.19% for the 2 pearl upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 21.42% and 24.65% for the 1 pearl and 2- pearls scenarios respectively. The savings in the annual energy consumption were 14.82% and 17.06% for the 1 pearl scenarios and 2- pearl scenario respectively.

Annual reductions in electricity consumption for the 1 pearl wall upgrades is estimated at 15.8382 MWeh/yr, and 18.228 MWeh/yr for the 2 pearls wall. Also, the annual reduction in CO2 emissions are estimated at 8,188 KgCO2 and 9,424 KgCO2 for the 1 pearl and 2 pearls upgrades respectively. For a monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.

| | | | Combined- | | Combined- |
|---|-----------|-----------|-----------|------------|-----------|
| | | | 1 Pearl | a | 2 Pearl |
| Oratarat | Develop | Combined- | Savings | Combined-2 | Savings |
| Output | Basenne | I Peari | (%) | Peari | (%) |
| Room cooling plant sens. load (MWh) | 127.3355 | 97.2532 | 23.62% | 92.7087 | 27.19% |
| Chillers energy (MWh) | 56.8844 | 44.7012 | 21.42% | 42.8629 | 24.65% |
| Ap Sys chillers energy (MWh) | 56.8844 | 44.7012 | 21.42% | 42.8629 | 24.65% |
| Ap Sys heat rej fans/pumps energy (MWh) | 17.0653 | 13.4104 | 21.42% | 12.8589 | 24.65% |
| Total system energy (MWh) | 84.1811 | 68.3432 | 18.81% | 65.9531 | 21.65% |
| Total electricity (MWh) | 106.78 | 90.9418 | 14.83% | 88.552 | 17.07% |
| Total energy (MWh) | 106.8647 | 91.0268 | 14.82% | 88.6367 | 17.06% |
| Total CO2 Emissions ((kgCO2) | 55,222.00 | 47,034.00 | 14.83% | 45,798.00 | 17.07% |

Table 23 Load, Energy and Carbon results of combined upgrades solution for roof floor model.

Similar to the typical floor, the additional savings beyond the 1 pearl rating upgrades are greater than in the individual elements upgrades scenarios. The results indicated additional savings that ranges from of 2.24% to 3.57%. It has to be noted, however, that the results for the roof floor model indicates better savings than the typical floor for the combined scenario. That is because the roof refurbishment adds to the overall savings with additional 5% for the cooling loads.

The total of the individual savings for the roof, glazing and external walls in the roof floor model for the 1 pearl rating add up to 20.95%. This is less than the savings in the cooling load when both upgrades are implemented simultaneously; which results in 23.62% savings. This is explained through the difference in the solar gain and external conduction profiles for the external envelope; further investigations has been conducted and presented later in this chapter.

5.5.3 GROUND AND MEZZANINE FLOORS

The results for the ground and mezzanine floors –presented in Table 24- indicated cooling loads savings of around 23.42% for the 1 pearl upgrade, and 28.80% for the 2 pearl upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 21.60% and 26.56% for the 1 pearl and 2 pearls scenarios respectively. The savings in the annual energy consumption were 15.25% and 18.76% for the 1 pearl scenarios and 2 pearl scenario respectively.

Annual reductions in electricity consumption for the 1 pearl wall upgrades is estimated at 30.2955 MWeh/yr, and 37.2588 MWeh/yr for the 2 pearls wall. Also, the annual reduction in CO2 emissions are estimated at 15,663 KgCO2 and 19,263 KgCO2 for the 1 pearl and 2 pearls upgrades respectively. For a monthly breakdown of the Load, Energy and Carbon results; refer to Appendix E.

| | | | Combined - | | Combined - |
|---|------------|------------|------------|------------|------------|
| | | | 1 Pearl | | 2 Pearl |
| | | Combined - | Savings | Combined - | Savings |
| Output | Baseline | 1 Pearl | (%) | 2 Pearl | (%) |
| Room cooling plant sens. load (MWh) | 245.7228 | 188.179 | 23.42% | 174.9468 | 28.80% |
| Chillers energy (MWh) | 107.9103 | 84.6061 | 21.60% | 79.2497 | 26.56% |
| Ap Sys chillers energy (MWh) | 107.9103 | 84.6061 | 21.60% | 79.2497 | 26.56% |
| Ap Sys heat rej fans/pumps energy (MWh) | 32.3731 | 25.3818 | 21.60% | 23.7749 | 26.56% |
| Total system energy (MWh) | 155.2918 | 124.9974 | 19.51% | 118.0336 | 23.99% |
| Total electricity (MWh) | 198.4932 | 168.1977 | 15.26% | 161.2344 | 18.77% |
| Total energy (MWh) | 198.6329 | 168.3385 | 15.25% | 161.3748 | 18.76% |
| Total CO2 Emissions ((kgCO2) | 102,649.00 | 86,986.00 | 15.26% | 83,386.00 | 18.77% |

Table 24 Load, Energy and Carbon results of combined upgrades solution for GF and Mezz floor model.

The results indicate higher energy consumption for the ground and mezzanine floors compared to the typical floor for the combined solution; however the savings in cooling loads are slightly less than the roof floor. That is due to the high ratio of glazing in the ground floor level which is used for retail and office spaces, where refurbishment of the glazing components highly contribute to the savings compared to the typical floor. However, the savings for the roof floor are almost the same as the ground and mezzanine floors savings; due to the additional savings achieved through roof refurbishment. The additional savings beyond the 1 pearl rating upgrades are greater than that for the individual elements refurbishment. The additional savings ranges between 3.51% and 5.39%.

The total of the individual savings for the glazing and external walls in the ground and mezzanine floor model for the 1 pearl rating add up to 22.20%. This is less than the savings in the cooling load when both upgrades are

implemented simultaneously; which results in 23.42% savings. This is explained through the difference in the solar gain and external conduction profiles for the external envelope; further investigations has been conducted and presented later in this chapter.

5.5.4 ALL BUILDING

The results for the building consist of 14 typical floors, roof floor, and ground and mezzanine floors. The results –presented in Table 25- indicated cooling loads savings of around 18.90% for the 1 pearl upgrade, and 22.12% for the 2 pearl upgrade. The reduction in annual chillers energy and related auxiliary chiller system and heat rejection system are estimated at 17.14% and 20.05% for the 1 pearl and 2 pearls scenarios respectively. The savings in the annual energy consumption were 11.85% and 13.86% for the 1 pearl scenarios and 2 pearl scenarios respectively.

Annual reduction in electricity consumption for the 1 pearl upgrades is estimated at 211.8671 MWeh/yr, and 247.837 MWeh/yr for the 2 pearls. Also, the annual reduction in CO2 emissions are estimated at 109,545 KgCO2 and 128,143 KgCO2 for the 1 pearl and 2 pearls upgrades respectively.

| | | | Combined - | | Combined - |
|---|------------|-----------------------|---------------------------|-----------------------|---------------------------|
| Output | Baseline | Combined - 1 Pearl | 1 Pearl Savings (%) | Combined - 2 Pearl | 2 Pearl Savings (%) |
| Room cooling plant sens. load (MWh) | 2129.6187 | 1727.0486 | 18.90% | 1658.5681 | 22.12% |
| Chillers energy (MWh) | 950.7911 | 787.8169 | 17.14% | 760.1472 | 20.05% |
| Ap Sys chillers energy (MWh) | 950.7911 | 787.8169 | 17.14% | 760.1472 | 20.05% |
| Ap Sys heat rej fans/pumps energy (MWh) | 285.2376 | 236.3448 | 17.14% | 228.0446 | 20.05% |
| Total system energy (MWh) | 1404.4605 | 1192.5892 | 15.09% | 1156.6101 | 17.65% |
| Total electricity (MWh) | 1786.6916 | 1574.8245 | 11.86% | 1538.8546 | 13.87% |
| Total energy (MWh) | 1788.0556 | 1576.1857 | 11.85% | 1540.2053 | 13.86% |
| Total CO2 Emissions ((kgCO2) | 923,993.00 | 814,448.00 | 11.86% | 795,850.00 | 13.87% |

The results indicate significant energy, cooling load, and CO2 emissions savings for the overall combined refurbishment solutions applied to the building. The reduction in cooling loads is slightly higher than achieved in the typical floor. That is due to the contribution of roof retrofitting application, as well as the high savings in the ground and mezzanine floors for glazing refurbishment. Generally, the savings in the typical floor could be generalized for the overall building as a representation of the reduction in cooling loads, energy, and CO2

emissions reduction. Although, it has to be noted that the behavior of the ground, mezzanine and roof floors vary than that for the typical floor. That is due to the high ratio of glazing in the ground floor level which is used for retail and office spaces, where refurbishment of the glazing components highly contribute to the savings compared to the typical floor. And, the savings for the roof floor are almost the same as the ground and mezzanine floors savings; due to the additional savings achieved through roof refurbishment. The additional savings beyond the 1 pearl rating upgrades are greater than that for the individual elements refurbishment. The additional savings ranges between 2.01% and 3.22%.

The total of the individual savings for the roof, glazing and external walls for the overall building for the 1 pearl rating add up to 17.23%. This is less than the savings in the cooling load when both upgrades are implemented simultaneously; which results in 18.90% savings. This is explained through the difference in the solar gain and external conduction profiles for the external envelope; further investigations has been conducted and presented later in this chapter.

5.6 SOLAR GAIN AND EXTERNAL CONDUCTION GAIN

The results as presented on the previous sections indicated that the combined refurbishment solutions, where several retrofitting applications are applied simultaneously, are more efficient than when individual scenarios are implemented. In order to explain the buildings behavior according to the results indicated, further investigations were conducted to understand the thermal performance of the building envelope when individual elements are refurbished, and when the combined solutions are implemented. This study has been conducted on a sample room within the building floors, which is the southern-west corner room.

Prior to presenting the results for solar gain and external conduction gain, it is necessary to define both parameters as measured in the IES-VE tool for better understanding of the results. The following are the definitions as stipulated in the IES-VE manual (IES 2013, p. 42)

"Solar gain: Solar radiation absorbed on the internal surfaces of the room, plus solar radiation absorbed in glazing and transferred to the room by conduction.

External conduction gain: Heat conducted into (or if negative, out of) the room through the internal surfaces of externally exposed elements, including ground floors."

According to the definitions above, the solar gain depends on the radiation absorbed on the internal surface of the room. Therefore, the results presented in Figure 26 indicates that the external wall refurbishment in the typical floor have the same exposure to solar gain as for the baseline. However, since the composition of the glazing varies than the baseline, the solar gain when the glazing elements are replaced is less than that for the walls. It is also noted that the for the combined solutions, for 1 pearl rating and 2-5 pearls rating, that the solar gain is similar to that for the glazing respective to the same rating upgrades. This is explained through the calculations criteria for the solar; in the case of walls upgrade only, the glazing elements still transfers great amounts for solar radiation, which results in all models where no glazing upgrades are implemented remain of the same total solar gain value; meaning that the glazing elements are the weakest elements within the building envelope that allows for the solar radiation transfer into the building.

However, once the glazing elements are upgraded, less solar radiation is allowed into the building. This is why the upgrades for the glazing elements into 1 pearl, and 2-5 pearls rating result in similar solar gain for the overall upgrades for the typical floor respectively. This behavior has also been noticed for the other floors, where the glazing has been the weakest element for solar radiation exposure and solar gain transfers. For further details on the results, please refer to Appendix E.



Figure 28 Solar gain profile for the typical floor.

Having analyzed the building envelope reaction to solar gain, it is necessary to understand the external conduction gain which will further explain the behavior of the building through refurbishment of the individual elements versus the combined refurbishment solution. The following Figure 27 presents the results for the external conduction gain for the sample room in the typical floor. The results indicate negative figures for the months between November to March for the baseline, and wall upgrades scenarios, and December to March for the glazing and combined refurbishment models. The negative figures indicate that the heat transfers from inside the building to outside, unlike the summer months where the building interior is heated through the external conduction gain properties.





In order to tabulate the difference in the building behavior when combined solutions are applied and when individual elements are applied, the following comparison for 1 pearl rating upgrades –presented in Table 26-indicates that the nominal difference in the external conduction gain between the sum of the individual refurbishment solutions to the baseline, and the combined solution to the baseline vary slightly. Although the

difference is minimal, which around 0.0386 (MWh), it still contributes to the additional savings when a combined solution is implemented over individual scenarios. Figure 28 presents the results for the 1 pearl ratings upgrades graphically for the walls, glazing, and combined solution for the typical floor. It is noticed that the difference between the individual refurbishment applications, and combined scenario in terms of external conduction gains are the greatest during the summer from June to September, and in the winter from December to January.

| | External conduction gain (MWh) | | | | Absolute Difference (MWh) | | | |
|--------------|--------------------------------|--------------------|--------------|----------|---------------------------|-----------------------|------------------------|---------------------------------|
| | 1 Pearl (combined) | Glazing 1 Pearl | Wall 1 Pearl | Baseline | Baseline - wall | Baseline - glazing | Baseline - combined | Sum of individual savings |
| Date | | | | | | | | |
| Jan 01-31 | -0.0798 | -0.1082 | -0.2154 | -0.2501 | 0.0347 | 0.1419 | 0.1703 | 0.1766 |
| Feb 01-28 | -0.0476 | -0.0628 | -0.1558 | -0.1821 | 0.0263 | 0.1193 | 0.1345 | 0.1456 |
| Mar 01-31 | -0.0231 | -0.0153 | -0.1129 | -0.1199 | 0.007 | 0.1046 | 0.0968 | 0.1116 |
| Apr 01-30 | 0.0345 | 0.0774 | 0.0014 | 0.0221 | 0.0207 | 0.0553 | 0.0124 | 0.076 |
| May 01-31 | 0.0968 | 0.1796 | 0.1185 | 0.1696 | 0.0511 | 0.01 | 0.0728 | 0.0611 |
| Jun 01-30 | 0.1261 | 0.2343 | 0.1783 | 0.2526 | 0.0743 | 0.0183 | 0.1265 | 0.0926 |
| Jul 01-31 | 0.1546 | 0.2779 | 0.2289 | 0.3144 | 0.0855 | 0.0365 | 0.1598 | 0.122 |
| Aug 01-31 | 0.1538 | 0.2808 | 0.2257 | 0.3156 | 0.0899 | 0.0348 | 0.1618 | 0.1247 |
| Sep 01-30 | 0.123 | 0.2276 | 0.1675 | 0.2396 | 0.0721 | 0.012 | 0.1166 | 0.0841 |
| Oct 01-31 | 0.061 | 0.1219 | 0.047 | 0.0832 | 0.0362 | 0.0387 | 0.0222 | 0.0749 |
| Nov 01-30 | 0.0022 | 0.0273 | -0.0554 | -0.0455 | 0.0099 | 0.0728 | 0.0477 | 0.0827 |
| Dec 01-31 | -0.0578 | -0.0754 | -0.1713 | -0.197 | 0.0257 | 0.1216 | 0.1392 | 0.1473 |
| Summed total | 0.5437 | 1.1652 | 0.2566 | 0.6027 | 0.5334 | 0.7658 | 1.2606 | 1.2992 |

Table 26 External conduction gain (MWh) for the typical floor.



Figure 30 External Conduction Gain (MWH) for 1 Pearl refurbishment scenarios for the typical floor.

The study has been conducted for the typical floor, roof, and ground and mezzanine floor. It has been noticed that the external building envelope behavior –in all cases- had the same differences in the external conduction gain profile for the individual versus the combined solutions. The study was conducted for both the 1 pearl upgrades set, and 2 pearls upgrades set. The following Figure 29 highlights the external conduction gain for the roof floor when the refurbishment applications for 2 pearls rating are simulated. It is noted that both the external walls, and roof have similar behavior profile, which varies from the glazing. That is again supports the results highlighted for the solar gain analysis, where glazing has been identified as the weakest element for solar gain. In this example, the 2 pearl combined scenario has 0.0727 MWh less conduction gain than the sum of the individual scenarios. For the results of the 1 and 2 pearls sets of refurbishment scenarios for all models, refer to Appendix E.



Figure 31 External Conduction Gain (MWH) for 2 Pearl refurbishment scenarios for the roof floor.

In this section above, it is concluded that the combined refurbishment scenario results in higher savings and better building envelope performance. However, in order to understand the economic feasibility of these scenarios the following section presents a simple payback period study, for future considerations of optimal refurbishment solution.

5.7 ECONOMIC FEASIBILITY OF THE BUILDING ENVELOPE REFURBISHMENT

The economic feasibility study of the proposed refurbishment solutions is critical to allow for a comprehensive understanding prior to making decisions of which building elements and which refurbishment technique shall be implemented in order to reach the desired outcome to reduce energy consumption. The economic viability study presented in this section has been based on simple payback period analysis where the consideration of reduction in electricity consumption is the main objective. Similar, to the results presented for the energy savings earlier, this section will address the economic feasibility for the refurbishment applications to each of the models and for the overall building. The economic feasibility has been considered based on the current market analysis, and the available applications for wall insulation, roof insulation, and glazing replacement.

5.7.1 REFURBISHMENT APPLICATIONS AND CURRENT AVAILABILITY IN THE UAE MARKET

As highlighted earlier, there are two applications for external walls upgrades, which are available in the UAE market; the addition of thermal insulation boards, and the curtain wall application. For the roof refurbishment, a simple addition of thermal insulation boards is available, whereas the glazing panels are easily replaced. For selection of available thermal insulation materials, and better understanding of the market applications, the research highlights the materials adopted by the UPC Estidama product database stipulated under Estidama Villa Product Database (EVPD) as guidance. (UPC 2013c). Figure 30 illustrates a thermal insulation product that could be used as a curtain wall application to provide additional external insulation mechanically fixed to the existing structure and then covered by external cladding finishing. Another method is shown in Figure 31 which illustrates insulation boards that could be fixed internally to the existing building envelope.



Figure 32 External insulation applicable for curtain wall solution. (UPC 2013c, p.1)



Figure 33 Insulation board application for building envelope. (UPC 2013c, p.1)

The estimated cost of the different refurbishment scenarios was calculated based on an estimated refurbishment unit cost inclusive of the material, transportation, and installation costs in the UAE. The estimated cost is highlighted in Table 27.

| Refurbished construction | Unit refurbishment cost (AB | ED/ m2); inclusive of supply, | | | | | |
|--------------------------|---|-------------------------------|--|--|--|--|--|
| element | installation and painting (not for glazing) | | | | | | |
| | 1 Pearl requirements | 2 Pearls requirements | | | | | |
| Wall (insulation boards) | 140 | 165 | | | | | |
| Wall (curtain wall) | 300 | 325 | | | | | |
| Roof | 125 | 150 | | | | | |
| Glazing | 260 | 280 | | | | | |

Table 27 Refurbishment unit cost in the UAE. (Manneh et al 2013, p. 5)

5.7.2 REFURBISHMENT COST SAVINGS

Prior to calculating the simple payback period (SPP), the cost savings due to reduction in electricity consumption has to be calculated. Tables Tables 28 - 31 present the cost savings for each of the individual floors models, and the overall building for each of the refurbishment scenarios. The cost savings were estimated based on electricity unit cost rate of 0.33 AED/KWeh Which is highlighted in tables 28- 31.

 Table 28 Cost savings due to refurbishment applications for the typical floor.

| | 1 P | earl Configurat | ion | 2 Pearls Configuration | | | |
|--|------------------------------------|--|--|------------------------------------|--|--|--|
| Refurbished construction element | Cooling load saving (MWh/yr) | Electricity [*] saving (MW _e h/yr) | Cost saving ^{**} (AED/yr) | Cooling load saving (MWh/yr) | Electricity [*] saving (MW _e h/yr) | Cost saving ^{**} (AED/yr) | |
| Wall | 7.1158 | 3.7520 | 1,238.16 | 7.2832 | 3.8403 | 1,267.30 | |
| Roof | n/a | n/a | n/a | n/a | n/a | n/a | |
| Glazing | 13.8321 | 7.2712 | 2,399.496 | 16.9383 | 8.9012 | 2,937.40 | |
| All | 22.496 | 11.8381 | 3,906.573 | 26.1177 | 13.7393 | 4,533.97 | |

* Assuming a HVAC system with a coefficient of performance (COP) of 2.2 based on ASHRAE 90-1975

** Using electricity rate of 0.33 AED/kWeh

| Table 29 | Cost savings | due to refurbishme | nt applications for | the roof floor. |
|----------|--------------|--------------------|---------------------|-----------------|
|----------|--------------|--------------------|---------------------|-----------------|

| | 1 P | earl Configurat | ion | 2 Pearls Configuration | | | |
|--|------------------------------------|---|-----------|------------------------------------|--|------------------------------|--|
| Refurbished construction element | Cooling load saving (MWh/yr) | Electricity [*] saving (MW _e h/yr) (AED/yr) | | Cooling load saving (MWh/yr) | Electricity [*] saving (MW _e h/yr) | Cost saving** (AED/yr) | |
| Wall | 7.5687 | 3.9896 | 1,316.568 | 7.7492 | 4.0848 | 1,347.98 | |
| Roof | 4.3832 | 2.3083 | 761.739 | 4.6323 | 2.4396 | 805.07 | |
| Glazing | 14.7282 | 7.7473 | 2,556.609 | 18.0834 | 9.5098 | 3,138.23 | |
| All | 30.0823 | 15.8382 | 5,226.606 | 34.6268 | 18.2280 | 6,015.24 | |

 \ast Assuming a HVAC system with a coefficient of performance (COP) of 2.2 based on ASHRAE 90-1975

** Using electricity rate of 0.33 AED/kWeh

Table 30 Cost savings due to refurbishment applications for the ground and mezzanine floors.

| | 1 P | earl Configurat | ion | 2 Pearls Configuration | | | |
|--|------------------------------------|---|-----------|------------------------------------|--|--|--|
| Refurbished construction element | Cooling load saving (MWh/yr) | Electricity [*] saving (MW _e h/yr) (AED/yr) | | Cooling load saving (MWh/yr) | Electricity [*] saving (MW _e h/yr) | Cost saving ^{**} (AED/yr) | |
| Wall | 9.5392 | 5.0284 | 1,659.372 | 9.7722 | 5.1512 | 1,699.90 | |
| Roof | n/a | n/a | n/a | n/a | n/a | n/a | |
| Glazing | 45.0216 | 23.6931 | 7,818.723 | 57.1812 | 30.0891 | 9,929.40 | |
| All | 57.5438 | 30.2955 | 9,997.515 | 70.776 | 37.2588 | 12,295.40 | |

 \ast Assuming a HVAC system with a coefficient of performance (COP) of 2.2 based on ASHRAE 90-1975

** Using electricity rate of 0.33 AED/kW_eh

Table 31 presents both the overall cost savings and the unit cost savings. The unit cost savings will be used later to verify the overall savings that could be achieved in Abu Dhabi if the refurbishment applications are implemented on a wide scale for all buildings presented through the studied prototype.

| 1 Pe | earl Configura | tion | 2-5 Pearls Configuration | | |
|---------------------------------------|---|--|---|--|---|
| Cooling load saving (MWh/yr) | Electricity [*] saving (MW _e h/yr) | Cost saving ^{**} (AED/yr) | Cooling load saving (MWh/yr) | Electricity [*] saving (MW _e h/yr) | Cost saving ^{**} (AED/yr) |
| 109.1604 | 61.5460 | 20310.18 | 119.4862 | 63.0002 | 20,790.07 |
| 4.3832 | 2.3083 | 761.739 | 4.6323 | 2.4396 | 805.07 |
| 253.3992 | 133.2372 | 43968.276 | 312.4008 | 164.2157 | 54,191.18 |
| 402.5701 | 211.8671 | 69916.143 | 471.0506 | 247.8370 | 81,786.21 |
| | | | | | |
| 0.0148 | 0.0083 | 2.7466 | 0.0162 | 0.0085 | 2.8115 |
| 0.0006 | 0.0003 | 0.1030 | 0.0006 | 0.0003 | 0.1089 |
| 0.0343 | 0.0180 | 5.9459 | 0.0422 | 0.0222 | 7.3284 |
| 0.0544 | 0.0287 | 9.4549 | 0.0637 | 0.0335 | 11.0601 |
| | 1 Pe Cooling load saving (MWh/yr) 109.1604 4.3832 253.3992 402.5701 0.0148 0.0006 0.0343 0.0544 | 1 Pearl Configura Cooling load saving (MWh/yr) Electricity* saving (MWeh/yr) 109.1604 61.5460 4.3832 2.3083 253.3992 133.2372 402.5701 211.8671 0.0148 0.0083 0.0006 0.0003 0.0343 0.0180 0.0544 0.0287 | 1 Pearl Configuration Cooling load saving (MWh/yr) Electricity* saving (MWeh/yr) Cost saving* (AED/yr) 109.1604 61.5460 20310.18 4.3832 2.3083 761.739 253.3992 133.2372 43968.276 402.5701 211.8671 69916.143 0.0148 0.0083 2.7466 0.0006 0.0003 0.1030 0.0343 0.0180 5.9459 0.0544 0.0287 9.4549 | $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | I Pearl Configuration2-5 Pearls ConfigurCooling load saving (MWh/yr)Electricity* saving (MWeh/yr)Cost saving* (AED/yr)Cooling load saving (MWh/yr)Electricity* saving (MWh/yr)109.160461.546020310.18119.486263.00024.38322.3083761.7394.63232.4396253.3992133.237243968.276312.4008164.2157402.5701211.867169916.143471.0506247.83700.01480.00832.74660.01620.00850.00060.00030.10300.00060.00030.03430.01805.94590.04220.02220.05440.02879.45490.06370.0335 |

Table 31 Cost savings due to refurbishment applications for the overall building.

* Assuming a HVAC system with a coefficient of performance (COP) of 2.2 based on ASHRAE 90-1975 ** Using electricity rate of 0.33 AED/kWeh

5.7.3 SIMPLE PAYBACK PERIOD STUDY

The estimated SPP was calculated by dividing the refurbishment cost by the cost of the energy saved annually – as highlighted in the previous tables. Table 32 summerizes the results of the simple payback period study for all individual floors, and for the overall building. As highlighted, the glazing elements upgrade to 2-5 pearl rating is the most economically viable solution to in all scenarios, where 9 years payback period could achieve savings of 164.2157 MWhe of annual electricity consumption.

It also, have to be noted that the upgrades in the combined solution for the overall building to 2-5pearl rating when thermal insulation boards for the walls are used along with roof, and glazing refurbishment, has a SPP of around 16 years. Therefore, the additional cost used for the refurbishment could be justified by the significant savings as well as the fact that this simple payback period did only consider the rewards from energy savings perspective only. It is important to highlight – within this context- that the payback period calculations excludes the savings in government electricity cost subsidies, evaluation of building envelop climatic performance upgrade such as humidity resistance, air tightness, aesthetical appearance, as well as future increases in the cost of electricity. It is expected that once all the benefits are quantified, the SPP analysis will result in reasonable timeframe for the owners to recoup their initial investment cost.

Table 32 Summary of the SPP for all configurations.

| | | 1 Pearl Configuration | | | 2-5 Pearls Configuration | | |
|----------|----------------------------------|-----------------------------|----------------------------|-------------------------------------|-----------------------------|-------------------------|-------------------------------------|
| MODEL | Refurbished construction element | Refurbishment cost (AED) | Cost saving (AED/yr) | Simple payback period (yr) | Refurbishment cost (AED) | Cost saving (AED/yr) | Simple payback period (yr) |
| | Wall (insulation boards) | 40,555.20 | 1,238.16 | 32.75 | 47,797.20 | 1,267.30 | 37.72 |
| | Wall (curtain wall) | 86,904.00 | 1,238.16 | 70.19 | 94,146.00 | 1,267.30 | 74.29 |
| SR | Roof | n/a | n/a | n/a | n/a | n/a | n/a |
| , FLOO | Glazing | 24,398.40 | 2,399.50 | 10.17 | 26,275.20 | 2,937.40 | 8.95 |
| PICAL | All (insulation boards) | 64,953.60 | 3,906.57 | 16.63 | 74,072.40 | 4,533.97 | 16.34 |
| TYI | All (curtain wall) | 111,302.40 | 3,906.57 | 28.49 | 120,421.20 | 4,533.97 | 26.56 |
| | Wall (insulation boards) | 40,555.20 | 1,316.57 | 30.80 | 47,797.20 | 1,347.98 | 35.46 |
| | Wall (curtain wall) | 86,904.00 | 1,316.57 | 66.01 | 94,146.00 | 1,347.98 | 69.84 |
| | Roof | 55,887.50 | 761.74 | 73.37 | 67,065.00 | 805.07 | 83.30 |
| OOR | Glazing | 24,398.40 | 2,556.61 | 9.54 | 26,275.20 | 3,138.23 | 8.37 |
| JF FL | All (insulation boards) | 120,841.10 | 5,226.61 | 23.12 | 141,137.40 | 6,015.24 | 23.46 |
| ROG | All (curtain wall) | 167,189.90 | 5,226.61 | 31.99 | 187,486.20 | 6,015.24 | 31.17 |
| | Wall (insulation boards) | 56,229.60 | 1,659.37 | 33.89 | 66,270.60 | 1,699.90 | 38.99 |
| ORS | Wall (curtain wall) | 120,492.00 | 1,659.37 | 72.61 | 130,533.00 | 1,699.90 | 76.79 |
| TO | Roof | n/a | n/a | n/a | n/a | n/a | n/a |
| O ANI | Glazing | 89,525.80 | 7,818.72 | 11.45 | 96,412.40 | 9,929.40 | 9.71 |
| OUNI | All (insulation boards) | 145,755.40 | 9,997.52 | 14.58 | 162,683.00 | 12,295.40 | 13.23 |
| GR ME | All (curtain wall) | 210,017.80 | 9,997.52 | 21.01 | 226,945.40 | 12,295.40 | 18.46 |
| | Wall (insulation boards) | 664,557.60 | 20,310.18 | 32.72 | 783,228.60 | 20,790.07 | 37.67 |
| | Wall (curtain wall) | 1,424,052.00 | 20,310.18 | 70.12 | 1,542,723.00 | 20,790.07 | 74.20 |
| U | Roof | 55,887.50 | 761.74 | 73.37 | 67,065.00 | 805.07 | 83.30 |
| LDIN | Glazing | 455,478.40 | 43,968.28 | 10.36 | 490,515.20 | 54,191.18 | 9.05 |
| BUI | All (insulation boards) | 1,175,923.50 | 69,916.14 | 16.82 | 1,340,808.80 | 81,786.21 | 16.39 |
| ALI | All (curtain wall) | 1,935,417.90 | 69,916.14 | 27.68 | 2,100,303.20 | 81,786.21 | 25.68 |

Based on the above, it is recommended to invest on a combined refurbishment scenario for the 2-5 pearl rating standards where the capital cost allows for such application. Where financial restrictions on the capital cost, it is recommended to upgrade the building glazing, especially for the ground floor since it is an easy application, and contributes greatly to the energy savings. Table 33 summerized the potential savings in the cooling loads, energy, and Carbon emissions for the overall building once the refurbishment scenarios are applied. Figure 32 highlights the savings in percentage compared to the baseline.

| | Refurbished construction element | Room cooling plant sens. load (MWh/yr) | Chillers energy (MWh/yr) | Ap Sys chillers energy (MWh/yr) | Ap Sys heat rej fans/pumps energy (MWh/yr) | Total system energy (MWh/yr) | Total electricity (Mweh/yr) | Total energy (MWh) | Total Carbon Emissions (KgCO2/yr) |
|-----------------|--|--|--------------------------------|--|--|---------------------------------------|-----------------------------------|--------------------------|--|
| | Baseline | 2129.6187 | 950.7911 | 950.7911 | 285.2376 | 1404.4605 | 1786.6916 | 1788.0556 | 923,993.00 |
| ion | Wall | 2020.4583 | 903.4474 | 903.4474 | 271.034 | 1342.9365 | 1725.1456 | 1726.5317 | 894,233.00 |
| earl gurati | Roof | 2125.2355 | 949.0155 | 949.0155 | 284.7049 | 1402.1523 | 1784.3833 | 1785.7474 | 922,800.00 |
| 1 F onfig | Glazing | 1876.2195 | 848.3 | 848.3 | 254.4901 | 1271.1959 | 1653.4544 | 1654.7911 | 855,097.00 |
| 0 | All | 1727.0486 | 787.8169 | 787.8169 | 236.3448 | 1192.5892 | 1574.8245 | 1576.1857 | 814,448.00 |
| u | Wall | 2010.133 | 902.3291 | 902.3291 | 270.6994 | 1341.483 | 1723.691 | 1725.078 | 891,428.00 |
| Pearl uratio | Roof | 2124.986 | 948.9146 | 948.9146 | 284.6747 | 1402.021 | 1784.252 | 1785.616 | 922,732.00 |
| 2-5 1 Jonfig | Glazing | 1817.218 | 824.471 | 824.471 | 247.342 | 1240.208 | 1622.476 | 1623.803 | 839,077.00 |
| 0 | All | 1658.568 | 760.1472 | 760.1472 | 228.0446 | 1156.61 | 1538.855 | 1540.205 | 795,850.00 |

Table 33 Summary Comparison for Load, Energy, and Carbon Savings for the overall building.



Figure 34 Summary Comparison for Load, Energy, and Carbon Savings for the overall building.

In conclusion, the significant 22.12% reduction in cooling loads could be achieved with a simple payback period estimated at 16 years, when 2-5 pearls rating combined solution refurbishment is applied.

5.8 POTENTIAL ENERGY SAVINGS ACROSS ABU DHABI

This study aimed at conducting an assessment of the potential energy savings in Abu Dhabi. Since this case study has been identified as a representation of the commercial building in Abu Dhabi for the period from 1980 - 1989, and based on the studies presented in the literature review; it is considered that the case study represents an overall of 550,000 square meters of office space GFA.

Table 34 presents the overall unit savings and the overall savings in electricity consumption in Abu Dhabi for the existing buildings stock built in the period from 1980 to 1989. The annual savings of the electricity consumptions are estimated at 18,433.52 MWeh for the combined solution upgrades to 2-5 pearl rating retrofitting application. Whereas, the refurbishment of the most economically feasible solution to upgrade the building glazing to 2-5 pearl rating standards, can achieve an overall reduction for the same buildings estimated at 12,213.97 MWeh/yr. CO2 emissions reduction for the combined solution of 2-5 pearls rating is estimated at 9,530,968.13 KgCO2/yr, whereas that for the 1 pearl combined solution upgrade is estimated at 8,147,693.62 KgCO2/yr.

| | Unit S | avings | Abu Dhabi 1980s Buildings | | |
|-------------------------|--|-----------|------------------------------------|------------------------------------|--|
| | 1 Pearl | 2-5 Pearl | 1 Pearl | 2-5 Pearl | |
| | Rating | Rating | Rating | Rating | |
| | ElectricityElectricitysavingsaving(MWeh/yr)(MWeh/yr) | | Electricity saving (MWeh/yr) | Electricity saving (MWeh/yr) | |
| | | | | | |
| Wall (4746.84 sq.m.) | 0.0083 | 0.00852 | 4,577.64 | 4,685.80 | |
| Roof (447.1 sq.m.) | 0.0003 | 0.00033 | 171.69 | 181.45 | |
| Glazing (1751.84 sq.m.) | 0.0180 | 0.02221 | 9,909.86 | 12,213.97 | |
| All (GFA 7394.7 sq.m.) | 0.0287 | 0.03352 | 15,758.17 | 18,433.52 | |

Table 34 Summary of Annual Electricity Savings in Abu Dhabi for 1980s Buildings.

Having stated the above, and in consideration of the building prototype identified earlier for the 1990s building stock, it can be concluded that the ground floor level with great percentage of external glazing can be considered as a representation for the 1990s buildings. The difference could be summarized for the baseline in the case of 1990s building; it shall use clear double glazed panels with U-value of 3.0 W/m2.K and SHGC of 0.7, HVAC COP of 3.0, and an open space plan. Therefore, the modifications above were introduced to the ground floor model to conclude a rough estimation as a start point for further investigation on the behavior of

the typical office floor for a 1990s building, and the potential reduction in electricity when the building is upgraded to 1 pearl rating and 2 pearls rating for the glazing elements. Table 35 highlights the savings in electricity consumption in Abu Dhabi if glazing has been refurbished to the 1 pearl and 2 pearls rating standards. Since the existing building stock is higher for this building prototype (represented in a total GFA of 862,500 sq.m.); the overall savings for Abu Dhabi are estimated at 28,598.86 MWeH/yr and 20,152.07 MWeh/yr for the 2 pearls and 1 pearl rating respectively.

Abu Dhabi 1990s Buildings Unit Savings 2-5 Pearl 2-5 Pearl 1 Pearl 1 Pearl Rating Rating Rating Rating Electricity Electricity Electricity Electricity saving saving saving saving (MWeh/yr) (MWeh/yr) (MWeh/yr) (MWeh/yr) 0.0234 0.03316 Glazing 20,152.07 28,598.86

Table 35 Summary of Annual Electricity Savings in Abu Dhabi for 1980s Buildings.

Although, the above results for the 1990s prototype is rough, it is considered indicative of the situation and will require further studies to better estimate the savings for various techniques.

The following Chapter presents a set of recommendations for further studies in light of this research. Also, it concludes the study by presenting the major findings of this research.

CHAPTER 6: CONCLUSION AND RECOMMENDATION

6 CONCLUSION AND RECOMMENDATIONS CONCLUSION

The UAE has witnessed rapid growth in the urban development in the past few decades. Since the discovery of oil in 1960s, and the increase in population, the construction industry has been a greatly active sector in the country. This development, however, was accompanied with great growth rate in energy consumption in the Emirates. According to Al-Iriani (2005), the average growth rate in energy consumption in the UAE for the period between 1980 and 2000 was estimated at 10% annual growth rate, which topped that for the world estimated at 3%. In the UAE, the built environment is estimated to contribute to nearly 40% of the total energy consumption, in which around 98%-99.5% were built prior to enforcement of green building regulations in the country such as Estidama Pearl Rating System in Abu Dhabi. (Alawadi et al. 2013). Therefore it is estimated that the major savings in energy consumption can be achieved through refurbishment of the existing building stock. This increased demand in energy consumption, and the environmental impact of the existing building stock triggered the question whether refurbishment applications can significantly reduce the energy consumption and positively contribute to the achievements of the national goals in reducing CO2 emissions by 2030.

The research studied the urban development in Abu Dhabi since 1960s to identify the existing building stock, and the typologies responding to the development of construction methods and materials. It has been identified that around 54% of the existing building stock in Abu Dhabi is categorized under commercial and governmental sectors, which gives more value to conducting research on office buildings. The research also concluded that the existing building stock mainly include the buildings constructed in 1980s onwards. The buildings prior to 1980s were mostly demolished due to two main reasons; being of poor quality, and having changed the regulations for buildings heights to more vertical development. The study has investigated the building regulations applicable to the building envelope thermal performance, and concluded that there were no specific standards enforced on this regard. However, it wasn't until the year 2010 when Estidama Pearl Rating requirements for minimum one pearl rating for all new buildings, and two pearls for governmental buildings have been enforced.

Based on the literature review, and the studies of the existing building stock, two building prototypes were identified to represent office buildings in the 1980s and 1990s. The major differences between both prototypes have been identified to be as following;

For the buildings in the 1980s;

- Mixed use buildings with conversion from residential to commercial spaces
- Post-modern Architecture
- 15-20 stories height
- Plaster finishing with stone cladding introduced in the late 1980s
- No external wall insulation
- Single glazing
- Window-type HVAC units

For the buildings in 1990s;

- Both mixed-use residential conversion, and stand-alone office buildings
- Post-modern and modern Architecture
- 20-25 stories height
- Curtain wall and/or fully glazed facades, aluminum cladding, and stone cladding
- Concrete and steel structure
- Double glazing
- Central AC system

The literature review of the existing building stock and analysis of the chronological order of the urban development in Abu Dhabi facilitated identifying the total GFA representative of each of the periods from 1980-1989 and 1990-1999.

Further to the identification of representative prototype for commercial buildings in 1980s and 1990s and the estimated total GFA for each decade, a case study of an existing building in Abu Dhabi has been selected. The building represents the mixed-use buildings built in the 1980s. Computer modelling was used to assess the savings in electricity consumption, associated cooling loads, energy consumption, and CO2 emissions for the selected prototype. The 17 stories building was modeled in three simulation models; typical floor, roof floor, and ground and mezzanine floors. Severn to Nine building simulations for each of the models were conducted to assess savings due to individual elemental refurbishment and combined scenarios considering upgrades to 1 and 2 pearls rating thermal properties. The potential reduction in cooling loads for the overall building varies dramatically depending on the refurbishment application. For the upgrades to 1 pearl rating standards, the

savings range from 0.21% in the case of roof, to 5.13% and 11.90% in the case of the wall and fenestration upgrades respectively. However, for the upgrades to 2 pearls rating requirements, the savings were estimated at 0.22% for the roof upgrades, 5.61% and 14.67 for the wall and fenestration upgrades respectively.

The results indicated that the savings in the typical floor were the closest representation to the results for the overall building; that is because the total GFA representing the typical floor is around 82% of the total building GFA. Also, it has been noted that the savings from the roof refurbishment is considered negligible for the overall building savings. On the other hand, the glazing upgrades have proven to be the most effective solution which achieves the highest savings. One of the important conclusions of this study is the fact that individual elements of the building, and individual floors could be looked at for prioritized refurbishment strategy depending on the individual savings that could be achieved, easement of implementation, and economic feasibility.

Moreover, the study highlights that combined solutions achieve greater savings than when individual refurbishment applications are considered. Solar gain, and external conduction gain analysis was conducted to understand the results for the combined solution. Based on the analysis, it has been noticed that the elements behavior and specifically the external conduction gain profile varies for the various applications. The solar gain analysis identified the glazing as the weakest element, where the overall solar gain is always linked to the glazing properties. An example for the set of upgrades to 2 pearls was presented where it has been noted that both the external walls, and roof have similar behavior profile, which varies from the glazing. In this example, the 2 pearls combined scenario has 0.0727 MWh less annual conduction gain than the sum of the individual scenarios. For the combined solutions, the savings for the overall building were significant and were estimated at 18.90% and 22.12% for the 1 pearl and 2 pearls upgrades respectively.

The feasibility study indicated that the most feasible refurbishment solution for the building prototype of 1980s is for 2 pearls glazing upgrade, where 9 years payback period could achieve savings of 164.2157 MWhe of annual electricity consumption. However, it was noted that the highest savings for the combined solution in the case of 2 pearls upgrades would return its capital cost in around 16 years. It is important to highlight – within this context- that the payback period calculations excludes the savings in government electricity cost subsidies, evaluation of building envelop climatic performance upgrade such as humidity resistance, air tightness, aesthetical appearance, as well as future increases in the cost of electricity. It is expected that once all the

benefits are quantified, the SPP analysis will result in reasonable timeframe for the owners to recoup their initial investment cost.

Finally, the research is concluded by magnifying the annual reduction in electricity consumption to represent the savings across Abu Dhabi. For the 1980s, the implementation of a combined retrofitting scenario which targets upgrading the external walls, roof, and glazing to 2-5 pearls rating requirements; is estimated to achieve annual reduction in electricity consumption of 18,433 MWeh/yr. Whereas, the refurbishment of the most economically feasible solution to upgrade the building glazing to 2-5 pearl rating standards, can achieve an overall reduction for the same buildings estimated at 12,213.97 MWeh/yr. CO2 emissions reduction for the combined solution of 2 pearls rating is estimated at 9,530,968.13 KgCO2/yr.

Moreover, an indication of the typical building prototype for the 1990s has been provided, based on the building characteristics concluded from the literature review. Since the buildings in the 1990s have a predominant feature of high ratio of external glazing –if not fully glazed- the refurbishment was targeted for the glazing elements only. Based on the initial estimates, the overall savings for Abu Dhabi for the 1990s buildings represented by the sample floor are estimated at 28,598.86 MWeH/yr and 20,152.07 MWeh/yr for the 2 pearls and 1 pearl rating respectively.

6.1 **RECOMMENDATIONS FOR FUTURE RESEARCH**

Further to this research, there are several opportunities for continuation and problems to be further investigated. With regards to potential of energy savings, cooling load reduction, and CO2 emissions reduction, further investigations could be conducted on the building prototype representative of the period from 1908 to 1989. The investigations could target refurbishment strategies of various types of glazing including triple-glazing panels. Also, a combination between active and passive retrofitting strategies could be investigated. As highlighted during the research, there is a major difference between the HVAC systems and their efficiency for those used in 1980s and 1990s. Further research could target the potential savings due to replacement of the

HVAC system.

Moreover, further studies could be conducted on an existing building representative of the 1990s for comprehensive analysis of the cooling loads, energy, and CO2 emissions through implementation of various retrofitting strategies.

On another level, the research could be used as a basis to investigate formation of retrofitting policies and regulations similar to that established for the US Green Building Council as LEED for Existing Buildings. Since the Abu Dhabi Urban Planning Council has already established the Estidama Pearl Rating System, there is great benefit to form a rating system for existing buildings. The formation of standards, regulations, and policies for upgrades in the existing building thermal performance need to be further investigated from a regulatory framework perspective.

Another aspect that could be further investigated is the construction constraints and opportunities, implementation strategies, and other constructability aspects of the retrofitting strategies. Such investigations shall identify any potential risks associated with the retrofitting strategies suggested in this research.

Finally, detailed economic feasibility study could be conducted to evaluate the additional benefits associated with building envelope refurbishment inclusive of humidity resistance, air tightness, sound insulation, building durability, etc. Also, parameters such as governmental subsidies and inflation rates shall be taken into consideration to provide a better picture of the payback period versus the identified benefits of the building retrofitting.

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<u>1XUxEq9Q7OmnDAGAGiynZNRkLWMpFL7rmMjc3LiV0wwrqd0oPcHW4PVbtmjgzb&sig=AHIEtbTmzbL</u> 8rI9SjMhdfwu8GNDJZnCDow

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APPENDIX A - LITERATURE REVIEW SUPPORTING DATA

Table A36 Consumption of Electricity per Region in MWh. (Source: SCAD 2012, p. 67)

| Year | Total | Abu Dhabi | Al Ain | Al Garbia |
|------|------------|----------------------|-----------|-----------|
| 1972 | 223,314 | 198,741 | 24,573 | 0 |
| 1973 | 336,242 | 299,242 | 37,000 | 0 |
| 1974 | 428,537 | 377,537 | 51,000 | 0 |
| 1975 | 629,350 | 540,281 | 89,069 | 0 |
| 1976 | 845,072 | 710,324 | 134,748 | 0 |
| 1977 | 1,219,023 | 1,029,651 | 189,372 | 0 |
| 1978 | 1,377,251 | 1,121,522 | 255,729 | 0 |
| 1979 | 1,878,240 | 1,499,011 | 379,229 | 0 |
| 1980 | 2,376,367 | 1,846,765 | 529,602 | 0 |
| 1981 | 2,870,532 | 2,205,829 | 664,703 | 0 |
| 1982 | 3,426,085 | 2,557,424 | 868,661 | 0 |
| 1983 | 3,807,402 | 2,848,166 | 959,236 | 0 |
| 1984 | 4,148,898 | 3,065,922 | 1,082,976 | 0 |
| 1985 | 4,523,421 | 3,348,037 | 1,175,384 | 0 |
| 1986 | 5,490,985 | 4,139,064 | 1,351,921 | 0 |
| 1987 | 5,950,056 | 4,492,728 | 1,457,328 | 0 |
| 1988 | 6,464,509 | 4,863,535 | 1,600,974 | 0 |
| 1989 | 6,830,833 | 5,096,929 | 1,733,904 | 0 |
| 1990 | 6,605,690 | 4,670,690 | 1,935,000 | 0 |
| 1991 | 6,724,047 | 4,636,047 | 2,088,000 | 0 |
| 1992 | 7,079,949 | 4,881,949 | 2,198,000 | 0 |
| 1993 | 7,787,185 | 5,462,137 | 2,325,048 | 0 |
| 1994 | 8,351,385 | 5,906,447 | 2,444,938 | 0 |
| 1995 | 9,074,210 | 6,212,210 | 2,862,000 | 0 |
| 1996 | 10,346,470 | 7,201,470 | 3,145,000 | 0 |
| 1997 | 10,883,760 | 7,462,760 | 3,421,000 | 0 |
| 1998 | 16,104,368 | 10,810,768 | 4,181,580 | 1,112,020 |
| 1999 | 17,507,862 | 11,515,152 | 4,741,220 | 1,251,490 |
| 2000 | 19,128,380 | 12,158,360 | 5,442,130 | 1,527,890 |
| 2001 | 20,648,660 | 12,963,260 | 5,983,830 | 1,701,570 |
| 2002 | 22,398,850 | 14,178,270 | 6,295,720 | 1,924,860 |
| 2003 | 23,289,990 | 14,924,760 | 6,506,630 | 1,858,600 |
| 2004 | 24,365,800 | 15,620,760 | 6,569,450 | 2,175,590 |
| 2005 | 25,423,862 | 16,158,411 | 6,849,131 | 2,416,320 |
| 2006 | 27,323,017 | 17,376,073 | 7,091,412 | 2,855,532 |
| 2007 | 29,342,214 | 18,577,267 | 7,528,700 | 3,236,247 |
| 2008 | 31,480,854 | 19,803,499 | 7,881,926 | 3,795,429 |
| 2009 | 34,716,166 | 22,062,262 | 8,474,342 | 4,179,562 |
| 2010 | 39,173,140 | 24,850,010 | 9,081,380 | 5,241,750 |
| | | 1972 to 2010 net cha | inge, % | |
| | 17,442 | 12,404 | 36,857 | _ |

Sources:

Abu Dhabi Water and Electricity Company (ADWEC) (2000-2009)

Abu Dhabi Water and Electricity Authority (ADWEA) (1994-1999)
 Department of Water and Electricity (1972-1993)

Notes:

2002-2003 AI Ain and AI Ghrabia figures are estimates
 Consumption include internal Electrical Consumption by Power Stations and Technical Losses Through the Network

| Maran | D. Hilling | Harris an | Pe | ermits Issued by Regi | on |
|-------|------------|-----------|-------|-----------------------|--------|
| Year | Buildings | Housing | Total | Abu Dhabi | Al Ain |
| 1968 | 3,007 | 6,625 | 53 | 29 | 24 |
| 1969 | 4,540 | 10,001 | 135 | 71 | 64 |
| 1970 | 6,072 | 13,378 | 55 | 27 | 28 |
| 1971 | 7,604 | 16,754 | 117 | 74 | 43 |
| 1972 | 9,136 | 20,130 | 222 | 162 | 60 |
| 1973 | 10,668 | 23,506 | 325 | 232 | 93 |
| 1974 | 12,200 | 26,883 | 552 | 378 | 174 |
| 1975 | 13,736 | 30,259 | 787 | 488 | 299 |
| 1976 | 16,872 | 37,117 | 2,310 | 1,433 | 877 |
| 1977 | 20,007 | 43,975 | 2,242 | 1,475 | 767 |
| 1978 | 23,074 | 50,743 | 2,758 | 1,720 | 1,038 |
| 1979 | 41,905 | 75,447 | 3,748 | 1,619 | 2,129 |
| 1980 | 46,738 | 84,416 | 4,188 | 2,042 | 2,146 |
| 1981 | 46,746 | 88,683 | 4,590 | 2,468 | 2,122 |
| 1982 | 48,988 | 92,949 | 5,130 | 2,620 | 2,510 |
| 1983 | 51,230 | 97,216 | 4,999 | 2,808 | 2,191 |
| 1984 | 53,473 | 101,482 | 4,636 | 2,263 | 2,373 |
| 1985 | 55,635 | 105,749 | 4,457 | 2,380 | 2,077 |
| 1986 | 55,001 | 85,532 | 7,854 | 2,331 | 5,523 |
| 1987 | 54,367 | 90,865 | 5,760 | 2,946 | 2,814 |
| 1988 | 53,733 | 96,198 | 5,301 | 3,315 | 1,986 |
| 1989 | 53,099 | 101,532 | 7,918 | 3,423 | 4,495 |
| 1990 | 52,465 | 106,865 | 5,064 | 3,196 | 1,868 |
| 1991 | 51,831 | 112,199 | 4,862 | 3,062 | 1,708 |
| 1992 | 51,194 | 117,532 | 5,989 | 3,787 | 2,087 |
| 1993 | 70,431 | 141,514 | 5,457 | 3,482 | 1,777 |
| 1994 | 73,483 | 147,657 | 6,028 | 4,633 | 1,061 |
| 1995 | 76,419 | 153,800 | 5,505 | 4,036 | 1,162 |
| 1996 | 83,080 | 180,354 | 5,925 | 4,119 | 1,611 |
| 1997 | 86,358 | 187,338 | 5,897 | 4,224 | 1,501 |
| 1998 | 89,636 | 194,321 | 7,844 | 5,234 | 2,476 |
| 1999 | 92,914 | 201,305 | 9,568 | 7,348 | 2,096 |
| 2000 | 96,192 | 208,289 | 7,366 | 5,677 | 1,577 |
| 2001 | 98,917 | 215,273 | 6,536 | 4,241 | 2,164 |
| 2002 | 103,523 | 213,368 | 7,513 | 4,994 | 2,381 |
| 2003 | 108,202 | 223,329 | 7,499 | 5,073 | 2,293 |
| 2004 | 112,882 | 233,290 | 7,606 | 5,327 | 2,144 |
| 2005 | 117,254 | 243,251 | 8,555 | 5,947 | 2,608 |
| 2006 | 126,817 | 248,686 | 9,631 | 6,055 | 3,576 |

Table A2 Key Statistics of Construction Activities (Source: SCAD 2012, p. 69)

| 2007 | 136,380 | 254,121 | 6,272 | 3,316 | 2,956 |
|-------------------------------|-------------------------|------------------|-----------------|----------------------|-------------------|
| 2008 | 145,943 | 259,556 | 6,603 | 4,129 | 2,474 |
| 2009 | 155,506 | 264,991 | 12,623 | 9,674 | 2,949 |
| 2010 | 165,072 | 270,428 | 11,532 | 8,155 | 3,377 |
| | | 1968 to 2010 | net change, % | | |
| | 5,389 | 3,982 | 21,782 | 28,021 | 14,148 |
| Sources for | r building and | | Sources for n | umber of permits: | |
| nouses. | | | Sources for the | inder of permits. | |
| Building | and housing unit Cer | nsus (1995-2001) | Department | t of Municipality ar | nd Agriculture (2 |
| Central S | Statistical Administrat | tion (1985) | 🛠 Abu Dhabi N | Aunicipality and Al | Ain Municipalit |
| Populati | on and housing censu | us (1980) | 🛠 Abu Dhabi N | /lunicipality (1975) |) |
| | | | | | |

Building and housing unit surveys (1972,1992)

Department of Town Planning, Abu Dhabi (1968-1974)

Note: Figures for buildings and housing for the period 2006 - 2009 estimated based on the primary result of the frame update project conducted by SCAD in October 2010

Table A3 Comparison of 20 simulation software according to their capabilities (Source: Crawley et al 2005, p. 21)

ABBREVIATIONS IN THE TABLES

- Х feature or capability that is available and in common use (e.g. a mature facility, well supported in documentation/interface/examples)
- Р feature or capability that is partially implemented (e.g., it addresses part of an issue, does not yet fully represent the underlying physics or is a work-in-progress)
- 0 optional feature or capability that is not included in the standard distribution or requires additional payment and/or a download.
- R optional feature or capability that is intended for research use (e.g., links to experimental data, validation tests, and options to invoke alternative correlations or modify the underlying solution technique)
- E feature or capability that requires considerable domain expertise or knowledge of the underlying models (e.g., computational fluid dynamics, 2D/3D conduction, fire evacuation)
- Τ feature or capability that requires input data that can be difficult to obtain (e.g., parameter estimates from optimization, difficult to obtain curve fits, no manufacturer data available, little or no research has been done to characterize model coefficients)

Table A4 Comparison of 20 simulation software according to their capabilities (Source: Crawley et al 2005, p. 26)

| Table 3 Building Envelope, Daylighting and Solar | BLAST | BSim | DeST | DOE-2.1E | ECOTECT | Ener-Win | Energy Express | Energy-10 | EnergyPlus | eQUEST | ESP-r | НАР | HEED | IDA ICE | IES <ve></ve> | PowerDomus | SUNREL | Tas | TRACE | TRNSYS |
|---|-------|----------|------|-----------------|-----------------|----------|-------------------|-----------|------------|--------|-----------------|-----|-----------------|-----------------|---------------|--------------|--------|-----------------|-------|-----------------|
| Solar analysis | Ī | | | | 1 | | | | | | | | [| | | | Ī | | | |
| Beam solar radiation reflection from outside and inside window reveals | | x | Р | | x | | | | x | | | | | | | | | | | x |
| Solar gain through blinds accounts for different transmittances for sky and ground diffuse solar | | | x | | 3 | x | | | x | | | | | | х | | | x | | x |
| Solar gain and daylighting calculations account for inter-reflections from external building components and other buildings | | P | | | x | | | | x | | X ⁵⁷ | | | | x | Р | | x | | X ⁵⁸ |
| Creation of optimized shading devices | | | | | Х | | | | | | | | | | | | | | | |
| Shading surface transmittance | х | | | P | X | | X | | X | X | | | | | х | | | X ⁹⁵ | | 1 |
| Shading device scheduling | х | X | X | P | X | | | | X | X | | | X ⁸³ | X | X | P | х | X | X | X |
| User-specified shading control | | X | X | P | X ³⁹ | | | | X | | X ⁶⁰ | | X ⁸³ | X | X | | | X | х | X |
| Bi-directional shading devices | | | P | | 3 | | | | X | | X ⁶¹ | | | X | х | | | X | х | X |
| Shading of sky IR by obstructions | | | X | Х | 3 | Х | | | X | X | | | | | X | | | X | | X |
| Insolation analysis | | | | | | | | | | | | | | | | | | | | |
| time-invariant and/or user stipulated⁶² | х | | | P ⁶³ | | | | | X | P | X | | х | | | | X | | | X |
| distribution computed at each hour⁶⁴ | х | | | X ⁶⁵ | | | | | | X | X | | | | х | | | | | E I66 |
| distribution computed at each timestep⁶⁷ | | | | | | | | | X | | | | | | х | | | | | E I66 |
| Beam solar radiation passes through interior | | v | P | | x | | | | v | X68 | | | | V ⁶⁹ | v | P | | v | | v |
| windows (double-envelope) | | ^ | 1 | | <u>^</u> | | | | <u>^</u> | 1 | | | | ^ | ^ | ¹ | | 1 | | ^ |
| Track insolation losses (outside or other zones) | | | | | | | | | | | X | 1 | | | X | | | | | 1 |

⁷⁷ Does not include specular reflection from obstructing bodies or diffuse shading. Insolation calculation for any shape of room and includes surfaces within the room.
 ⁸⁷ No specular reflection
 ⁹⁰ Using embedded scripting engine allows a function to be called each time-step to change shading parameters or shading masks.
 ⁹⁶ For two blind positions and daylighting accounted for in light switching for multiple sensors and circuits per thermal zone.
 ⁹⁶ Using reflection
 ⁹⁷ Using embedded scripting engine allows a function to be called each time-step to change shading parameters or shading masks.
 ⁹⁶ For two blind positions and daylighting accounted for in light switching for multiple sensors and circuits per thermal zone.
 ⁹⁶ Usi surfaces
 ⁹⁶ Use refines where direct sunlight (insolation) falls in a room, e.g., put 45% on the floor and 55% on the back wall or the application distributes insolation in the same pattern for all hours.
 ⁹⁷ There invariant except for sunspaces, where solar distribution is calculated hour-by-hour
 ⁹⁶ At each hour, application calculates the distribution of direct sunlight (insolation) entering via each window (at run-time or calculated and stored for retrieval at run time).
 ⁹⁷ Direct solar radiation impinging on surfaces is calculated every hour, but the obstructed fraction due to shading surfaces is calculated hour-by-hour every two weeks.
 ⁹⁶ Must be calculated outside the building model and requires additional data.
 ⁹⁷ At each timestep, application calculates the distribution of direct sunlight (insolation) entering via each window (at run-time or calculated and stored for retrieval at run time).
 ⁹⁶ For sunspaces (attriums) only, not used for double envelope buildings
 ⁹⁶ With separate add-in for double sheet facades

Table A5 Comparison of 20 simulation software according to their capabilities (Source: Crawley et al 2005, p. 27)

| Table 3 Building Envelope, Daylighting and Solar | BLAST | BSim | DeST | DOE-2.1E | ECOTECT | Ener-Win | Energy Express | Energy-10 | EnergyPlus | eQUEST | ESP-r | HAP | HEED | IDA ICE | IES <ve></ve> | PowerDomus | SUNREL | Tas | TRACE | TRNSYS |
|--|-------|------|------|----------|-----------------|----------|-------------------|-----------|------------|-----------------|-----------------|-----|-----------------|---------|---------------|------------|--------|-----|-------|-----------------|
| Advanced fenestration | | | | | | | | | | | | | | | | | | | | |
| Controllable window blinds | | X | X | X | X ⁷⁰ | | X | | Х | X | Х | | Х | Х | Х | | Х | Х | ' | X |
| Between-glass shades and blinds | | | X | X | X | | | | x | X | X71 | | | X | X | | | X | | X |
| Electrochromic glazing | | | | | X72 | | | | X | X | X | | | X | | | | | ' | E ⁷³ |
| Thermochromic glazing | | - 75 | | _ | X | | | | | 76 | X | | | X | | | 1 | | _ | E's |
| Datasets of window types" WDEDOW 6 1 1 1 4 | | P" | X | P | X | | Р | | X | X ⁷⁶ | P" | X'* | X'' | X | X | | | X | Р | X |
| WINDOW 5 calculations WINDOW 4.1 data immediate | v | | | 776 | 3 | | | | x | X76 | v | | | | | | 7780 | | v | X |
| WINDOW 4.1 data import Dirt correction factor for glass solar and visible | ^ | | | • | | | | | | л | ^ | | | | | | л | | ^ | ^ |
| transmittance | | | E | P | X | | | | X | P | | | | Х | | | | | ' | E ⁷³ |
| Movable storm windows | | | x | | x | | | | x | | X ⁸¹ | | | x | x | | | x | ' | x |
| Bi-directional shading devices | | | P | | 3 | | | | x | | X ⁶¹ | | | x | x | | | x | x | x |
| Window blind model⁸² | | | Х | | Х | | | | х | X | X ⁶⁰ | | X ⁸³ | | X | | | | ' | x |
| User-specified daylighting control | | X | X | | X ⁸⁴ | | | | X | | X ⁶⁰ | | X ⁸³ | X | X | | | X | X | X |
| Window gas fill as single gas or gas mixture | | | X | | X | | | | X | | X | | | | Х | | | Х | | X |
| General Envelope Calculations | | | | | | | | | | | | | | | | | | | ' | |
| Outside surface convection algorithm | | | | | | | | | | | | | | | | | | | ' | |
| BLAST/TARP | X | | | | 3 | | | | X | | | | | | | | | | Х | |
| DOE-2 | | | | X | 3 | | | | X | X85 | | | | | | | | | x | |
| MoWiTT | | | | | 3 | | | | X | | X | | | | | | | | X | |
| ASHRAE simple | | 1 | 1 | 1 | 3 | | 1 | | X | 1 | 1 | | X | 1 | | | 1 | | | 1 |

⁷⁰ Using embedded scripting engine allows a function to be called each time-step to change glass parameters based on analysis results.

⁷¹ Using embedded scripting engine allows a function to be called each time-step to change glass parameters based on analysis results.
 ⁷¹ Multiple representations possible: as part of a constructions optical properties, as solar obstructions associated with the zone or as explicit surfaces with full treatment of convection and radiation exchange.
 ⁷² With freely available electrochromic/thermochromic plug-in developed at Welds School of Architecture.
 ⁷³ By applying a correction factor outside the building model (Type-56) or defining several windows in WINDOW 5 and switching from one to the other during simulation based on conditions or control signal.
 ⁷⁴ Conventional, reflective, low-E, gas-fill, electrochromic, and WINDOW-S layer-bu-layer custom glazing description
 ⁷⁸ Extensible window library with possibility of defining individual 3rd order polynomial transmission versus angle of incidence curves.
 ⁷⁰ Window 4 single band calculation for layer-by-layer descriptions or accepts Window 5 multiband output for composite window descriptions.
 ⁷⁸ Window 4 single band calculation for layer-by-layer descriptions or accepts Window 5 multiband output for composite window descriptions.
 ⁷⁰ Window 5 glazing and window assembly defined; performance calculation based on Window 4.
 ⁷⁰ Chechlicit to the store three on gas and window may call data invert for up to 25 windows.

⁷¹ Configuration of window glazing and window assembly defined, performance calculations based on Window 4.
 ⁷⁹ Checklist with 11 glazing types and two frame types, or advanced numerical data input for up to 25 windows.
 ⁸⁰ Window 4.1, 5.1 and 5.2 data import capabilities
 ⁸¹ Via general facility for substituting constructions thermophysical and optical properties during simulation.
 ⁸² Slat-type shading devices such as Venetian blinds coupled to daylighting, with movable slats and associated slat-angle controls
 ⁸⁴ Italiage controls reading devices or interior window shades for passive heating/cooling/daylighting
 ⁸⁴ Using embedded scripting engine allows a function to be called each time-step to change shading parameters or shading masks.
 ⁸⁵ Uses combined MoWiTT, TARP and ASHRAE formulations for various portions

Table A6 Comparison of 20 simulation software according to their capabilities (Source: Crawley et al 2005, p. 28)

| Table 3 Building Envelope, Daylighting and Solar | BLAST | BSim | DeST | DOE-2.1E | ECOTECT | Ener-Win | Energy Express | Energy-10 | EnergyPlus | eQUEST | ESP-r | НАР | HEED | IDA ICE | IES <ve></ve> | PowerDomus | SUNREL | Tas | TRACE | TRNSYS |
|---|-------|-------------|-------------|------------------|--|-------------|-------------------|-------------------|---|------------------|---|------------|--------|----------------------|---|------------|--------|--|--------|-------------|
| Ito, Kimura, and Oka (1972) correlation User-selectable Inside radiation view factors Radiation-to-air component separate from detailed convection (exterior) Air emissivity/radiation coupling | | x x | x x x | | 3 3 3 | | | | X ⁸⁶ X X | x x | X X X X | | | X X X X | x x x x | х | P X | x x x | X P | x x |
| Sky model • Isotropic ¹⁷ • Anisotropic ¹⁹ • User-selectable | x | x x | x | x | x x x | x | x | x | x | x | X X X | X88 X90 | x | X X ⁹¹ | X X X | x | x | x | x | x x x |
| Daylighting illumination and controls Interior illumination from windows and skylights Stepped or dimming electric lighting controls ⁵⁰ Glare simulation and control Geometrically and optically complex fenestration systems using bidirectional transmittance Radiosity interior light interreflection calculation Daylight illuminance maps Tubular daylighting devices ⁵⁷ | | x x x | x | x x x | X ³ P ³ X X 3 | x x x | | X ⁹² X | X X X I X X X X X | X X X | X X ⁹⁴ X ⁹⁴ X ⁹⁴ X X ⁹⁶ X ⁹⁶ | | X X | x x x x | X X X X X X X X X | | | X X X ⁹⁵ X ⁹⁵ X ⁹⁵ X ⁹⁵ | X X | x |
| Movable/transparent insulation | X | X | Р | X | 3 | | | | Х | | X | | X98 | Х | Х | | P | | | X |
| Zone surface temperatures ⁹⁹ | X | Х | E | P ¹⁰⁰ | X | X | | | X | X ¹⁰¹ | X ¹⁰² | | | Х | Х | Х | Х | X | Х | Х |

⁴⁶ Can specify different correlations by surface type (e.g. all exterior windows)
 ⁴⁷ Uniform solar radiation and illumination distribution
 ⁴⁸ For energy simulation calculations
 ⁴⁹ For energy and advactulations
 ⁴⁰ Artomatic diffuse solar radiation and illumination vary with sun position
 ⁴⁰ For design day calculations
 ⁴¹ Altomatic diffuse solar radiation and illumination vary with sun position
 ⁴² For energy and Xondraijev
 ⁴³ LSNL split-flux daylighting model
 ⁴⁴ Through a link with Lumen Designer
 ⁴⁵ Resolution can be increased via use of Radiance to define shelf properties and light sensor characteristics. Tubular devices require combined Radiance & surfaces description.
 ⁴⁷ Automatic operable night time window insulation
 ⁴⁹ Wall, window, door, floor, ceiling, roof
 ⁴¹⁰⁰ Reverse calculation from heat flows (module added by EMPA)

| Table A7 C | omparison o | of 20 simulation | ı software a | according to | their ca | pabilities (| Source: | Crawlev | et al 2005. | p. 2 | 9) |
|------------|----------------------|------------------|---------------|---------------|----------|--------------------|------------|---------|-------------|------|-----|
| | Care Personal Care 1 | | A DOLUTION OF | needs anny eo | | Deelo ana en elo (| NO GAL COV | ~~~~, | | P | - 1 |

| Table 3 Building Envelope, Daylighting and Solar | BLAST | BSim | DeST | DOE-2.1E | ECOTECT | Ener-Win | Energy Express | Energy-10 | EnergyPlus | eQUEST | ESP-r | HAP | HEED | IDA ICE | IES <ve></ve> | PowerDomus | SUNREL | Tas | TRACE | TRNSYS |
|--|-------|------|--------|----------|-------------|----------|-------------------|-----------|----------------------------|--------|------------------|-----|------|-------------|---------------|---|-------------|-----|-------|---|
| Airflow windows | | | | | Х | | | | Х | | X ¹⁰³ | | | 0 | X | Х | Х | Х | | Х |
| Surface conduction 1-dimension 2- and 3-dimension | x | x | X P | x | x | x | x | x | x x | x | X R I | x | x | x o | x | x | x | x | x | x |
| Ground heat transfer ASHRAE simple method ¹⁰⁴ 1-dimension 2 - and 3-dimension slabs 2 - and 3-dimension basements | Р | x | X P | Р | X 3 3 | x | x | x | X X ¹⁰⁶ X | x | X R R | x | x | X O O | x | X O ¹⁰⁷ O ¹⁰⁷ | X R R | x | Р | X O ¹⁰⁵ O ¹⁰⁵ O ¹⁰⁵ |
| Variable thermophysical properties | | | | | Х | | | | | | I | | | Х | | Х | | | | |
| Phase change materials | | | 0 | | | | | | | | I | | | 0 | | R | Х | | | E |
| Building integrated photovoltaic system accounts for heat removed from surfaces layers which have defined electrical characteristics | | x | | | 3 | | | | x | x | x | | | | | Р | | | | E |

¹⁰¹ User selectable in some versions
 ¹⁰² Also temperatures within constructions as well as full energy balance at each surface.
 ¹⁰³ As an additional zone with flow network or CFD domain
 ¹⁰⁴ ASHRAE (2001a)
 ¹⁰⁵ Through additional component (optional TESS libraries)
 ¹⁰⁵ 2.D and 3-D ground calculations for basements and slabs using auxiliary programs.
 ¹⁰⁷ Through a link with the Solum software (Santos et al. 2003)

APPENDIX B – EXISTING BUILDING EMPORIS DATABASE

 Table B1 List of Existing Buildings in Abu Dhabi and their properties. (Source: EMPORIS 2013)

| Archited: Wimberly Allisom Tong & Goo | | 2005 | 2003 | 00 | 70.85 m | 70.85 m | Abu Dhabi | | Corniche Road | shops, restaurant, fitness center | hotel | postmodern | concrete | high-rise building | 2005 71 m | EmiratesPalaace | |
|--|------------|-------------|-----------------|-----------------------------|---------------------------------------|-------------|------------------------|-------------------|------------------------|--------------------------------------|--|--------------------------------|---|--|--------------|--|---------|
| | - | 1999 | | 17 | 87.00 m | | Abu Dhabi | 8 | Fotouh Al Khair Centr | | rental apartments | postm odern | concrete | high-rise building | 1999 87 m | Fotouth Al Khair Centre III | 70 |
| | | 1999 | | 17 | 87.00 m | | Abu Dhabi | | Fotouh Al Khair Centr | | rental apartments | postmodern | concrete | high-rise building | 1999 87 m | Fotouh Al Khair Centre II | ræ. |
| | | 1999 | | 22 | 87.00 m | | Abu Dhabi | | Fotouh Al Khair Centro | | rental apartments | postmodern | concrete | high-rise building | 1999 87 m | Fotouh Al Khair Centre I | |
| 3 | | | | 24 | 89.92 m | 89.92 m | Abu Dhabi | | | | | | | high-rise building | 90 m | Abu Dhabi National Oil Company Building | m - |
| Architect: Nikken Sekkei Ltd, Leo A. Daly | | | | 28 | 93.00 m | 93.00 m | Abu Dhabi | 9TS | Zadco and Gasco Towe | | | | | high-rise building | 93 m | GASCO Tower [Zadco and G asco Towers] | |
| Daly | | | | 20 | 93.00 m | 93.00 m | Abu Dhata | IS | Zadco and Gasco Towe | | | | | high-rise building | 93 m | ZADCO Tower [Zadco and Gasco Towers] | IN: |
| avaluate William Valler That I an A | | | | | 100.00 m | | Abu Dhabi | | | | | | | ovservation towe | 100 m | Marina Mall Viewing Tower | 1 |
| Archited: MZ Architeds | | 2010 | | 23 | 110.03 m | | Abu Dhabi | | | | commercial office | te structural expressionism | composi structure | skyscraper | 2010 110 m | Alder Headquarters | 15 |
| lighting consultant, concrete supplier | | | | | 115.00 m | 115.00 m | Abu Dhabi | | | | mosque | islamic | | mosque | 115 m | Mosqu | |
| | | 2004 | 2001 | 29 | 117.00 m | | Abu Dhabi | | ADNOC Headquarters | | | postm odern | | skyscraper | 2004 117 m | Tower | 0 |
| | | 2004 | 2001 | 29 | 117.00 m | | Abu Dhabi | | ADNOC Headquarters | | | postmodern | a de ser a El ser a de s | skyscraper | 2004 117 m | Abu Khabi Oil Refining Company Tower Abu Dhabi Gas Processing Company | h. h. |
| Architect: N orr Group Consultants International Ltd, Carlos Ott Architect. | | 1996 | | 21 | 120.00 m | | Abu Dhabi | | | | commercial office | | 1 | skyscraper | 1996 120 m | Urion National Bank 2 | 12 |
| Architect: Arthur Enicksom Architectural Corporation, Norr Group Consultants International Ltd. | | 1993 | | 32 | 120.70 m | 120.70 m | Abu Dhabi | 8 | Khalifa Bin Zayed Stre | | hotel | modernism | | skyscraper | 1993 121 m | Le Royal Meridien Hotel | |
| | | | | | 138.00 m | 138.00 m | Abu Dhabi | | | | | | | mast (wired) | 138 m | Etisal at Radio Mast | -1-1-1 |
| | | 2012 | 2009 | 29 | 145.00 m | | Abu Dhabi | | Al Bahr Tower | | governmental office | 8 | composit | skyscraper | 2012 145 m | Al Bairr Tower 2 [Al Bairr Towers] | 5 |
| | | 2012 | 2009 | 29 | 145.00 m | | Abu Dhata | | Al Bahr Tower | | governm ental office | 8 | composi structure | skysoraper | 2012 145 m | Al Bair Tower 1 [Al Bair Towers] | 15 |
| | | 2011 | 2004 | 31 | 145 50 m | 145_50 m | Abu Dhabi | | Capital Plaza | | hotel | postmodern | | skysoraper | 2011 146 m | Capital Plaza Hotel Tow er [Capital Plaza] | 10 |
| | | 2011 | 2004 | 3 | 156 50 m | 156.50 m | Abu Dhabi | | Capital Plaza | | commercial office | postmodern | | skyscraper | 2011 157 m | Capital Plaza Office Tower[Capital Plaza] | To |
| Architect: Adel Al Mojil Engineering Consultant, Carlos Ott Architect | | 2001 | | 27 | 160.00 m | | Abu Dhabi | | Airport Road | | | postmodern | | skysoraper | 2001 160 m | Etisal at Headquarters | 117 |
| Architect: Goettsch Partners, inc. | | 2011 | | 31 | 160.00 m | | 1 Abu Dhabi | Al Maryah Islan | Sowwah Square | | commercial office | | concrete | skyscraper | 2011 160 m | Al Sila Tower [Sowwah Square] | 15 |
| Architect: Goettsch Partners,inc. | | 2012 | | 31 | 160.00 m | | Abu Dhabi | Al Maryah Islan | SowwahSquare | | commercial office | | concrete | skyscraper | 2012 160 m | Al Sarab Tower [Sowwah Square] | |
| Architect: RMJM Dubai | | 2010 | 2008 | 35 | 160.00 m | | Abu Dhabi | | | | office/hotel | | | skyscraper | 2010 160 m | Capital G ate | TE. |
| (Architect: Arkan Architects, (Consultants | | 1994 | | 8 | 164.90 m | 164.90 m | Abu Dhabi | | Corniche Road | | hotel | postmodern | | skyscraper | 1994 165 m | Baymanah Hilton Tower Hotel | |
| Arcinical: Arciniceture & Flammig Group, Add Al Mojil Engineering Consultant, Carlos Ott Architect | = | 2002 | 1999 | 33 | 173.00 m | | Abu Dhata | | Sheikh Khalifa Street | | commercial office | modernism | | skyscraper | 2002 173 m | National Bank of Abu Dhabi Headquarters | 19 |
| Architect: Goettsch Partners, inc. | | 2012 | | 37 | 184.00 m | | Abu Dhabi | Al Maryah Islam | SowwahSquare | | commercial office | | concrete | skyscraper | 2012 184 m | Al khatem Tower [Sowwah Square] | r= |
| Architect: Goettsch Partners,inc. | | 2012 | | 37 | 184.00 m | | Abu Dhabi | Al Maryah Islan | Sowwah Square | | commercial office | | concrete | skyscraper | 2012 184 m | Al Maqam Tower [Sowwah Square] | 15 |
| Architect: Kohn Pedersen Fox Associates | 13 | 2006 | 2001 | 8 | 185.00 m | 185.00 m | Abu Dhabi | | Corrache Street | | commercial office | modernism | concrete | skyscraper | 2006 185 m | Abu Dhai Investment Authority Tower | I. |
| | | 2011 | 2004 | 51 | 210.00 m | | Abu Dhabi | | Capital Plaza | | residental | postmodern | | skyscraper | 2011 210 m | Caraital Plaza Residential Towder | 10 |
| Archited: DBI Design (Pty Ltd) | | 2011 | | 56 | 217 50 m | 217.50 m | Abu Dhabi | | Etihad Towers | | residental | modernism | concrete | skyscraper | 2011 218 m | Etihad Tower 5[Etihad Towers] | 171 |
| Archited: DBI Design (Pty Ltd) | | 2011 | | 61 | 234.00 m | 234.00 m | Abu Dhabi | | Etihed Towers | | residental | modernism | concrete | skyscraper | 2011 234 m | Etihad Tower 4 Etihad Towers] | mr. |
| general contractor | | 2012 | 2007 | 20 | 205 UU m 260 34 m | 260 34 m | Abu Unata Ahu Dhahi | | Philad Tourers | | rescental office | modernism | monorate | droortaper | 2011 260 m | Nation 1 owers residential Fished Trazer 3 [Fished Trazers] | |
| Archited: DBI Design (Pty Ltd) | | 2011 | 1004 | 70 | 277.61 m | 277.61 m | Abu Dhabi | | Etihad Towers | | apartments | modernism | concrete | skyscraper | 2011 270 m | Etihad Tower 1 [Etihad Towers] | and the |
| Architect: DBI Design (Pty Ltd) | | 2011 | 2007 | 79 | 305.30 m | 305.30 m | Abu Dhabi | | Etihad Towers | | residental hotel/servical | modernism | concrete | skyscraper | 2011 305 m | Etihad Tower 2 [Etihad Towers] | |
| Architect: A2so4 Architecture,RW Armstrong | 0 m 27 | 2010 2.7 | 2006 | 74 | 310.00 m | 310.00 m | Abu Dhabi | Shams | The gate | shopping center, fitness center | commercial office, rental apartments | postmodern | concrete | skyscraper | 2010 310 m | Sky Tower | 1 74 |
| NG ST | apricupi | End be | Start | rioors (above ground) | neign (Architectural) in meters | in meters | -uity | Lone | Complex | Secondary Use | Fmnary Use | a Architectural Style | Material | Building 1 ype | Y ear Height | blanging Name | |
| Involved Companies | The sector | A TTTTTT BI | echracal L) ata | 1 | A TT | A THAT I AN | ig . | Emirate of Abu Dh | Location # | 20 | US | aneral | acture in Ge | The state of the s | Walter House | Identification | ar- |

| Al Nuwais Building I [1999 | Al Nuwais Building III 1999 | Al Nuwais Building II [1999 | Al Maha Rotana States 2002 | ADMO, OPCO & ADGAS Tower II | Abdulla Al Musar Building 1993 | Al-Muharby Building [1997 | Buti Bin Ahmad Building [1999 | Tower Sector E-07, Plot C-42 | | Pulding | Nizar Almed Al Obaidly Tower | Alia Tower | Benkaram Tower | Etisals Tower 1986 | Bara Yas Tower 1988 | The Six Towers 2 [The Six Towers] 2005 | The Six Towers 1 [The Six Towers] 2005 | Abu Dhabi World Trade Center Building | Zayed Military City Tower X | Zayed Military City Tower IX | Zayed Militæry City I ower v 11 Zared Militæry City Tower V 11 | Zayed Military City Tower VI | Zayed Military City Tower V | Zayed Military City Tower IV | Zayed Militæry City Tower III | Zayed Militiary City Tower I Zayed Militiary City Tower II | Abu Dhabi Grand Hotel | Nahda Tower 1998 | Al Ain Tower | Bin Ara Centre | | Grand Millennium Al Wahda 2010 | Infinity Tower 2011 | Marina Heights I 2011 | Marina H a ghts II 2011 | RAK Tower 2011 | Al Maha Tower (2012 | Burnni Biews (2012) | DOI1 | 0110 100 100 100 100 100 100 100 100 10 | Nanna Dute 2012 | Sun Tower 2010 | | Ferreri World Abu Dhabi 2010 4 | |
|----------------------------|-----------------------------|-----------------------------|-------------------------------|-----------------------------|--------------------------------|---------------------------|-------------------------------|-----------------------------------|-------------------------|--------------------|------------------------------|--------------------|--------------------|--------------------------|----------------------------------|--|--|---------------------------------------|-----------------------------|------------------------------|---|------------------------------|-----------------------------|------------------------------|-------------------------------|---|-----------------------|--------------------|--------------------|--------------------|--------------------|--------------------------------|-------------------------------|-----------------------|-------------------------|----------------|---------------------|---------------------|--------------------------|---|-----------------|-------------------------|---------------------------------|---|-------------------------|
| high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | | high-rise building | high-rise building | skyscraper | skyscraper | skyscraper | skyscraper | skusoraper | sa, ysur aper | skysuaper | skystraper | skyscraper | | 45 m hall | |
| | | | | | | | | | | | | | | postmodern | | | | | | | | | | | | | | | | | | | m oderni sm | | | | | III UUBIIII MII | | | | concrete | | steel | and and and and and and |
| | | | hotel | | | commercial office | commercial office | residential | 3 | | | office | | | | residential onice, | residential | | | | | | | | | | | hotel | residential | condominium in e | commercial office, | hotel res | condominium | residential | residential | residential | residential | residential par | readential readential | I ES UEILIAN | readential | residential res | | am usem ent. | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | rcamble | | dential | | | | | | and. | 1 | | | aurant | | | |
| Al Nuwais Buildings | Al Nuvais Buildings | Al Nuwais Buildings | Mohammed Street | Sheikh Ham dan Bin | | | Liwa Street | Sheikh Khalifa Bin Zaye Street | Sector E-07, Plot C-42, | Corniche Road | | | | | Corrache Koad and Luiu Street | The Six Towers | The Six Towers | | | | | | | | | | Khalifa Street | Corriche Road | Mohammed Street | Al Naj da Street | | Hazza Bin Zayed Street | Marina Square | Marina Square | MarinaSquare | MarinaSquare | MarinaSquare | Marina Scillare | anarberannar | a danna comercia | Marina Smiara | Abu Dhabi | The gate District, shams | Y as Island | |
| | | | | | | | | , d | | | | | | | | | | | | | | | | | | | | | | | | | Al Reen Island | Al Reem Island | Al Reem Island | Al Reem Island | Al Reem Island | Al Reem Island | ture ist unear 147 | At Daam Islaud | Al Reem Island | shams At Dasm Toland | | Yas Island | |
| Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhaba | Abu Dhabi | Abu Dhabi | Abu Dhabi | | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhaba | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | | Abu Dhabi | Abu Dhabi Ahu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Ahu Dhahi | A Diam | A C. Divis | Abu Dhah | Abu Dhabi | ! | Abu Dhabi | |
| 114.27 m | 114.27 m | 114.27 m | 122.84 m | 114.27 m | 119.46 m | 119.46 m | 119.46 m | 114.12 m | | 119.46 m | 119.46 m | 124.65 m | 124.65 m | 129.85 m | 129 85 m | 124.05 m | 124.05 m | 116.14 m | 129.85 m | 129.85 m | m C2 671 | 129.85 m | 129.85 m | 129.85 m | 129.85 m | 129 85 m | 139 59 m | 135.04 m | 122.98 m | 129.01 m | | * 11 J J M | 141 90 m | | | | | 111 10 777 | 22 | | | 307.45 m | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 45.00 m | in meters |
| 22 | 22 | 22 | ß | | 123 | 23 | 23 | 23 | | 13 | 23 | 24 | 24 | 25 19 | B | 25 2 | 25 2 | 25 | 25 | 25 | 36 | 20 | 25 | 25 | 25 | 8.6 | 25 | 26 19 | 26 | 26 | | 28 | 3 23 | \$ | 43 | 43 | 43 0 | 45 2 | 3 4 | 5 6 | 5 | 65 Z | | 3 | ground |
| | | | | | | | | 05 | | | | | | ŝ | | 04 | 04 | | | | | | | | | | | 96 | | | | | | | | | 8 | 06 | 0 | | | 107 | | 07 | |
| 1999 | 1999 | 1999 | 2002 | | 1993 | 1997 | 1999 | 2007 | | | | | | 1986 | 1988 | 2005 | 2005 | | | | | | | | | | | 1998 | | | | 2010 | 2011 | 2011 | 2011 | 2011 | 2012 | 2012 | 2011 | 2102 | 2012 | 2010 | | 2010 | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | - | | | | | height(m) |
| 면 2 | 2 12 2 | · 면 2 | 2 | | | | | A | | | | | | 2 2 | 10 | | | | | | | | | | | | | 8 | | | | 0 | | | | | | | | | - | A | 0 | 부분교회 | |
| ngineers | ngineers | ngineers | solution Davis Assolutions Pr | | | | | rchitect: Planar | | | | | | rchitectural Corporation | 1 | | | | | | | | | | | | | onseltent | | | | epa Ltd | rohitent: Cassia & Associates | | | | | | | | | rchitect: RW Arm strong | eagn Architect: Arquitectoraca, | essgi Automett, benny, Automett, enny, Glass supplier: interparie Glas idustrie AG, Interior fit-lut: Depa .d> | |

| | | | | 19 | 58 m | Abu Dhabi 98. | ari YasStreet | 1 | office | | high-rise building | | Al Oteiba Tower |
|--|-----------------|------|----------------|-------------------|--------------|---------------|--|--------------|---------------------------------|----------------|--------------------|----------|--|
| | | | | 19 | 58 m | Abu Dhabi 98. | ari Yas Street | | affice | | high-rise building | | Green House |
| | | | | 10 | 52 m | Ahu Dhahi 198 | vri VasStreet | | office | | high-rise huilding | | A1 V asat Tower |
| | | | | 10 | 109 m | Abu Dhabi 10 | orniche Road | | hotel | | high-rise building | | Hilton Corniche Residence Dediener 949 Hotel |
| | | 1976 | T | 20 | .67 m | Abu Dhaba 11. | | | hotel | | high-rise building | 1976 | Novotel Center Hotel |
| Architect: BTA Architects, Inc. | | 1982 | | 20 | .67 m | Abu Dhabi 11. | 1 Khalidya Street | × | hotel | modernism | high-rise building | 1982 | Hotel InterContinental |
| Architect: Flamar | | 1995 | | 20 | u 88'. | Abu Dhabi 100 | ilam Street | 70 | | | high-rise building | 1995 | Al Wahda Tower |
| | | 1995 | | 20 | m 88 | Abu Dhabi 100 | | | | | high-rise building | 1995 | Rashed Al Dhaheri Building |
| Architect: Arkan Architects, Consultants | | 1996 | 1995 | 20 | .88 m | Abu Dhabi 103 | | | | | high-rise building | 1996 | Mohammed Bin Zaved Building |
| Archited: Dewan Architeds & Engineers | | 1997 | | 20 | 50 m | Abu Dhabi 94 | heikhRashidBin Saeed 1 Maktoum Street | 10.00 | residental | | high-rise building | 1997 | Al Khazraji Tower |
| Aronitect. Canadat Limited | | 2665 | 0.661 | 20 | | ADD DIADO 11 | | | Tertott | posmodern | naga-rise outroang | 1998 | CTOWINE F18Z8 F10761 |
| | | 1998 | 1002 | 20 | m 88. | Abu Dhaba 10. | amdan Street | | | | high-rise building | 8661 | Darwish Bin Karam Tower |
| Engineers | | 1999 | | 20 | 8 H | Abu Dhabi 91 | Johammed Street | | university | modernism | high-rise building | 1999 | Millerium Tower |
| Engineers | | 1999 | | 20 | .88 m | Abu Dhabi 10. | lot C-18, Sector E-6 | 0.50 | | | high-rise building | 1999 | Al Qubais Tower |
| Archited: Dewan Architeds & | | 2002 | 1998 | 20 | 1.38 m | Abu Dhabi 10 | bu Dhabi Trade Certer | el / | residential, ho | modernism | high-rise building | 2002 | Abu Dhabi Trade C enter Tow er IV |
| | | 2002 | 1998 | 20 | .88 m | Abu Dhabi 10. | bu Dhabi Trade Center | hee. | residential, ho commercial d | modernism | high-rise building | 2002 | Abu Dhabi Trade Center Tower III |
| | | | | - | | | | fice, | commercial d | | 9 | | |
| | | 2002 | 1998 | 20 | 38 m | Abu Dhabi 100 | bu Dhabi Trade Center | Hee, | commercial of residential ho | modernism | high-rise building | 2002 | Abu Dhabi Trade Center Tower II |
| | | 2002 | 1998 | 20 | .38 m | Abu Dhabi 101 | bu Dhabi Trade Center | let / | residential, ho | modernism | high-rise building | 2002 | Abu Dhabi Trade Center Tower I |
| | | 2006 | | 20 | 50 m | Abu Dhabi 94. | reet reet | office | residental | concrete | high-rise building | 2006 | Tower Sector E-06, Plot C-02 |
| | | 2006 | | 20 | 50 m | Abu Dhabi 94 | teet) | nts | rental apartme | | high-rise building | 2006 | Tower Sector W-01 Plot C-13 |
| | | | | | | | asfadBinZayed Al | | | | | | |
| | | | | 20 | 88 m | Abu Dhabi 103 | heikh Rashi d Bin Saeed 1Maktoum Street | 5 70 | office | | high-rise building | | Al Ghaith Tower |
| | | | | 20 | 88 m | Abu Dhabi 103 | heikh Rashid Bin Saeed I Maltoum Street | > 10 | affice | | high-rise building | | HSBC Builáng |
| | | | | 20 | 60 m | Abu Dhabi 94. | arnonSquare | 0 | residental | | high-rise building | | Moderna |
| | | | | 20 | m 88. | Abu Dhaba 10: | halifa Bin Zayed Street | * | | | high-rise building | | Liberty Tower |
| Consultants | + | | | 20 | m 88. | Abu Dhabi 10 | | | | | high-rise building | | Ahmed Al Obaidaly Tower |
| Availated Availatertived & Browneering | | | Ī | 20 | 38 m | Abu Dhabi 10. | amdan Street | | | | high-rise building | | Al-Otaiba Tower |
| company | | | | 20 | . 382 m | Abu Dhabi 101 | ani Yas (Najda) Street | | | | high-rise building | | A1 Masaood Tower |
| toroperty management, construction | | 1995 | | 21 | 1.UV m | Abu Dhaba 10. | | | | | hagh-rise building | 1995 | Sheikh Mohammed Building |
| | | 1995 | | 21 | 1.07 m | Abu Dhabi 10 | | fice | commercial of | | high-rise building | 1995 | Sheikha Shamsa Building |
| | | | | 21 | .07 m | Abu Dhabi 105 | 11, Plot No 126 | fice | commercial of | modernism | high-rise building | | Al Khazana Insurance Tower |
| | | | | 21 | 07 m | Abu Dhabi 109 | thu Shreet | | office | | high-rise building | | Elmilein Bank Building |
| | | - | | 21 | 33 m | Abu Dhata 199 | inZayed Stree | | residental | concrete | high-rise building | | Al Dana Tower |
| | | | | | 6 | | uidingn°206, Sultan | 111 7/ | 1 17 | | | | |
| | | | | 21 | 1,07 m | Abu Dhabi 100 | | | | | high-rise building | | Al Hosan Plaza |
| | | | -+ | 21 | 33 m | Abu Dhabi 99. | vaCentre | 4 | residental | | high-rise building | -+ | Liwa Centre Tower III [Liwa Centre] |
| | | | | 21 | 33 m | Abu Dhaba 99 | va Certire | | residental | | high-rise building | - | Liwa Certire Tower II [Liwa Certire] |
| | | | | 21 | 107 m | Abu Dhabi 10. | re Cartra | | - paintent si | | high-rise building | | Hanna Centre Livre Centre Tower I II ivre Centre] |
| | + | 1993 | | 22 | 1.27 m | Abu Dhaba 11- | | | | | high-rise building | 1993 | Ahmed Al Dhairi Building |
| | | 1995 | | 22 | 27 m | Abu Dhabi 11- | halifa Street | 7 | | | high-rise building | 1995 | Dinna Tower |
| Associates,Inc. Taillibert Gulf Environment. Design Architect Khtib & Alami AbuDhati | | 1997 | | 12 | 27 m | Abu Dhabi 114 | | 15 0 0 | commercial d | postmodern | high-rise building | 1997 | Abu Dhabi Marine Operating Company Headquarters |
| Architect: WZMH Architects | | 1998 | | 22 | .16 m | Abu Dhabi 108 | | fice, | residential | | high-rise building | 1998 | Three Sails Tower |
| | beight (m) | End | Start | (tectural) (above | neters (Arch | un un | anno | acontinuario | rinnay ose | Material Style | n Domonia Aba | Bur ma t | |
| Involved C omparies | In the Internet | | Technical Date | 176 | TTAN VICE | nata u | Location in Emirate of Abu Dt | Use | | ure in General | Struct | | Identification |

| Y as Hotel Abu Dhabi | Bin Talmoon Tower | Al Diar Mina Hotel | Golden Tulip Dalma Suites II | Golden Tulip Dalma Suites I | Dew an Commercial Development Tower | Giffin Tower | Ferook International Stationery Building | Al Diar Palm Hotel | Sheikh Zayed Military Hospital | Golden Tulip Dalma Suites Hotel Tower] | Headquarters | Al Rawda Rotana Suites Hotel Ahu Dhahi National Instrance Company | Golden Tulip Dalma States Hotel Tower] | Union National Bank | CrownPrince Tower IV | Crown Prince Lower II | CrownPrince Tower I | The Six Towers 6 | The Six Towers 5 | The Six Towers 4 | The Six Towers 3 | Abu Dhata Comache Residence Hotel | AL Diar Kegency Hotel | Sands Hotel | ADCO Headquarters | Al Muhairy Group Building | ALS ata lower | E-15, PlotsC-51 | Badar Tower | Mohammed Sherife Hussein Building | Khalidya Mali | Sheikh Tahnoon Tower | ARBIFT Building | El dorado Cinem a Buil ding | City Centre | Al Diar Sands Hotel | Sheikha Aysha Birt Ali Building | Bin Ham oodah Tower | Sheraton Residence | BinSubail Building | AlFardan Tower | BinSweedBuilding | bulung Name | Identification |
|---|--------------------|--------------------|------------------------------|-----------------------------|-------------------------------------|--------------------|--|--------------------|--------------------------------|---|--------------------|--|---|---------------------|----------------------|-----------------------|---------------------|--------------------|--------------------|--------------------|--------------------|-----------------------------------|--------------------------------|--------------------|--------------------|---|----------------------------------|--------------------|--------------------|-----------------------------------|--------------------|----------------------|--------------------|-----------------------------|--------------------|---------------------|---------------------------------|--------------------------------|--------------------|--------------------|-----------------------|--------------------|--|-------------------|
| 2009 | | | | | | 1996 | | | | <u>=</u> | | | | 1996 | 1996 | 1990 | 1996 | 2005 | 2005 | 200.5 | 2005 | - | 1661 | | 1998 | 1998 | | | | 1995 | 1998 | 2002 | | | | | | | 1772 | 1993 | 1995 | | i en hegi | |
| high-rise foulding | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | gunnarise oundand | high-rise building | high-rise building | high-rise building | ingh-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | high-rise building | t buttang type Smutrura Material | Structure in Gene |
| Instel | residential | hotel | | | | | office | hotel | hospital | hotel | | hotel | hotel | | | | | residential | residential | residential | residential | inotel | notei | hotel | | residential, mercantile | moderria sm commercial office | | | residental | | commercial office | commercial offi | commercial offi | commercial office | hotel | | | | | residental | residential | Style | |
| | shopping certer | | | | | | | | | | | | | | | _ | | 5 | | | | | | + | | | ce, | | | shop(s) | | ce office | ce | Ce | ce | | | | | | | 59 | Secondary Use | 14 |
| | Eastern Road | | | | | | Lulu Street | | | Sheikh Hamdan Street | Sh Khafila Street | Old AirportRoad | Sheikh Ham dan Street | Corniche Street | | | | The Six Towers | The Six Towers | The Six Towers | The Six Towers | | | Zayed 2nd Street | Corniche Road | Khalidya Street | Sheikh Zayed 1st Street | 21.11.7 | | 5020 LiwaStreet | Khali dya Street | | Hamal Street | (Electra) Street | Mohammed Street | SCIEV. A. B. | | Sheikh Khalifa Street | | | Sheikh Ham dan Street | Street | Comprex | Location in H |
| Y as Island | | | | | | | | | | | | | | | | - | | | | | | | | + | | | | | | | - | | | | | | | | | | | | Come | mirate of Abu Dh |
| Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Uhabi | Abu Uhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Uhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Abu Dhabi | Чţ | natai |
| | 56.76 m | 72.59 m | 67.52 m | 67.52 m | 67.52 m | 72.71 m | 72.71 m | 78.17 m | 58.62 m | 78.17 m | 72.71 m | 78.17 m | 78.17 m | 77.91 m | 77.91 m | 7701 m | 77.91 m | 74.43 m | 74.43 m | 74.43 m | 74.43 m | 85./0 m | 89.54 m | 89.34 m | 88.30 m | 84.35 m | 88.30 m | 8830m | 88.30 m | 85.14 m | 93.49 m | 93,40 m | 93.49 m | 93.49 m | 93.49 m | 100.50 m | 93.49 m | 93.49 m | 93.49 m | m 89'86 | 89.87 m | 94.28 m | in meters (/ | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | agn Architectural) Aneters | |
| 12 2007 | 12 | 13 | 13 | 13 | | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 15 1995 | 5 | | 5 | 15 2004 | 15 2004 | 15 2004 | 15 2004 | 0 | 10 | 16 | 17 1996 | 17 1995 | 17 | | 17 | 18 | 18 | 18 2000 | 100 | 18 | 18 | 18 | 00 | 18 | 8 | 19 | 19 | 19 | rioars ⊂ans (above Start ground) | Techn |
| 2009 | | | | | | 1996 | | | | | | | | 1996 | 1996 | 1006 | 1996 | 200.5 | 2005 | 2005 | 2005 | | 1661 | | 1998 | 1998 | | | | 1995 | 1998 | 2002 | | | | | | | 7001 | 1993 | 1995 | | ruction Const End | cal Data |
| | | | | | | 1000 | | | | | | | | | | | | | | | | | - | | | | | | | | | | | | | | | | - | - | | | ruction r 10 or- ceilin beight | 174 |
| P | | | | | | | | | - | | | | | | | - | | | | | | | | | | | | | | | _ | | | | | | | | - | | | | (m) | 1 |
| Architect. Asymptote Architecture, Architect. Asymptote Architecture, Architect. Deven Architecta& Enginees, Tilee & Partners WL.L. Abu Dhata | | | | | | | | | | | | | | Consultants | | | | | | | | | Archatect: Casa a & Associates | | International Ltd. | Architect: Nerr Group Consultants International Ltd. | | | | | | | Group | | | | | Architect: Cassia & Associates | | | Enginears | | | InvolvedCompanies |

| Architect: Dewan Architects & | | 1993 | | | | Ahn Dhahi | Ribelt Po Rit ant | | A C | | Intraise huilding | 1002 | The Terret |
|----------------------------------|------------|-------|----------------|-----------------------|-----------|------------|---------------------------|----------------|-----------------|--|--------------------|-------------|-------------------------------------|
| | | 200.5 | | | | Abu Dhabi | Airport Road | 05 A | terminal | | low-rise building | 200.5 | Abu Dhabi Airport Terminal 2 |
| | | 2006 | 2005 | | | Abu Dhabi | Khalidya Towers | | residential | | low-rise building | 2006 | Khalidya Tower 3 |
| | | 2006 | 2005 | | | Abu Dhabi | Khalidya Towers | | residential | | low-rise building | 2006 | Khalidya Tower 2 |
| | | 2006 | 200.5 | | | Abu Dhabi | Khali dya Towers | ffice | commercial o | | low-rise building | 2006 | Khalidya Tower 1 |
| (New York) | | 2009 | 2006 | | | Abu Dhabi | Airport Road | đi P | terminal | | low-rise building | 2009 | Etihad Passenger Terminal 3 |
| | | | | | | Abu Dhabi | | er ice skating | shopping cer | | low-rise building | | Marina Mall |
| | | | | | | Abu Dhabi | Airport Road | | aircraft traffi | | airport tow er | | Abu Dhata Air Traffic Control Tower |
| | - | +- | | | | Abu Dhata | Airport Road | | TRITTIN | | hall | | Abu Dhabi Airport Cargo Terminal |
| | | | | | | Am Dhohi | Airport Doud | 69 8 | amort passes | | low-size building | | ∆tus ∏habi Airmort Terminal 1 |
| | | | | | | Abu Dhabi | Sheikh Khalifa Street | | | | low-rise building | | Airline Tower |
| | | 83.5 | | | | Abu Dhabi | Hamdan Street | | | | low-rise building | | SamanTower |
| | | | | | | Abu Dhata | | ffice | commercial o | | low-rise building | | Office Tower |
| | | | | | | Abu Dhabi | | | | | low-rise building | | Garden Tower |
| | | | | | | Abu Dhabi | | | | | low-rise building | | Sultan Tower Building |
| | | | | | | Abu Dhabi | | | | | low-rise building | | AIS alam Tower |
| | | | | | | Abu Dhabi | Maidan Al Ittihad Street | | | | low-rise building | | Al Bader Tower |
| | | | | | | Abu Dhata | | | | | low-rise building | | Al S dada Tower |
| | | | | | | Abu Dhabi | Al Salam Street | | | | low-rise building | | Al Mansour Tower |
| | | | | | | Abu Dhabi | | | | | low-rise building | | Hanna Tower |
| | | | | | | Abu Dhabi | | | | | low-rise building | | Plaza Tower |
| | | | | | | Abu Dhabi | Khalifa Street | | | | low-rise building | | Tawam Tower II |
| | | | | | | Abu Dhabi | Nazda Street | | | | low-rise building | | Sagar Tower |
| | | | | | | Abu Dhabi | Abu Dhabi Road | | | | low-rise building | | Sity Tower |
| | | | | | | Abu Dhabi | Khalifa Street | | | | low-rise building | | Deena Tower |
| | | | | | | Abu Dhabi | Abu Dhabi Highway | | | | low-rise building | | Al Moosa Tower |
| | | | | | | Abu Dhabi | | | | | low-rise building | | Al Khubairah Tower |
| | | | - | | | Abu Dhabi | Electra Street | | + | | low-rise building | | Bin Butti Tower |
| | | | | | | Ahn Dhahi | A Mittory Towner | | | | low-nee huilding | | Al Manara Tourat |
| | | | | | | Abu Dhaki | Al Neido Street | | | | low rise building | | Parcont 1 0w et |
| | | - | | | | AU DIAU | onentin annonenti | | | | Strutton as ti-mor | | Carao Lower |
| | | | | | | Aler Diate | Shall b U and an Ofmat | THE | TELOTOMINICO | | Tow in huiding | | And Torrat |
| | | _ | | | | Abu Dhati | | | commercial | | low-rise building | | Al Mansoori Office Lower |
| | | | | | | Abu Dhaba | Electra Street | 1 | | | low-rise building | | Saadiyat Tower |
| Architect: Golden Planners | | | 1999 | | | Abu Dhabi | Airport Road | | | | low-rise building | | Rabdan Complex |
| | | | | | | Abu Dhabi | | | | | low-rise building | | Dhabi Tower |
| | | | | | | Abu Dhabi | Khalifa Street | | | | low-rise building | | The Blue Tower |
| | | | 894.V | | | Abu Dhabi | Hamdan Street | | | | low-rise building | | Bin Ghanem Tower |
| | | | | | | Abu Dhabi | Salam Street | | | | low-rise building | | Al Ferdaws Tower |
| Daly | | | | ω | 15.58 m | Abu Dhabi | Zadco and Gasco Towers | | | | low-rise building | | Car Park |
| | | | | 5 | 44.28 m | Abu Dhabi | Between the Bridges | | hotel | | low-rise building | | Shangri-La Hotel |
| Interior fit out Depa Ltd | | | | 60 | 37.17 m | Abu Dhate | | | office | | low-rise building | | Ministry of Foreign Affairs |
| Interior fit-out: Depa Ltd | | 1979 | | 10 | 46.46 m | Abu Dhabi | Corniche Road | | hotel | | low-rise building | 1979 | Sheraton Abu Dhabi |
| Interior fit out: Depa Ltd | | | | 10 | 46.46 m | Abu Dhabi | Al Na da Street | | office | | low-rise building | | ADWEA Building |
| Abu Dhabi | | | | 10 | 55.84 m | Abu Dhabi | | | hotel | modernism | low-rise building | | Hilton International Abu Dhabi |
| Archited: AdnenZ Saffenni Engr - | height(m) | |)d) | mmeters around | | | | | _ | | | | |
| 1000 | Burgeo tro | End | re Start | (Architectural) (abov | in meters | city | ⊂ ompuex. | as n. Kimmacr | r Innary Ose | Material Style | adif r Srmining | uffaur na t | aune a Branna |
| samedun ~ navmanna | | | Lectura car De | 17.1.4.1 T1-1. | | ADD DIAD | Contraction in Emirate or | U 93280 | 1 D.J | of the state of th | DUILET | V 11 | Deal dia a Maria - |

APPENDIX C – SIMULATION INPUT DATA

Table C1 Thermal Conditions Input in IES Baseline Model for Washroom Thermal Template

Thermal Template: Washroom

[L01W0000]

L01 WC

| Heating | | |
|---|----------------------------|----------------------------------|
| Profile | | off continuously |
| Setpoint: Constant | | 19 °C |
| Hot Water consumption | | 0.00 l/(h·pers) |
| Cooling | | |
| Profile | | 8 - 6 weekday working (no lunch) |
| Setpoint: Constant | | 23 °C |
| Model Settings | | |
| Solar Reflected Fraction | | 0.05 |
| Furniture Mass Factor | | 1.00 |
| Systems | | |
| HVAC System | | Main system |
| Auxilliary vent. system | | Main system |
| DHW system | | Main system |
| Heating | | |
| Radiant Fraction | | 0.20 |
| Capacity | | unlimited |
| Cooling | | |
| Radiant Fraction | | 0.00 |
| Capacity | | unlimited |
| Humidity Control | | |
| Min. % Saturation | | 30 % |
| Max. % Saturation | | 70 % |
| System outside air supply | , | |
| Min. Flow Rate | | 0.80 l/(s⋅m²) |
| Add. Free Cooling Capacity | | 0.00 AC/h |
| Variation Profile | | off continuously |
| Internal Gains | | , |
| • Fluorescent Lighting : Flu | orescent Lighting Washroom | |
| Max Sensible Gain | 5 5 | 9.00 W/m ² |
| Max Power Consumption | | 9.00 W/m ² |
| Radiant Fraction | | 0.45 |
| Fuel | | Electricity |
| Variation Profile | | 8 - 6 weekday working (no lunch) |
| Dimming Profile | | on continuously |
| Air Exchanges | | , |
| Infiltration | | |
| Туре | | Infiltration |
| Variation Profile | | on continuously |
| Adjacent Condition | | External Air |
| Max A/C Rate | | 0.25 AC/h |
| Auxiliary ventilation | | |
| Type | | Auxiliary Ventilation |
| Variation Profile | | 8 - 6 weekday working (no lunch) |
| Adjacent Condition | | External Air |
| Max A/C Rate | | 2.00 AC/h |
| Pooms using thi | is tomplato | |
| | | |
| Room ID | Name | |
| [L01B0008] | L01 Bathroom | |
| [L01B0005] | L01 Bathroom | |
| [L01B0011] | L01 Bathroom | |
| [01R0002] | L01 Bathroom | |
| | | |

| Rooms using this template | | |
|---------------------------|--|--|
| Name | | |
| L01 WC | | |
| L01 WC | | |
| L01 WC | | |
| L01 Bathroom | | |
| L01 WC | | |
| L01 Bathroom | | |
| L01 WC | | |
| | | |

Table C2 Thermal Conditions Input in IES Baseline Model for Office Thermal Template

Thermal Template: Office

| Heating Profile Setpoint: Constant Hot Water consumption Cooling Profile 8 - 6 weekday working (no lunch) 23 °C Model Settings Solar Reflected Fraction 0.05 Furniture Mass Factor Systems HVAC System Auxilliary vent. system Heating Radiant Fraction Cooling Radiant Fraction Cooling Radiant Fraction Cooling Radiant Fraction Support Solar Reflected Fraction O.05 Furniture Mass Factor Solar Reflected Fraction O.05 Furniture Mass Factor Solar Reflected Fraction O.05 Guina System Main system Main system Main system Main system Main system O.20 Capacity Cooling Radiant Fraction Cooling Cooling Radiant Fraction Cooling Cooli | Room Conditions | _ |
|--|---|----------------------------------|
| Profileoff continuouslySetpoint: Constant19 °CHot Water consumption0.00 l/(h-pers)• Cooling8 - 6 weekday working (no lunch)Profile8 - 6 weekday working (no lunch)Setpoint: Constant23 °C• Model Settings0.05Solar Reflected Fraction0.05Furniture Mass Factor1.00SystemsMain systemHVAC SystemMain systemDHW systemMain systemDHW system0.20capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Humidity Control30 %Min. % Saturation70 %• System outside air supply0.00 AC/hMin. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Latent Gain90.00 W/P | • Heating | T |
| Setpoint: Constant19 °CHot Water consumption0.00 l/(h-pers)• Cooling8 - 6 weekday working (no lunch)Profile8 - 6 weekday working (no lunch)Setpoint: Constant23 °C• Model Settings0.05Solar Reflected Fraction0.05Furniture Mass Factor1.00SystemsMain systemHVAC SystemMain systemDHW systemMain systemHeating0.20Radiant Fraction0.20Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Humidity Control30 %Min. % Saturation30 %Max. % Saturation70Nin. Flow Rate0.80 l/(s-m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Latent Gain90.00 W/P | Profile | off continuously |
| Hot Water consumption0.00 l/(h-pers)• Cooling8 - 6 weekday working (no lunch)Profile8 - 6 weekday working (no lunch)Setpoint: Constant2 3 °C• Model Settings0.05Solar Reflected Fraction0.05Furniture Mass Factor1.00SystemsMain systemHVAC SystemMain systemDHW systemMain systemDHW system0.20capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Katuration30 %Max. % Saturation70 %• System outside air supply0.80 l/(s·m²)Min. Flow Rate0.80 l/(s·m²)• People : People Office90.00 W/PMax Sensible Gain90.00 W/PMax Latent Gain60.00 W/P | Setpoint: Constant | 19 °C |
| Cooling Profile B - 6 weekday working (no lunch) Setpoint: Constant Model Settings Solar Reflected Fraction Furniture Mass Factor Systems HVAC System Auxilliary vent. system DHW system Heating Radiant Fraction Cooling Radiant Fraction O.00 Capacity Unlimited Humidity Control Min. % Saturation System outside air supply Min. Flow Rate Add. Free Cooling Capacity Variation Profile Internal Gains People : People Office Max Sensible Gain 90.00 W/P Max Latent Gain | Hot Water consumption | 0.00 l/(h·pers) |
| Profile8 - 6 weekday working (no lunch)Setpoint: Constant23 °C• Model Settings0.05Solar Reflected Fraction0.05Furniture Mass Factor1.00SystemsMain systemHVAC SystemMain systemDHW systemMain system• Heating0.20Radiant Fraction0.20Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Katuration30 %Max. % Saturation70 %• System outside air supply0.80 I/(s·m²)Min. Flow Rate0.80 I/(s·m²)• People : People Office90.00 W/PMax Sensible Gain90.00 W/PMax Latent Gain60.00 W/P | • Cooling | |
| Setpoint: Constant23 °C• Model Settings0.05Solar Reflected Fraction0.05Furniture Mass Factor1.00SystemsMain systemHVAC SystemMain systemAuxilliary vent. systemMain systemDHW systemMain system• Heating0.20Radiant Fraction0.20Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Humidity Control30 %Min. % Saturation30 %Max. % Saturation30 %• System outside air supply0.80 l/(s·m²)Min. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Latent Gain90.00 W/P | Profile | 8 - 6 weekday working (no lunch) |
| Model Settings Solar Reflected Fraction Furniture Mass Factor HVAC System HVAC System Main system Max Saturation Max Sensible Gain Max Latent Gain | Setpoint: Constant | 23 °C |
| Solar Reflected Fraction0.05Furniture Mass Factor1.00SystemsMain systemHVAC SystemMain systemAuxilliary vent. systemMain systemDHW systemMain system• Heating0.20Radiant Fraction0.20Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Auxiliary Control0.00Max. % Saturation30 %Max. % Saturation70 %• System outside air supply0.00 AC/hWin. Flow Rate0.80 I/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Latent Gain90.00 W/P | Model Settings | |
| Furniture Mass Factor1.00SystemsMain systemHVAC SystemMain systemAuxilliary vent. systemMain systemDHW systemMain system• Heating0.20Radiant Fraction0.20Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Humidity Control30 %Min. % Saturation30 %• System outside air supply0.00 AC/hMin. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Sensible Gain90.00 W/PMax Latent Gain60.00 W/P | Solar Reflected Fraction | 0.05 |
| SystemsMain systemHVAC SystemMain systemAuxilliary vent. systemMain systemDHW systemMain system• Heating0.20Radiant Fraction0.20Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Humidity Control30 %Min. % Saturation70 %• System outside air supply0.80 l/(s·m²)Min. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Sensible Gain90.00 W/P | Furniture Mass Factor | 1.00 |
| HVAC SystemMain systemAuxilliary vent. systemMain systemDHW systemMain system• Heating0.20Radiant Fraction0.20Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Humidity Control30 %Min. % Saturation30 %• System outside air supply0.80 l/(s·m²)Min. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Sensible Gain90.00 W/PMax Latent Gain60.00 W/P | Systems | |
| Auxilliary vent. systemMain systemDHW systemMain system• Heating0.20Radiant Fraction0.20Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Auxility Control0.00Min. % Saturation30 %Max. % Saturation70 %• System outside air supply0.00 AC/hMin. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Sensible Gain90.00 W/PMax Latent Gain60.00 W/P | HVAC System | Main system |
| DHW systemMain system• Heating0.20Radiant Fraction0.20Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Humidity Control30 %Min. % Saturation30 %Max. % Saturation70 %• System outside air supply0.00 AC/hWin. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Sensible Gain90.00 W/P | Auxilliary vent. system | Main system |
| Heating Radiant Fraction Capacity Cooling Radiant Fraction Cooling Radiant Fraction Capacity Unlimited Humidity Control Min. % Saturation System outside air supply Min. Flow Rate Add. Free Cooling Capacity Variation Profile Internal Gains People : People Office Max Sensible Gain 90.00 W/P Max Latent Gain | DHW system | Main system |
| Radiant Fraction0.20Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Humidity Control30 %Min. % Saturation30 %Max. % Saturation70 %• System outside air supply0.80 l/(s·m²)Min. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Sensible Gain90.00 W/P | Heating | |
| Capacityunlimited• Cooling0.00Radiant Fraction0.00Capacityunlimited• Humidity Control30 %Min. % Saturation30 %Max. % Saturation70 %• System outside air supply80 l/(s·m²)Min. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Sensible Gain90.00 W/P | Radiant Fraction | 0.20 |
| Cooling Radiant Fraction Capacity Humidity Control Min. % Saturation System outside air supply Min. Flow Rate Add. Free Cooling Capacity Variation Profile Internal Gains People : People Office Max Sensible Gain 90.00 W/P | Capacity | unlimited |
| Radiant Fraction0.00Capacityunlimited• Humidity ControlunlimitedMin. % Saturation30 %Max. % Saturation70 %• System outside air supply0.80 l/(s·m²)Min. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Sensible Gain90.00 W/PMax Latent Gain60.00 W/P | • Cooling | |
| Capacityunlimited• Humidity Control30 %Min. % Saturation30 %Max. % Saturation70 %• System outside air supply80 l/(s·m²)Min. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Sensible Gain90.00 W/P | Radiant Fraction | 0.00 |
| Humidity Control Min. % Saturation Max. % Saturation System outside air supply Min. Flow Rate Add. Free Cooling Capacity Variation Profile Internal Gains People : People Office Max Sensible Gain 90.00 W/P Max Latent Gain | Capacity | unlimited |
| Min. % Saturation30 %Max. % Saturation70 %• System outside air supply70 %Min. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains90.00 W/PMax Sensible Gain90.00 W/PMax Latent Gain60.00 W/P | Humidity Control | |
| Max. % Saturation70 %• System outside air supply0.80 l/(s·m²)Min. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains•• People : People Office90.00 W/PMax Latent Gain60.00 W/P | Min. % Saturation | 30 % |
| • System outside air supply Min. Flow Rate Add. Free Cooling Capacity Variation Profile Internal Gains • People : People Office Max Sensible Gain 90.00 W/P Max Latent Gain | Max. % Saturation | 70 % |
| Min. Flow Rate0.80 l/(s·m²)Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains•• People : People Office90.00 W/PMax Sensible Gain90.00 W/PMax Latent Gain60.00 W/P | System outside air supply | |
| Add. Free Cooling Capacity0.00 AC/hVariation Profileoff continuouslyInternal Gains•• People : People Office90.00 W/PMax Sensible Gain90.00 W/PMax Latent Gain60.00 W/P | Min. Flow Rate | 0.80 l/(s⋅m²) |
| Variation Profileoff continuouslyInternal Gains•• People : People Office90.00 W/PMax Sensible Gain90.00 W/PMax Latent Gain60.00 W/P | Add. Free Cooling Capacity | 0.00 AC/h |
| Internal Gains • People : People Office Max Sensible Gain Max Latent Gain 60.00 W/P | Variation Profile | off continuously |
| People : People Office Max Sensible Gain 90.00 W/P Max Latent Gain 60.00 W/P | Internal Gains | |
| Max Sensible Gain90.00 W/PMax Latent Gain60.00 W/P | People : People Office | |
| Max Latent Gain 60.00 W/P | Max Sensible Gain | 90.00 W/P |
| | Max Latent Gain | 60.00 W/P |

| Occupant Density | | 12.00 m ² /person |
|--|--------------------------|------------------------------------|
| Variation Profile | | 8 - 6 weekday working (no lunch) |
| Fluorescent Lighting : Flu | orescent Lighting Office | |
| Max Sensible Gain | | 11.00 W/m ² |
| Max Power Consumption | | 11.00 W/m² |
| Radiant Fraction | | 0.45 |
| Fuel | | Electricity |
| Variation Profile | | 8 - 6 weekday working (no lunch) |
| Dimming Profile | | on continuously |
| Computers : Computers C | Office | 00.0014// 2 |
| Max Sensible Gain | | 20.00 W/m ² |
| Nax Power Consumption | | 20.00 W/m² |
| | | U.22 Electricity |
| Variation Profile | | 8 - 6 weekday working (no lunch) |
| Air Exchanges | | o - o weekday working (no farieri) |
| Infiltration | | |
| | | Infiltration |
| Variation Profile | | on continuously |
| Adjacent Condition | | External Air |
| Max A/C Rate | | 0.25 AC/h |
| Auxiliary ventilation | | |
| Туре | | Auxiliary Ventilation |
| Variation Profile | | 8 - 6 weekday working (no lunch) |
| Adjacent Condition | | External Air |
| Max A/C Rate | | 2.00 AC/h |
| Rooms using th | is template | |
| Room ID | Name | |
| [L01B0010] | L01 Bedroom | |
| [L01B0001] | L01 Bedroom | |
| [L01B0003] | L01 Bedroom | |
| [L01B0004] | L01 Bedroom | |
| [L01B0007] | L01 Bedroom | |
| [L01B0006] | L01 Bedroom | |
| [L01B0000] | L 01 Bedroom | |
| [101B0000] | | |
| | | |
| | LUT LIVING ROOM | |

L01 Living Room L01 Living Room L01 Living Room

[L01L0002] [L01L0003] [L01L0001] Table C3 Thermal Conditions Input in IES Baseline Model for Corridor Thermal Template

Thermal Template: Corridor

[L01C0008]

[MZNN0000]

L01 Corridor

Mezanine offices

| • Heating | | |
|-----------------------------|----------------------------|----------------------------------|
| Profile | | off continuously |
| Setpoint: Constant | | 19 °C |
| Hot Water consumption | | 0.00 l/(h·pers) |
| • Cooling | | |
| Profile | | 8 - 6 weekday working (no lunch) |
| Setpoint: Constant | | 23 °C |
| Model Settings | | |
| Solar Reflected Fraction | | 0.05 |
| Furniture Mass Factor | | 1.00 |
| Systems | | |
| HVAC System | | Main system |
| Auxilliary vent. system | | Main system |
| DHW system | | Main system |
| Heating | | |
| Radiant Fraction | | 0.20 |
| Capacity | | unlimited |
| Cooling | | |
| Radiant Fraction | | 0.00 |
| Capacity | | unlimited |
| Humidity Control | | |
| Min. % Saturation | | 30 % |
| Max. % Saturation | | 70 % |
| System outside air supply | | |
| Min. Flow Rate | | 0.80 l/(s⋅m²) |
| Add. Free Cooling Capacity | | 0.00 AC/h |
| Variation Profile | | off continuously |
| Internal Gains | | |
| Fluorescent Lighting : Flue | prescent Lighting Corridor | |
| Max Sensible Gain | | 13.00 W/m ² |
| Max Power Consumption | | 13.00 W/m ² |
| Radiant Fraction | | 0.45 |
| Fuel | | Electricity |
| Variation Profile | | 8 - 6 weekday working (no lunch) |
| Dimming Profile | | on continuously |
| Air Exchanges | | |
| • Infiltration | | |
| Туре | | Infiltration |
| Variation Profile | | on continuously |
| Adjacent Condition | | External Air |
| Max A/C Rate | | 0.25 AC/h |
| • Auxiliary ventilation | | |
| Type | | Auxiliary Ventilation |
| Variation Profile | | 8 - 6 weekday working (no lunch) |
| Adjacent Condition | | External Air |
| Max A/C Rate | | 2.00 AC/h |
| Rooms using thi | s template | |
| Room ID | Name | |
| | L01 Corridor | |
| | | |
| | | |
| [L01C0003] | LUI Corridor | |
| [L01C0002] | L01 Corridor | |
| [L01C0005] | L01 Corridor | |
| [L01C0006] | L01 Corridor | |
| [L01C0007] | L01 Corridor | |
| | | |

| Rooms using the | is template |
|-----------------|------------------|
| Room ID | Name |
| [MZNN0001] | Mezanine offices |
| [MZNN0002] | Mezanine offices |
| [MZNN0003] | Mezanine offices |
| [MZNN0004] | Mezanine offices |
| [MZNN0005] | Mezanine offices |
| [MZNN0006] | Mezanine offices |
| [MZNN0007] | Mezanine offices |
| [MZNN0008] | Mezanine offices |
| [MZNN0009] | Mezanine offices |
| [MZNN0010] | Mezanine offices |
| [MZNN0011] | Mezanine offices |
| [MZNN0012] | Mezanine offices |
| [MZNN0013] | Mezanine offices |
| [MZNN0014] | Mezanine offices |
| [MZNN0015] | Mezanine offices |
| [L01C0009] | L01 Corridor |
| [L01C0010] | L01 Corridor |
| [L01C0011] | L01 Corridor |
| [L01C0012] | L01 Corridor |
| [GRND0000] | Ground Retail |
| [GRND0002] | Ground Retail |
| [GRND0003] | Ground Retail |
| [GRND0005] | Ground Retail |
| [GRND0006] | Ground Retail |
| [GRND0007] | Ground Retail |
| [GRND0010] | Ground Retail |
| [GRND0011] | Ground Retail |

Table C4 Thermal Conditions Input in IES Baseline Model for Kitchen Thermal Template

Thermal Template: Kitchen

| Heating | - |
|--------------------------|----------------------------------|
| Profile | off continuously |
| Setpoint: Constant | 19 °C |
| Hot Water consumption | 0.00 l/(h·pers) |
| • Cooling | |
| Profile | 8 - 6 weekday working (no lunch) |
| Setpoint: Constant | 23 °C |
| Model Settings | |
| Solar Reflected Fraction | 0.05 |
| Furniture Mass Factor | 1.00 |
| Systems | |
| HVAC System | Main system |
| Auxilliary vent. system | Main system |
| DHW system | Main system |
| • Heating | |
| Radiant Fraction | 0.20 |
| Capacity | unlimited |
| • Cooling | |
| Radiant Fraction | 0.00 |
| Capacity | unlimited |
| Humidity Control | |
| | |

| Min. % Saturation | 30 % |
|---|----------------------------------|
| Max. % Saturation | 70 % |
| System outside air supply | |
| Min. Flow Rate | 0.80 l/(s⋅m²) |
| Add. Free Cooling Capacity | 0.00 AC/h |
| Variation Profile | off continuously |
| Internal Gains | |
| Fluorescent Lighting : Fluorescent Lighting Kitchen | |
| Max Sensible Gain | 9.00 W/m ² |
| Max Power Consumption | 9.00 W/m ² |
| Radiant Fraction | 0.45 |
| Fuel | Electricity |
| Variation Profile | 8 - 6 weekday working (no lunch) |
| Dimming Profile | on continuously |
| Cooking : Cooking | |
| Max Sensible Gain | 10.00 W/m ² |
| Max Latent Gain | 0.00 W/m ² |
| Max Power Consumption | 10.00 W/m ² |
| Radiant Fraction | 0.60 |
| Fuel | Electricity |
| Variation Profile | 8 - 6 weekday working (no lunch) |
| Air Exchanges | |
| Infiltration | |
| Туре | Infiltration |
| Variation Profile | on continuously |
| Adjacent Condition | External Air |
| Max A/C Rate | 0.25 AC/h |
| Auxiliary ventilation | |
| Туре | Auxiliary Ventilation |
| Variation Profile | 8 - 6 weekday working (no lunch) |
| Adjacent Condition | External Air |
| Max A/C Rate | 2.00 AC/h |
| Rooms using this template | |
| Room ID Name | |
| | |

| Room ID | Name |
|------------|-------------|
| [L01K0003] | L01 Kitchen |
| [L01K0001] | L01 Kitchen |
| [L01K0002] | L01 Kitchen |
| [L01K0000] | L01 Kitchen |
| | |

Table C5 Thermal Conditions Input in IES Baseline Model for Lobby Thermal Template

Thermal Template: Lobby

[L01L0005]

L01 Lobby

| Heating | |
|---|----------------------------------|
| Profile | off continuously |
| Setpoint: Constant | 19 °C |
| Hot Water consumption | 0.00 l/(h.pers) |
| • Cooling | 0.00 %(p0.0) |
| Profile | 8 - 6 weekday working (no lunch) |
| Setnoint: Constant | |
| Model Settings | 20 0 |
| Solar Peflected Fraction | 0.05 |
| Surpiture Mass Easter | 1.00 |
| Suctome | 1.00 |
| Jystellis | Main avetem |
| Auxillianu vent evetem | Main system |
| Auximary vent. System | Main system |
| | Main system |
| • Heating | 0.00 |
| Radiant Fraction | 0.20 |
| Capacity | unlimited |
| • Cooling | |
| Radiant Fraction | 0.00 |
| Capacity | unlimited |
| Humidity Control | |
| Min. % Saturation | 30 % |
| Max. % Saturation | 70 % |
| System outside air supply | |
| Min. Flow Rate | 0.80 l/(s⋅m²) |
| Add. Free Cooling Capacity | 0.00 AC/h |
| Variation Profile | off continuously |
| Internal Gains | |
| Fluorescent Lighting : Fluorescent Lighting Lob | by |
| Max Sensible Gain | 12.00 W/m ² |
| Max Power Consumption | 12.00 W/m ² |
| Radiant Fraction | 0.45 |
| Fuel | Electricity |
| Variation Profile | 8 - 6 weekday working (no lunch) |
| Dimming Profile | on continuously |
| Miscellaneous : Miscellaneous Lift | |
| Max Sensible Gain | 5.00 W/m ² |
| Max Latent Gain | 0.00 W/m ² |
| Max Power Consumption | 5.00 W/m ² |
| Radiant Fraction | 0.22 |
| Fuel | Electricity |
| Variation Profile | 8 - 6 weekday working (no lunch) |
| Air Exchanges | |
| • Infiltration | |
| Туре | Infiltration |
| Variation Profile | on continuously |
| Adjacent Condition | External Air |
| Max A/C Rate | 0.25 AC/h |
| Auxiliary ventilation | |
| Type | Auxiliary Ventilation |
| Variation Profile | 8 - 6 weekday working (no lunch) |
| Adjacent Condition | External Air |
| Max A/C Rate | 2.00 AC/h |
| Rooms using this template | |
| Poom ID Name | |
| | |
| [L01C0004] L01 Lobby | |
| [L01L0004] L01 Lobby | |

Table C6 Thermal Conditions Input in IES Baseline Model for Void Zone

Thermal Template: Void

Room Conditions

| • Heating | |
|------------------------------------|--------------------|
| Profile | off continuously |
| Setpoint: Constant | 19 °C |
| Hot Water consumption | 0.00 l/(h·pers) |
| • Cooling | |
| Profile | off continuously |
| Setpoint: Constant | 23 °C |
| Model Settings | |
| Solar Reflected Fraction | 0.05 |
| Furniture Mass Factor | 1.00 |
| Systems | |
| HVAC System | Main system |
| Auxilliary vent. system | Main system |
| DHW system | Main system |
| • Heating | |
| Radiant Fraction | 0.20 |
| Capacity | unlimited |
| • Cooling | |
| Radiant Fraction | 0.00 |
| Capacity | unlimited |
| Humidity Control | |
| Min. % Saturation | 0% |
| Max. % Saturation | 100 % |
| • System outside air supply | |
| Min. Flow Rate | 0.80 l/(s⋅m²) |
| Add. Free Cooling Capacity | 0.00 AC/h |
| Variation Profile | off continuously |
| Internal Gains | N 1 |
| Air Evokonaso | None |
| Air Exchanges | |
| | Notural Vantilati |
| i ype Variation Brofile | inatural ventilati |
| variation Profile | on continuously |

 None

 ges
 Natural Ventilation

 rofile
 on continuously

 ondition
 External Air

 ate
 6.00 AC/h

 Rooms using this template

 Room ID
 Name

| | - |
|------------|------|
| Room ID | Nam |
| [VOID0001] | Void |
| [VOID0000] | Void |

Adjacent Condition

Max A/C Rate

APPENDIX D – SIMULATION INPUT DATA

| WALL Description External Wall-Baseline | | | | | | | | | | | |
|--|----------------|-------------------------------|------------------|--|---------------------|-------------------------------------|---------------|--|--|--|--|
| Outside suiface | | | | | Standa | rd | Generic | | | | |
| Emissivity 0.900 Resistance (m ² K/W) 0.0299 | 🗸 default | Solar abs | orptance | 0.700 | | | | | | | |
| Inside surface | | | | | | | | | | | |
| Emissivity 0.900 Resistance (m ² K/W) 0.1198 | 🗸 default | Solar abs | orptance | 0.550 | | | | | | | |
| Metal Cladding | | | | | | | | | | | |
|] This is a ground contact wall (not an external wall) | value adjustme | ent | | | | | | | | | |
| Material | Thickness m | Conductivity W/(m·K) | Density kg/m³ | Specific Heat Capacity J/(kg·K) | Resistance m²K/W | Vapour Resistivity GN·s/(kg·m | Category | | | | |
| PLASTER (DENSE) | 0.0150 | 0.5000 | 1300.0 | 1000.0 | | | Plaster | | | | |
| Concrete Lightweight (modified) | 0.2000 | 1.7000 | 1900.0 | 999.8 | | 0.000 | Concretes | | | | |
| Cavity | 0.1000 | | | | 0.1800 | | | | | | |
| Concrete Lightweight (modified) | 0.2000 | 1.7000 | 1900.0 | 999.8 | | 0.000 | Concretes | | | | |
| PLASTER (DENSE) | 0.0150 | 0.5000 | 1300.0 | 1000.0 | | | Plaster | | | | |
| Copy Paste Cavity Insert Add Delete Flip | | | | | | | | | | | |
| Total R-value 0.4753 m ² K/W | U-1 | value (VV/m²r value method | ASHRA | E 🔻 | | U-value | 1.6000 W/m²·K | | | | |

Figure D 35 Wall construction details for baseline model.

| | | | | | Standar | rd | Generic |
|--|---|---|---|---|--|--|---|
| inisivity 0,900 Resistance (m34/00) 0,0299 | default | Solar abeo | mtance | 0.700 | | | |
| | Gordan | 20101 0030 | iptance | 0.700 | | | |
| iside suiface | | | | 0.550 | | | |
| missivity 0.900 Resistance (m4V/VV) 0.1198 | default | 50lar abso | rptance | U.COU | | | |
| Metal Cladding | | | | | | | |
| This is a ground contact wall (not an external wall) | alue adjustme | nt | | | | | |
| | | | | | | | |
| onstruction layers (outside to inside) | | | | | | | |
| | | | | Specific | | Vacaur | |
| Material | Thickness | Conductivity | Density ka/m² | Heat | Resistance | Napour Resistivity | Category |
| | | w/(m/s) | Kg/m | J/(kg·K) | 111 IN W | GN·s/(kg·m | |
| PLASTER (DENSE) | 0.0150 | 0.5000 | 1300.0 | 1000.0 | | | Plaster |
| Concrete Lightweight (modified) | 0.2000 | 1.7000 | 1900.0 | 999.8 | | 0.000 | Concretes |
| Cavity | 0.1000 | | | | 0.1800 | | - |
| Concrete Lightweight (modified) | 0.2000 | 1.7000 | 1900.0 | 999.8 | | 0.000 | Concretes |
| | 0.0625 | 0.0250 | 30.0 | 1400.0 | | | Insulating Materials |
| CASTER (DENSE) | 0.0150 | 0.0000 | 1300.0 | 1000.0 | | | Plaster |
| Copy Paste Cavity Insert Add Delete | Flip | 1 | | | Sys | tem Materials | Project Materials |
| | | | | | | | |
| nstruction thickness 0.5925 m | - U-v | value (W/m²·K |) | | | _ | |
| Total Ravalue 2 9753 m ² K/M | U-v | alue method | ASHRAE | • | | U-value | 0.3200 W/m ² K |
| | | | | | | | |
| WALL11 Description External Wall-[2 pearl] | | | | | | | Consta |
| WALL11 Description External Wall-[2 pearl] utside surface missivity 0.900 Resistance (m%/W) 0.0299 | ✓ default | Solar abs | somtance | 0 700 | Stand | lard | Generic |
| WALL11 Description External Wall-[2 pear] utside surface | ✓ default | Solar abs | sorptance | 0.700 | Stand | lard | Generic |
| WALL11 Description External Wall-[2 pear] uutside surface missivity 0.900 Resistance (m ² K/W) 0.0299 uside surface missivity 0.900 Resistance (m ² K/W) 0.1100 | ☑ default | Solar abs | sorptance | 0.700 | Stand | lard | Generic |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 [uside surface missivity 0.900 Resistance (m ² K/W) 0.1198 [| ☑ default ☑ default | Solar abs Solar abs | sorptance sorptance | 0.700 | Stand | lard | Generic |
| WALL11 Description External Wall-[2 pearl] Jutside surface | ✓ default ✓ default | Solar abs Solar abs | sorptance sorptance | 0.700 | Stand | lard | Generic |
| WALL11 Description External Wall-[2 pearl] Dutside surface | ✓ default ✓ default | Solar abs | sorptance sorptance | 0.700 | Stand | lard | Generic |
| WALL11 Description External Wall-[2 pear] Dutside surface missivity 0.900 Resistance (m ² K/W) 0.0299 [Inside surface missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding This is a ground contact wall (not an external wall) U-v | ✓ default ✓ default ✓ alue adjustm | Solar abs Solar abs ent | sorptance sorptance | 0.700 | Stand | lard | Generic |
| WALL11 Description External Wall-[2 pearl] Dutside surface | ✓ default ✓ default ralue adjustm | Solar abs Solar abs ent | sorptance sorptance | 0.700 | Stand | lard | Generic |
| WALL11 Description External Wall-[2 pearl] Dutside surface Emissivity 0.900 Resistance (m ² K/W) 0.0299 [Inside surface Emissivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding This is a ground contact wall (not an external wall) U-v Construction layers (outside to inside) | default default ralue adjustm | Solar abs Solar abs ent | sorptance sorptance | 0.700 | Stand | lard | Generic |
| WALL11 Description External Wall-[2 pear] butside surface | default default ralue adjustm Thickness | Solar abs Solar abs ent | sorptance sorptance | 0.700 0.550 Specific | Stand | lard | Generic |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 [uside surface missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding This is a ground contact wall (not an external wall) U-v onstruction layers (outside to inside) Material | default default ralue adjustm Thickness m | Solar abs Solar abs ent Conductivit W/(mK) | sorptance sorptance | 0.700 0.550 Specific Heat Capacity | Stand | ard Vapour Besistivity | Generic |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 [side surface missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding This is a ground contact wall (not an external wall) U-v Onstruction layers (outside to inside) Material | default default ralue adjustm Thickness m | Solar abs Solar abs ent Conductivit W/(m·K) | sorptance sorptance | 0.700 0.550 Specific Heat Capacity J/(kg·K) | Stand | ard Vapour Resistivity GN:s/(kg-1 | Generic |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 [side surface missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding This is a ground contact wall (not an external wall) U-v onstruction layers (outside to inside) Material | default default ralue adjustm Thickness m 0.0150 | Solar abs Solar abs ent Conductivit W/(m·K) 0.5000 | sorptance sorptance socratics b b b c b c c s b c c s t c c c c c c c c c c c c c c c c | 0.700 0.550 Specific Heat Capacity J/(kg·K) 1000.0 | Stand | ard Vapour Resistivity GN·s/(kg·r | Generic M Category Plaster |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 I side surface missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding miss is a ground contact wall (not an external wall) U-v onstruction layers (outside to inside) Material PLASTER (DENSE) Concrete Lightweight (modified) | default default default Thickness m 0.0150 0.2000 | Solar abs Solar abs ent Conductivit W/(m·K) 0.5000 1.7000 | sorptance sorptance b b b b c sorptance b sorptance b c sorptance b sorptanc s sorptanc s s sorptanc s s s s s s s s s s s s s s s s s s s | 0.700 0.550 Specific Heat Capacity J/(kg·K) 1000.0 999.8 | Stand | ard Vapour Resistivity GN·s/(kg·r | Generic Generic Category Plaster Concretes |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 I uside surface missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding miss a ground contact wall (not an external wall) U-v onstruction layers (outside to inside) Material PLASTER (DENSE) Concrete Lightweight (modified) Cavity Cavity | default default default Thickness m 0.0150 0.2000 0.1000 | Solar abs Solar abs ent Conductivit W/(m·K) 0.5000 1.7000 | orptance orptance b Density kg/m ³ 1300.0 | 0.700 0.550 Specific Heat Capacity J/(kg·K) 1000.0 999.8 | Resistance m ² K/W | ard Vapour Resistivity GN⋅s/(kgn | Generic Generic Category Plaster Concretes |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 I side surface missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding Image: stance (m ² K/W) 0.1198 [[[Metal Cladding Image: stance (m ² K/W) 0.1198 [[[[Image: stance (m ² K/W) 0.1198 [<t< td=""><td>default default alue adjustm Thickness 0.0150 0.2000 0.1000 0.2000</td><td>Solar abs Solar abs ent Conductivit W/(m·K) 0.5000 1.7000</td><td>orptance orptance borptance by bensity kg/m³ 1300.0 1900.0</td><td>0.700 0.550 Specific Heat Capacity J/(kg·K) 1000.0 999.8 999.8</td><td>Resistance n²K./W</td><td>Vapour Resistivity GN·s/(kg·1 0.000</td><td>Generic Generic Category Plaster Concretes Concretes</td></t<> | default default alue adjustm Thickness 0.0150 0.2000 0.1000 0.2000 | Solar abs Solar abs ent Conductivit W/(m·K) 0.5000 1.7000 | orptance orptance borptance by bensity kg/m ³ 1300.0 1900.0 | 0.700 0.550 Specific Heat Capacity J/(kg·K) 1000.0 999.8 999.8 | Resistance n²K./W | Vapour Resistivity GN·s/(kg·1 0.000 | Generic Generic Category Plaster Concretes Concretes |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 I side surface missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding Image: stance (m ² K/W) 0.1198 [[[Metal Cladding Image: stance (m ² K/W) 0.1198 [| Image: Constraint of the second sec | Solar abs Solar abs ent Conductivit W/(m·K) 0.5000 1.7000 1.7000 0.2500 | sorptance sorptance 1300.0 1900.0 30.0 | 0.700 0.550 Specific Heat Capacity J/(kg·K) 1000.0 999.8 999.8 1400.0 | Resistance n²K/W 0.1800 | Vapour Resistivity GN·s/(kg·1 0.000 | Generic Generic Category Plaster Concretes Concretes Concretes |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 I side surface missivity 0.900 Resistance (m ² K/W) 0.0198 I missivity 0.900 Resistance (m ² K/W) 0.1198 I Metal Cladding Image: missivity 0.900 Resistance (m ² K/W) 0.1198 I Metal Cladding Image: missivity 0.900 Resistance (m ² K/W) 0.1198 I Metal Cladding Image: missivity 0.900 Resistance (m ² K/W) 0.1198 I Material Image: missivity Image: missi | Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constraint of the second state Image: Constrainton state Image: Cons | Solar abs Solar abs ent Conductivit W/(m K) 0.5000 1.7000 0.0250 0.5000 | sorptance sorptance 1 300.0 1 900.0 30.0 1 300.0 | 0.700 0.550 0.550 Specific Heat Capacity J/(kg·K) 1000.0 999.8 999.8 1400.0 1000.0 | Resistance nºK/W 0.1800 | Vapour Resistivity GN·s/(kgr) 0.000 0.000 | Generic Generic Category Plaster Concretes Concretes Concretes Insulating Materials Plaster |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 I side surface missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding Image: stance (m ² K/W) 0.1198 [| ✓ default ✓ default ✓ adue adjustm Thickness m 0.0150 0.2000 0.1000 0.2000 0.0706 0.0150 e Flip | Solar abs Solar abs ent Conductivit W/(m·K) 0.5000 1.7000 0.0250 0.5000 | sorptance sorptance 1300.0 1900.0 30.0 1300.0 | 0.700 0.550 Specific Heat Capacity J/(kg·K) 1000.0 999.8 999.8 1400.0 1000.0 | Resistance n²K/W 0.1800 | Vapour Resistivity 0.000 0.000 0.000 | Generic Generic Category Plaster Concretes Concretes Insulating Materials Plaster Ster Ster Plaster |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 I side surface missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding Image: missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding Image: missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding Image: missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding Image: missivity 0.900 Resistance (m ² K/W) 0.1198 [Material Image: missivity 0.900 Resistance (m ² K/W) 0.1198 [PLASTER (DENSE) Image: missivity | ✓ default ✓ default ✓ default ✓ adjustm ✓ Thickness m 0.0150 0.2000 0.1000 0.2000 0.0706 0.0150 e e Flip | Solar abs Solar abs ent Conductivit W/(m K) 0.5000 1.7000 0.0250 0.5000 | sorptance sorptance 1 300.0 1 900.0 30.0 1 900.0 30.0 1 300.0 | 0.700 0.550 0.550 Specific Heat Capacity J/(kg·K) 1000.0 999.8 999.8 1400.0 1000.0 | Resistance m²K/W 0.1800 | Vapour Resistivity GN·s/(kgr) 0.000 0.000 0.000 | Generic Generic Category Plaster Concretes Concretes Insulating Materials Plaster Insulating Materials Plaster |
| WALL11 Description External Wall-[2 pear] utside surface missivity 0.900 Resistance (m ² K/W) 0.0299 I side surface missivity 0.900 Resistance (m ² K/W) 0.1198 [Metal Cladding Image: stance (m ² K/W) 0.1198 [[[[Metal Cladding Image: stance (m ² K/W) 0.1198 [| ✓ default ✓ default ✓ default ✓ adjustm Thickness 0.0150 0.2000 0.1000 0.2000 0.0706 0.0150 e e Flip U | Solar abs Solar abs ent Conductivit W/(m·K) 0.5000 1.7000 0.0250 0.5000 | sorptance sorptance 1 300.0 1 900.0 30.0 1 900.0 30.0 1 300.0 1 900.0 | 0.700 0.550 Specific Heat Capacity J/(kg·K) 1000.0 999.8 999.8 1400.0 1000.0 | Resistance m ² K/W 0.1800 | Vapour Resistivity GN·s/(kg·t 0.000 0.000 | Generic Generic Category Plaster Concretes Insulating Materials Plaster Plaster Sector Materials |

Figure D 37 Wall construction details for Pearl 2-5 model.

| TD EXTW Do | erciption External Wi | ndow (baseline) | | | | | | | | |
|---------------------------------|----------------------------|-------------------------------|----------|--------------------------------|--------------------|------------------------|-----------------------|---------------------|-----------------------|----------------------|
| ID LATH DE | scription external m | laovi (bascinic) | | | | | | | | |
| Shading devices | | None | Internal | None | _ | | | | | |
| Local | 2 External | None ? | Interna | Horic | <u> </u> | | | | | |
| Outside surface | | Frame | | | | | | | | |
| Emissivity | 0.837 | Material | Softwood | | Standard | Ger | neric | Surfac | ce area ratio | 1.0 |
| Resistance (m²K/W) | 0.0299 🔽 default | Percentage | 20.00 | % | | | | | | |
| | | Resistance | 0.1526 | m²K/W | | | | | | |
| Inside surface | | Absorptance | 0.7 | | | | | | | |
| Emissivity | 0.837 | Outside surface | | | | | | | | |
| Resistance (m²K/W) | 0.1198 🔽 default | area ratio | 1.00 | | | | | | | |
| | | Inside surface area ratio | 1.00 | | | | | | | |
| | | U-value | 3.3080 | W/m²∙K | | | | | | |
| | | | | | | | | | | |
| Construction layers (outside to | o inside) | | | | | | | | | |
| | | Type of | Conve | ction | | | | | | |
| Description | Thickness Conduct | ivity glassor K11 blind Ga | as W/m | cient Resistance ∻K (m²K/W) | Transmittance | Outside reflectance | Inside reflectance | Refractive index | Outside emissivitu | Inside emissivitu |
| CLEAR FLOAT 6MM | 0.0060 1.0 | 600 Uncoated | | | 0.780 | 0.070 | 0.070 | 1.526 | onnoorrig | Childrenty |
| | , , | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| Copy Paste Inse | ert Add Dele | ete | | | | | System Ma | terials | Project N | /aterials |
| U-value | | | | | Visible light prop | erties | | | | |
| U-value (glass only) | 6.4369 W/m ² ·K | | | | | | | _ | | |
| Net U-value (including frame) | 5.8111 W/m ² ·K | U-value method | ASHRAE | • | Visible light no | ormal transmit | tance 0.76 | | | |
| iguro D 38 External | Clazing constru | uction dotails fo | r Boceli | no modol | | | | | | |
| gure D Jo External | Giazing Constra | uction uctails 10 | n Dasell | ne mouel. | | | | | | |

Table D 37 External Glazing construction details for Baseline model.

| External Window [Baseline] | | | | | |
|---|----------------------------|--|--|--|--|
| U-value (glass only) | 6.4369 W/m ² ·K | | | | |
| Net U-value (including frame*) | 5.8111 W/m²·K | | | | |
| Outside surface air-film resistance | 0.0299 m ² K/W | | | | |
| Inside surface air-film resistance | 0.1198 m²K/W | | | | |
| THETA 0° 10° 20° 30° 40° 50° 60° | 70° 80° 90° | | | | |
| T(D) 0.780 0.779 0.776 0.770 0.759 0.736 0.66 | 38 0.581 0.348 0.000 | | | | |
| T(R) 0.032 0.032 0.032 0.033 0.035 0.036 0.03 | 37 0.038 0.036 0.000 | | | | |
| Short-wave shading coefficient | 0.8966 | | | | |
| Long-wave shading coefficient | 0.0364 | | | | |
| Total shading coefficient | 0.9329 | | | | |
| SHGC (center-pane) | 0.8116 | | | | |

| Shading devices Local None 2 External Outside surface Emissivity 0.837 | None Frame Material | ? | (nternal | None | ? | | | | | |
|---|---------------------------------------|----------|----------------------------|---------------------------------------|--------------------|------------------------|-----------------------|---------------------|-----------------------|----------------------|
| Outside surface Emissivity 0.837 | Frame Material | 6 | | | | | | | | |
| Emissivity 0.837 | Material | | | | | | | | | |
| | | S | oftwood | • | Standard | Ger | neric | Surfac | e area ratio | 1.0 |
| Resistance (m ² K/W) 0.0299 V det | ault Percentag | ge 2 | 0.00 | % | | | | | | |
| | Resistanc | e C | . 1526 | m²K/W | | | | | | |
| Inside surface | Absorpta | nce 0 | .7 | | | | | | | |
| Emissivity | Outside s | urface 🔒 | 00 | | | | | | | |
| Resistance (m²K/W) 0.1198 🗹 de | fault area ratio | | | | | | | | | |
| | Inside sur area ratio | face 1 | .00 | | | | | | | |
| | U-value | 3 | .3080 | W/m²•K | | | | | | |
| Construction layers (outside to inside) Description Thickness (m) (| nductivity glass or w/(m·K)) blind | Gas | Convec coeffici W/m² | tion ient Resistance ∙K (m²K∕W) | Transmittance | Outside reflectance | Inside reflectance | Refractive index | Outside emissivity | Inside emissivity |
| CLEAR FLOAT 6MM 0.0060 | 0.0610 Uncoate | ed | _ | | 0.417 | 0.070 | 0.070 | 1.526 | | |
| Cavity 0.0120 | | 4 | Air 2.0 | 0.1730 | | | | | | |
| CLEAR FLOAT 6MM 0.0060 | 0.0610 Uncoate | ed | | | 0.414 | 0.070 | 0.070 | 1.526 | | |
| | | | | | | | System Ma | terials | Project N | laterials |
| Copy Paste Insert Add | Delete | | | | | | aystem Ma | | riojecci | |
| Copy Paste Insert Add | Delete | | | | Visible light prop | erties | System Ma | | riojecti | |
| Copy Paste Insert Add J-value J-value (glass only) 1.9228 W | Delete | | |] | Visible light prop | erties | o area | | Hojecti | |

Table D 38 External Glazing construction details for Pearl 1 model.

| External Window [1 Pearl] | | | | | | |
|--|--|--|--|--|--|--|
| U-value (glass only) | 1.9228 W/m ² ·K | | | | | |
| Net U-value (including frame*) | 2.1998 W/m ² ·K | | | | | |
| Outside surface air-film resistance | 0.0299 m ² K/W | | | | | |
| Inside surface air-film resistance | 0.1198 m ² K/W | | | | | |
| THETA 0° 10° 20° 30° 40° 50° 60° T(D) 0.173 0.172 0.167 0.158 0.146 0.130 0.10 T(R) 0.227 0.227 0.227 0.228 0.227 0.224 0.21 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | |
| Short-wave shading coefficient | 0.1994 | | | | | |
| Long-wave shading coefficient | 0.2604 | | | | | |
| Total shading coefficient | 0.4598 | | | | | |
| SHGC (center-pane) | 0.4000 | | | | | |

| ID EXTW11 Des | ID EXTW11 Description External Window [2 Pearl] | | | | | | | | | | | |
|---|---|---------------------------|------------------------------|---------|-----------------------------------|------------------------------|--------------------|------------------------|-----------------------|---------------------|-----------------------|----------------------|
| Shading devices Local None | ? Exter | nal N | one | ? Ini | ternal | None | ? | | | | | |
| Outside surface | 0.837 | | Frame Material | Sof | twood | • | | _ | | 0f- | | |
| Resistance (m²K/W) | 0.0299 | default | Percentage | 20. | 00 % | , | Standard | Ger | heric | Surrac | e area rauo | 1.0 |
| Inside surface Emissivity | 0.837 | | Resistance Absorptance | 0.1 | .526 m | ²κ/W | | | | | | |
| Resistance (m²K/W) | 0.1198 | default | Outside surfa area ratio | ace 1.0 | 0 | | | | | | | |
| | | | Inside surfac area ratio | e 1.0 | 0 1080 W | /m2*K | | | | | | |
| Construction layers (outside to | o inside) | | | | | , | | | | | | |
| Description | Thickness (m) | Conductivity (W/(m·K)) | Type of glass or blind | Gas | Convectio coefficier W/m²·K | n t Resistance (m²K/W) | Transmittance | Outside reflectance | Inside reflectance | Refractive index | Outside emissivity | Inside emissivity |
| CLEAR FLOAT 6MM | 0.0060 | 0.0370 | Uncoated | | | | 0.252 | 0.070 | 0.070 | 1.526 | | |
| Cavity | 0.0120 | | | Air | 2.080 | 0 0.1730 | | | | | | |
| CLEAR FLOAT 6MM | 0.0060 | 0.0370 | Uncoated | | | | 0.253 | 0.070 | 0.070 | 1.526 | | |
| Copy Paste Inse | ert Add | Delete |] | | | | | | System Ma | terials | Project N | 1aterials |
| U-value | | | | | | | Visible light prop | erties | | | | |
| U-value (glass only) Net U-value (including frame) | 1.5486 1.9005 | W/m²∙K W/m²∙K | U-value met | hod A | SHRAE | • | Visible light no | rmal transmit | tance 0.76 | | | |

Figure D 40 External Glazing construction details for Pearl 2-5 model.

Table D 39 External Glazing construction details for Pearl 2-5 model.

| External Window [2 Pearl] | | | |
|---|---------------------------------------|--|-----------------------|
| U-value (glass only) Net U-value (including frame*) Outside surface air-film resistance Inside surface air-film resistance | | 1.5486 W/m ² ·K 1.9005 W/m ² ·K 0.0299 m ² K/W 0.1198 m ² K/W | |
| THETA 0°10°20°30°T(D)0.0640.0630.0600.055T(R)0.2360.2360.2350.233 | 40°50°60°0.0490.0410.030.2300.2230.21 | $\begin{array}{ccc} 70^{\circ} & 80^{\circ} \\ 2 & 0.021 & 0.008 \\ 1 & 0.184 & 0.124 \end{array}$ | 90° 0.000 0.000 |
| Short-wave shading coefficient | | 0.0736 | |
| Long-wave shading coefficient | | 0.2713 | |
| Total shading coefficient | | 0.3450 | |

| Dutside surface | | | | | Standa | rd | Generic |
|---|---|--|--|---|---------------------------------|--|--|
| missivity 0.900 Resistance (m ² K/W) 0.0299 | default | Solar abso | rptance | 0.700 | | | |
| side surface | default | Solar abso | mtance | 0.550 | | | |
| | | 00101 0000 | iptanoo | 0.000 | | | |
| vietai Cladding | | | | | | | |
| | | | | | | | |
| onstruction lavers (outside to inside) | | | | | | | |
| | 1 | | | | | | |
| Material | Thickness m | Conductivity W/(m·K) | Density kg/m² | Specific Heat Capacity J/(kg·K) | Resistance m²K/W | Vapour Resistivity GN·s/(kg·m | Category |
| CONCRETE TILES | 0.0500 | 1.1000 | 2100.0 | 837.0 | | | Tiles |
| NSULATION BOARD - Dubai Company ISOFOAM | 0.0500 | 0.0330 | 32.0 | 837.0 | | 0.000 | Insulating Materials |
| Felt/Bitumen Layers | 0.0050 | 0.5000 | 1700.0 | 1000.0 | | 0.000 | Asphalts & Other Roofing |
| SCREED | 0.0500 | 0.4100 | 1200.0 | 840.0 | | | Screeds & Renders |
| Concrete Lightweight (modified) | 0.2500 | 1.7000 | 1900.0 | 999.8 | | 0.000 | Concretes |
| | | 1 | | | | | |
| Copy Paste Cavity Insert Add Delete | e Flip | J | | | Sys | tem Materials | Project Materials |
| struction thickness 0.4050 m | U-v | alue (W/m²-K |) | | | | |
| Tatal Duralua 1 9296 m3/ AM | U-v | alue method | ASHRAE | • | | U-value | 0.5058 W/m ² K |
| | | | | | | | |
| ROOF1 Description Roof [1 Pearl] | | | | | Stan | dard | Generic |
| ROOF1 Description Roof [1 Pearl] utside surface | 🗸 default | Solar ab: | sorptance | 0.700 | Stan | dard | Generic |
| ROOF1 Description Roof [1 Pearl] utside surface | 🗸 default | Solar ab: | sorptance | 0.700 | Stan | dard | Generic |
| ROOF1 Description Roof [1 Pearl] utside surface | ✓ default ✓ default | Solar ab: Solar ab: | sorptance | 0.700 | Stan | dard | Generic |
| ROOF1 Description Roof [1 Pearl] utside surface | ✓ default ✓ default | Solar ab: Solar ab: | sorptance | 0.700 | Stan | dard | Generic |
| ROOF1 Description Roof [1 Pearl] utside surface | ☑ default ☑ default | Solar ab: Solar ab: | sorptance | 0.700 | Stan | dard | Generic |
| ROOF1 Description Roof [1 Pearl] utside surface | ☑ default ☑ default | Solar ab: Solar ab: | sorptance | 0.700 | Stan | Jard | Generic |
| ROOF1 Description Roof [1 Pearl] utside surface | ☑ default ☑ default | Solar ab: Solar ab: | sorptance | 0.700 | Stan | dard | Generic |
| ROOF1 Description Roof [1 Pearl] utside surface missivity 0.900 Resistance (m²K/W) 0.0299 side surface missivity 0.900 Resistance (m²K/W) 0.1074 Metal Cladding onstruction layers (outside to inside) 0.000 0.000 | ☑ default ☑ default | Solar ab: Solar ab: | sorptance | 0.700 | Stan | Jard | Generic |
| ROOF1 Description Roof [1 Pearl] utside surface | ✓ default ✓ default | Solar ab: Solar ab: | sorptance | 0.700 0.550 Specific | Stan | Jard | Generic |
| ROOF1 Description Roof [1 Pearl] utside surface | default default Thickness | Solar ab: Solar ab: Conductivil | sorptance sorptance | 0.700 0.550 Specific Heat | Resistanc | e Vapour Besistivih | Generic |
| ROOF1 Description Roof [1 Pearl] tside surface | ✓ default ✓ default ✓ Thickness | Solar ab: Solar ab: Conductivil W/(m/K) | sorptance sorptance | 0.700 0.550 Specific Heat Capacity | Stand | e Vapour Resistivity GN:s/(kg | Generic |
| ROOF1 Description Roof [1 Pearl] tside surface | default default Thickness m | Solar ab: Solar ab: Conductivit W/(m:K) | sorptance sorptance | 0.700 0.550 Specific Heat Capacity J/(kg·K) | Resistanc m²K/W | e Vapour Resistivity GN·s/(kg | Generic Generic |
| ROOF1 Description Roof [1 Pearl] tside surface | default default Thickness 0.0500 | Solar ab: Solar ab: Conductivil W/(m·K) 1.1000 | sorptance sorptance | 0.700 0.550 Specific Heat Capacity J/(kg/K) 837.0 | Resistanc m²K/W | e Vapour Resistivity GN-s/(kg | Generic Generic Category Tiles |
| ROOF1 Description Roof [1 Pearl] tside surface | default default Thickness 0.0500 0.2204 | Solar ab: Solar ab: Conductivil W/(m·K) 1.1000 0.0330 0.0500 | sorptance sorptance | 0.700 0.550 Specific Heat Capacity J/(kg/K) 837.0 837.0 | Resistanc m²K/W | e Vapour Resistivity GN·s/[kg | Generic Generic Category Tiles Insulating Materials |
| ROOF1 Description Roof [1 Pearl] tside surface | default default default Thickness n.0500 0.2204 0.0050 0.0204 | Solar ab: Solar ab: Conductivil W/(m·K) 1.1000 0.0330 0.5000 | 3 Density kg/m³ 2100.0 32.0 1700.0 | 0.700 0.550 Specific Heat Capacity J/(kg/K) 837.0 837.0 837.0 1000.0 | Resistanc m²K/W | e Vapour Resistivity GN·s/(kg 0.000 0.000 | Generic Generic Category Tiles Insulating Materials Asphalts & Other Roof |
| ROOF1 Description Roof [1 Pearl] tside surface | ✓ default ✓ default ✓ default ✓ 0.0500 0.2204 0.00500 0.0500 0.0500 0.0500 | Solar ab: Solar ab: Conductivil W/(m·K) 1.1000 0.0330 0.5000 0.4100 1.7000 | sorptance sorptance 3 Density kg/m ³ 2100.0 32.0 1700.0 1200.0 | 0.700 0.550 0.550 Specific Heat Capacity J/(kg/K) 837.0 837.0 837.0 837.0 837.0 837.0 837.0 | Resistanc m²K/W | e Vapour Resistivity GN·s/[kg 0.000 0.000 | Category m Tiles Insulating Materials Asphalts & Other Roofi Screeds & Renders |
| ROOF1 Description Roof [1 Pearl] Itside surface Itside surface nissivity 0.900 Resistance (m ² K/W) 0.0299 side surface Itside surface Itside surface nissivity 0.900 Resistance (m ² K/W) 0.1074 Metal Cladding Itside surface Itside surface Instruction layers (outside to inside) Itside surface Itside surface Metal Cladding Itside surface Itside surface Instruction layers (outside to inside) Itside surface Itside surface Material Itside surface Itside surface Itside surface Instruction layers (outside to inside) Itside surface Itside surface Itside surface Itside surface Itside surface Itside surface Itside surface Itside surf | default default default nhickness 0.0500 0.2204 0.0500 0.2500 | Solar ab: Solar ab: Solar ab: V/(m·K) 1.1000 0.0330 0.5000 0.4100 1.7000 | sorptance sorptance | 0.700 0.550 Specific Heat Capacity J/(kg·K) 837.0 837.0 1000.0 840.0 999.8 | Resistanc | e Vapour Resistivity GN·s/(kg 0.000 0.000 0.000 | Category Tiles Insulating Materials Asphalts & Other Roof Screeds & Renders Concretes |
| ROOF1 Description Roof [1 Pearl] Itside surface inssivity 0.900 Resistance (m ² K/W) 0.0299 side surface inssivity 0.900 Resistance (m ² K/W) 0.1074 1 Vetal Cladding Instruction layers (outside to inside) Instruction layers (outside to inside) Instruction layers (outside to inside) Material Instruction BOARD - Dubai Company ISOFOAM Instruction layers (CREED Instruction layers (company lister) CONCRETE Lightweight (modified) Instruction layers (company lister) Instruction layers (company lister) | ✓ default ✓ default ✓ default ✓ nickness m 0.0500 0.2204 0.0050 0.0500 0.2500 | Solar ab: Solar ab: Solar ab: Conductivit W/(m·K) 1.1000 0.0330 0.5000 0.4100 1.7000 | sorptance sorptance | 0.700 0.550 Specific Heat Capacity J/(kg/K) 837.0 837.0 837.0 837.0 837.0 837.0 837.0 837.0 837.0 | Resistanc m²K/W | e Vapour Resistivity GN:s/(kg 0.000 0.000 0.000 | Generic Generic Category Tiles Insulating Materials Asphalts & Other Roof Screeds & Renders Concretes |
| ROOF1 Description Roof [1 Pearl] tside surface | ✓ default ✓ default ✓ default ✓ default ✓ 0.0500 0.2204 0.0050 0.2500 0.2500 0.2500 | Solar ab: Solar ab: Solar ab: V/(m·K) 1.1000 0.0330 0.5000 0.4100 1.7000 | 3 Density kg/m ³ 2100.0 32.0 1700.0 1200.0 1900.0 | 0.700 0.550 Specific Heat Capacity J/kg/K) 837.0 1000.0 840.0 999.8 | Resistanc m ² K/W | e Vapour Resistivity GN·s/(kg 0.000 0.000 0.000 | Category m Tiles Insulating Materials Asphalts & Other Roofi Screeds & Renders Concretes |
| ROOF1 Description Roof [1 Pearl] tside surface issivity 0.900 Resistance (m ² K/W) 0.0299 ide surface issivity 0.900 Resistance (m ² K/W) 0.1074 1 ide surface issivity 0.900 Resistance (m ² K/W) 0.1074 1 ide surface issivity 0.900 Resistance (m ² K/W) 0.1074 1 idetal Cladding issivity 0.900 Resistance (m ² K/W) 0.1074 1 instruction layers (outside to inside) issues issues issues 1 1 aterial DNCRETE TILES ISULATION BOARD - Dubai Company ISOFOAM isl/Bit/Bit/Bit/Bit/Bit/Bit/Bit/Bit/Bit/Bit | ✓ default ✓ default ✓ default ✓ default ✓ nickness m 0.0500 0.2204 0.0050 0.2500 0.2500 ie Flip | Solar ab: Solar ab: Solar ab: V/(mK) 1.1000 0.0330 0.5000 0.4100 1.7000 | sorptance sorptance | 0.700 0.550 Specific Heat Capacity J/(kg·K) 837.0 837.0 1000.0 840.0 999.8 | Resistanc m ² K/w | e Vapour Resistivity GN·s/(kg 0.000 0.000 0.000 | Generic Generic Category Tiles Insulating Materials Asphalts & Other Roof Screeds & Renders Concretes als Project Materi |
| ROOF1 Description Roof [1 Pearl] tside surface issivity 0.900 Resistance (m ² K/W) 0.0299 ide surface issivity 0.900 Resistance (m ² K/W) 0.1074 1 ide surface issivity 0.900 Resistance (m ² K/W) 0.1074 1 ide surface issivity 0.900 Resistance (m ² K/W) 0.1074 1 idetal Cladding issive issive issive 0.1074 1 instruction layers (outside to inside) issive issive issive issive issive aterial DNCRETE TILES Issue Issue Issue Issue issue SULATION BOARD - Dubai Company ISOFOAM el/Bitumen Layers CREED issue | ✓ default ✓ Defaul | Solar ab: Solar ab: Solar ab: V/(mK) 1.1000 0.0330 0.5000 0.4100 1.7000 value (W/m ² value method | sorptance sorptance 3 Density kg/m² 2100.0 32.0 1700.0 1200.0 1200.0 1900.0 | 0.700 0.550 0.550 Specific Heat Capacity J/(kg·K) 837.0 837.0 837.0 837.0 837.0 837.0 837.0 837.0 837.0 837.0 | Resistanc mřK/w | e Vapour Resistivity GN's/(kg 0.000 0.000 0.000 | Generic Generic Category Tiles Insulating Materials Asphalts & Other Roofi Screeds & Renders Concretes als Project Materi |

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| | | escription Roof [2 Pear | 1J | | | | | Standa | rd | Generic |
|----------------|------------------|---------------------------------|------------|-----------|---------------|----------|----------------------|--------------------|-----------------------|--------------------------|
| Outside sur | face | | | | | | | | | |
| missivity | 0.900 | Resistance (m ² K/W) | 0.0299 | default | Solar abso | orptance | 0.700 | | | |
| nside surfa | ice | | | | | | | | | |
| missivity | 0.900 | Resistance (m²K/W) | 0.1074 | / default | Solar abso | orptance | 0.550 | | | |
| Metal Cladding | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| onstructio | on layers (outsi | ide to inside) | | | | | | | | |
| | | | | | | | Specific | | | |
| Material | | | | Thickness | Conductivity | Density | Heat | Resistance | Vapour Besistivitu | Category |
| | | | | m | W/(m·K) | kg/m² | Uapacity J/(kg·K) | m ^e K/W | GN·s/(kg·m | 000030.9 |
| CONCRET | TE TILES | | | 0.0500 | 1.1000 | 2100.0 | 837.0 | | | Tiles |
| INSULATI | ION BOARD | Dubai Company ISOFO/ | ۹M | 0.2597 | 0.0330 | 32.0 | 837.0 | | 0.000 | Insulating Materials |
| Felt/Bitum | nen Layers | | | 0.0050 | 0.5000 | 1700.0 | 1000.0 | | 0.000 | Asphalts & Other Roofing |
| SCREED | - | | | 0.0500 | 0.4100 | 1200.0 | 840.0 | | | Screeds & Renders |
| Concrete I | Lightweight (n | nodified) | | 0.2500 | 1.7000 | 1900.0 | 999.8 | | 0.000 | Concretes |
| | | | | - | | | | | | |
| | | | | | ר | | | | | |
| Сору | Paste | Cavity Insert | Add Delete | Flip | | | | Sys | stem Materials | Project Matenais |
| | thickness 0 | 6147 m | | ~U-\ | value (W/m²·K | 0 | | | | |
| nstruction. | | | | | | | | | | |
| nstruction | | | | 1 la | value method | ленрл | | | Havalue | 0 1200 W/m²-K |

Figure D 43 Roof construction details for Pearl 2-5 model.

APPENDIX E IES RESULTS

 Table E1 IES Monthly Results for Cooling Loads, Energy and Carbon for Typical Floor for Baseline Model

| | | Total CE (kgCO2) | | |
|---------------------|------------------|------------------|-------|--|
| / Room cooling plan | t sens. load (MW | | | |
| Date | | Date | | |
| Jan 01-31 | 0.9059 | Jan 01-31 | 1627 | |
| Feb 01-28 | 1.8522 | Feb 01-28 | 1817 | |
| Mar 01-31 | 4.8052 | Mar 01-31 | 2938 | |
| Apr 01-30 | 9.6783 | Apr 01-30 | 4124 | |
| May 01-31 | 14.0266 | May 01-31 | 5307 | |
| Jun 01-30 | 17.2003 | Jun 01-30 | 6621 | |
| Jul 01-31 | 18.6062 | Jul 01-31 | 7254 | |
| Aug 01-31 | 19.5397 | Aug 01-31 | 7455 | |
| Sep 01-30 | 16.8354 | Sep 01-30 | 6789 | |
| Oct 01-31 | 11.9635 | Oct 01-31 | 4927 | |
| Nov 01-30 | 7.5186 | Nov 01-30 | 3654 | |
| Dec 01-31 | 2.5366 | Dec 01-31 | 2211 | |
| Summed total | 125.4686 | Summed total | 54723 | |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|-----------|--------------------------|---------------------------------|-------------------------------|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 0.39 | 0.39 | 0.117 | 1.3244 | 3.1459 | 3.1469 |
| Feb 01-28 | 0.7601 | 0.7601 | 0.228 | 1.8169 | 3.4943 | 3.5456 |
| Mar 01-31 | 2.165 | 2.165 | 0.6495 | 3.7086 | 5.6837 | 5.6837 |
| Apr 01-30 | 4.0051 | 4.0051 | 1.2015 | 6.0666 | 7.9757 | 7.9803 |
| May 01-31 | 5.8512 | 5.8512 | 1.7554 | 8.4347 | 10.2598 | 10.2715 |
| Jun 01-30 | 7.6953 | 7.6953 | 2.3086 | 10.8642 | 12.8037 | 12.8087 |
| Jul 01-31 | 8.6786 | 8.6786 | 2.6036 | 12.1375 | 14.0311 | 14.0311 |
| Aug 01-31 | 8.9828 | 8.9828 | 2.6948 | 12.5329 | 14.4188 | 14.4188 |
| Sep 01-30 | 7.9639 | 7.9639 | 2.3892 | 11.2143 | 13.1299 | 13.1359 |
| Oct 01-31 | 5.2899 | 5.2899 | 1.587 | 7.6932 | 9.5295 | 9.5295 |
| Nov 01-30 | 3.3013 | 3.3013 | 0.9904 | 5.147 | 7.0674 | 7.0674 |
| Dec 01-31 | 1.0593 | 1.0593 | 0.3178 | 2.2731 | 4.2758 | 4.2777 |
| Total | 56.1426 | 56.1426 | 16.8428 | 83.2134 | 105.8156 | 105.897 |
Table E2 IES Monthly Results for Cooling Loads, Energy and Carbon for Typical Floor for 1 Pearl Wall Scenario

| Pearl 1 - Wall Room cooling plant | | Total CE (kgCO2) | | |
|-----------------------------------|----------|------------------|-------|--|
| sens. load | (MWh) | | | |
| Date | | Date | | |
| Jan 01-31 | 1.0853 | Jan 01-31 | 1673 | |
| Feb 01-28 | 2.017 | Feb 01-28 | 1861 | |
| Mar 01-31 | 4.7584 | Mar 01-31 | 2926 | |
| Apr 01-30 | 9.2074 | Apr 01-30 | 3996 | |
| May 01-31 | 13.1215 | May 01-31 | 5060 | |
| Jun 01-30 | 15.9749 | Jun 01-30 | 6287 | |
| Jul 01-31 | 17.2209 | Jul 01-31 | 6877 | |
| Aug 01-31 | 18.1011 | Aug 01-31 | 7063 | |
| Sep 01-30 | 15.6486 | Sep 01-30 | 6467 | |
| Oct 01-31 | 11.2546 | Oct 01-31 | 4734 | |
| Nov 01-30 | 7.2578 | Nov 01-30 | 3583 | |
| Dec 01-31 | 2.7053 | Dec 01-31 | 2257 | |
| Summed total | 118.3528 | Summed total | 52783 | |

| | | | Ap Sys heat rej | | | |
|-----------|--------------------------|---------------------------------|----------------------------|------------------------------|----------------------------|-----------------------|
| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
| Date | | | | | | |
| Jan 01-31 | 0.4588 | 0.4588 | 0.1377 | 1.4141 | 3.2354 | 3.2366 |
| Feb 01-28 | 0.8253 | 0.8253 | 0.2475 | 1.9025 | 3.5791 | 3.6313 |
| Mar 01-31 | 2.1457 | 2.1457 | 0.6437 | 3.6836 | 5.6587 | 5.6587 |
| Apr 01-30 | 3.8145 | 3.8145 | 1.1443 | 5.8187 | 7.7278 | 7.7325 |
| May 01-31 | 5.4848 | 5.4848 | 1.6454 | 7.9583 | 9.7835 | 9.7951 |
| Jun 01-30 | 7.1993 | 7.1993 | 2.1598 | 10.2193 | 12.1588 | 12.1638 |
| Jul 01-31 | 8.1179 | 8.1179 | 2.4354 | 11.4085 | 13.3022 | 13.3022 |
| Aug 01-31 | 8.4005 | 8.4005 | 2.5201 | 11.7759 | 13.6617 | 13.6617 |
| Sep 01-30 | 7.4835 | 7.4835 | 2.2451 | 10.5898 | 12.5055 | 12.5114 |
| Oct 01-31 | 5.0029 | 5.0029 | 1.5009 | 7.3201 | 9.1564 | 9.1564 |
| Nov 01-30 | 3.1958 | 3.1958 | 0.9587 | 5.0098 | 6.9302 | 6.9302 |
| Dec 01-31 | 1.1275 | 1.1275 | 0.3383 | 2.362 | 4.3645 | 4.3666 |
| total | 53.2564 | 53.2564 | 15.9769 | 79.4628 | 102.0636 | 102.1464 |

Table E3 IES Monthly Results for Cooling Loads, Energy and Carbon for Typical Floor for 2 Pearl Wall Scenario

| Pearl 2 - Wall Room cooling plant | | | Total CE (kgCO2) | | |
|-----------------------------------|----------------|-----------|------------------|--|--|
| ser | ns. load (MWh) | | | | |
| Date | | Date | | | |
| Jan 01-31 | 1.0882 | Jan 01-31 | 1674 | | |
| Feb 01-28 | 2.0195 | Feb 01-28 | 1851 | | |
| Mar 01-31 | 4.7571 | Mar 01-31 | 2925 | | |
| Apr 01-30 | 9.196 | Apr 01-30 | 3993 | | |
| May 01-31 | 13.1014 | May 01-31 | 5055 | | |
| Jun 01-30 | 15.9473 | Jun 01-30 | 6280 | | |
| Jul 01-31 | 17.1898 | Jul 01-31 | 6869 | | |
| Aug 01-31 | 18.0687 | Aug 01-31 | 7054 | | |
| Sep 01-30 | 15.6213 | Sep 01-30 | 6459 | | |
| Oct 01-31 | 11.2376 | Oct 01-31 | 4729 | | |
| Nov 01-30 | 7.2507 | Nov 01-30 | 3581 | | |
| Dec 01-31 | 2.7077 | Dec 01-31 | 2257 | | |
| Summed tot | al 118.1854 | Summed to | tal 52738 | | |

| | | | Ap Sys heat rej | | | |
|--------------|-----------------|-----------------|-----------------|--------------|-------------------|--------------|
| | Chillers energy | Ap Sys chillers | fans/pumps | Total system | Total electricity | Total energy |
| | (MWh) | energy (MWN) | energy (MWh) | energy (MWN) | (IVIVIII) | (IVIVVII) |
| Date | | | | | | |
| Jan 01-31 | 0.4599 | 0.4599 | 0.138 | 1.4155 | 3.2368 | 3.238 |
| Feb 01-28 | 0.8263 | 0.8263 | 0.2479 | 1.9039 | 3.5804 | 3.6326 |
| Mar 01-31 | 2.1451 | 2.1451 | 0.6435 | 3.6828 | 5.6579 | 5.6579 |
| Apr 01-30 | 3.8099 | 3.8099 | 1.143 | 5.8128 | 7.7218 | 7.7265 |
| May 01-31 | 5.4767 | 5.4767 | 1.643 | 7.9478 | 9.7729 | 9.7846 |
| Jun 01-30 | 7.1881 | 7.1881 | 2.1564 | 10.2048 | 12.1443 | 12.1493 |
| Jul 01-31 | 8.1053 | 8.1053 | 2.4315 | 11.3922 | 13.2858 | 13.2858 |
| Aug 01-31 | 8.3874 | 8.3874 | 2.5162 | 11.7588 | 13.6447 | 13.6447 |
| Sep 01-30 | 7.4725 | 7.4725 | 2.2417 | 10.5755 | 12.4911 | 12.4971 |
| Oct 01-31 | 4.996 | 4.995 | 1.4988 | 7.3112 | 9.1474 | 9.1474 |
| Nov 01-30 | 3.1929 | 3.1929 | 0.9579 | 5.006 | 6.9264 | 6.9264 |
| Dec 01-31 | 1.1285 | 1.1285 | 0.3385 | 2.3633 | 4.3657 | 4.3678 |
| Summed total | 53.1885 | 53.1885 | 15.9566 | 79.3745 | 101.9753 | 102.0581 |

Table E 4 IES Monthly Results for Cooling Loads, Energy and Carbon for Typical Floor for 1 Pearl Glazing Scenario

| Pearl 1 - Glazing Room cooling plant | | 1 | Total CE (kgCO2) | | |
|--------------------------------------|------------|-----------|------------------|--|--|
| sens. | load (MWh) | | | | |
| Date | | Date | | | |
| Jan 01-31 | 0.6054 | Jan 01-31 | 1547 | | |
| Feb 01-28 | 1.3424 | Feb 01-28 | 1679 | | |
| Mar 01-31 | 3.9517 | Mar 01-31 | 2707 | | |
| Apr 01-30 | 8.5225 | Apr 01-30 | 3810 | | |
| May 01-31 | 12.524 | May 01-31 | 4898 | | |
| Jun 01-30 | 15.5056 | Jun 01-30 | 6159 | | |
| Jul 01-31 | 16.8337 | Jul 01-31 | 6772 | | |
| Aug 01-31 | 17.7432 | Aug 01-31 | 6966 | | |
| Sep 01-30 | 15.2474 | Sep 01-30 | 6357 | | |
| Oct 01-31 | 10.7449 | Oct 01-31 | 4595 | | |
| Nov 01-30 | 6.5906 | Nov 01-30 | 3401 | | |
| Dec 01-31 | 2.025 | Dec 01-31 | 2072 | | |
| Summed total | 111.6365 | Summed to | tal 50963 | | |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 0.2714 | 0.2714 | 0.0814 | 1.17 | 2.9917 | 2.9924 |
| Feb 01-28 | 0.5558 | 0.5558 | 0.1667 | 1.55 | 3.2288 | 3.2787 |
| Mar 01-31 | 1.8202 | 1.8202 | 0.546 | 3.2603 | 5.2355 | 5.2355 |
| Apr 01-30 | 3.5372 | 3.5372 | 1.0612 | 5.4583 | 7.3673 | 7.372 |
| May 01-31 | 5.2429 | 5.2429 | 1.5729 | 7.6439 | 9.469 | 9.4807 |
| Jun 01-30 | 7.0093 | 7.0093 | 2.1028 | 9.9723 | 11.9118 | 11.9168 |
| Jul 01-31 | 7.9611 | 7.9611 | 2.3883 | 11.2047 | 13.0983 | 13.0983 |
| Aug 01-31 | 8.2556 | 8.2556 | 2.4767 | 11.5876 | 13.4734 | 13.4734 |
| Sep 01-30 | 7.3211 | 7.3211 | 2.1963 | 10.3787 | 12.2943 | 12.3003 |
| Oct 01-31 | 4.7965 | 4.7965 | 1.439 | 7.0519 | 8.8881 | 8.8881 |
| Nov 01-30 | 2.9256 | 2.9256 | 0.8777 | 4.6586 | 6.579 | 6.579 |
| Dec 01-31 | 0.8526 | 0.8526 | 0.2558 | 2.0042 | 4.0071 | 4.0088 |
| Summed total | 50.5493 | 50.5493 | 15.1648 | 75.9404 | 98.5444 | 98.624 |

Table E 5 IES Monthly Results for Cooling Loads, Energy and Carbon for Typical Floor for 2 Pearl Glazing Scenario

| Pearl 2 - Glazing Room cooling plant | | | Total CE (kgCO2) | | |
|--------------------------------------|----------------|-----------|------------------|--|--|
| se | ns. load (MWh) | | | | |
| Date | | Date | | | |
| Jan 01-31 | 0.4897 | Jan 01-31 | 1517 | | |
| Feb 01-28 | 1.1675 | Feb 01-28 | 1632 | | |
| Mar 01-31 | 3.7043 | Mar 01-31 | 2640 | | |
| Apr 01-30 | 8.2494 | Apr 01-30 | 3736 | | |
| May 01-31 | 12.2262 | May 01-31 | 4817 | | |
| Jun 01-30 | 15.1881 | Jun 01-30 | 6073 | | |
| Jul 01-31 | 16.5098 | Jul 01-31 | 6684 | | |
| Aug 01-31 | 17.4131 | Aug 01-31 | 6876 | | |
| Sep 01-30 | 14.9362 | Sep 01-30 | 6273 | | |
| Oct 01-31 | 10.4725 | Oct 01-31 | 4521 | | |
| Nov 01-30 | 6.3365 | Nov 01-30 | 3332 | | |
| Dec 01-31 | 1.8371 | Dec 01-31 | 2021 | | |
| Summed to | tal 108.5303 | Summed to | otal 50120 | | |

| | | | Ap Sys heat rej | | | |
|--------------|--------------------------|---------------------------------|----------------------------|------------------------------|----------------------------|-----------------------|
| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
| Date | | | | | | |
| Jan 01-31 | 0.2265 | 0.2265 | 0.068 | 1.1116 | 2.9334 | 2.9341 |
| Feb 01-28 | 0.4861 | 0.4861 | 0.1458 | 1.4589 | 3.1382 | 3.1877 |
| Mar 01-31 | 1.7203 | 1.7203 | 0.5161 | 3.1305 | 5.1056 | 5.1056 |
| Apr 01-30 | 3.4266 | 3.4266 | 1.028 | 5.3145 | 7.2236 | 7.2283 |
| May 01-31 | 5.1224 | 5.1224 | 1.5367 | 7.4872 | 9.3123 | 9.324 |
| Jun 01-30 | 6.8808 | 6.8808 | 2.0642 | 9.8052 | 11.7447 | 11.7497 |
| Jul 01-31 | 7.83 | 7.83 | 2.349 | 11.0343 | 12.9279 | 12.9279 |
| Aug 01-31 | 8.122 | 8.122 | 2.4366 | 11.4138 | 13.2997 | 13.2997 |
| Sep 01-30 | 7.1952 | 7.1952 | 2.1585 | 10.2149 | 12.1306 | 12.1365 |
| Oct 01-31 | 4.6862 | 4.6862 | 1.4059 | 6.9085 | 8.7447 | 8.7447 |
| Nov 01-30 | 2.8228 | 2.8228 | 0.8468 | 4.5249 | 6.4452 | 6.4452 |
| Dec 01-31 | 0.7767 | 0.7767 | 0.233 | 1.9055 | 3.9084 | 3.91 |
| Summed total | 49.2955 | 49.2955 | 14.7887 | 74.3098 | 96.9144 | 96.9934 |

Table E 6 IES Monthly Results for Cooling Loads, Energy and Carbon for Typical Floor for 1 Pearl Combined Scenario

| Pearl 1 Combined Room cooling plant sens, load (MWh) | | Total CE (kgCO2) | |
|---|----------|------------------|-------|
| Date | | Date | |
| Jan 01-31 | 0.7344 | Jan 01-31 | 1579 |
| Feb 01-28 | 1.4428 | Feb 01-28 | 1706 |
| Mar 01-31 | 3.8108 | Mar 01-31 | 2658 |
| Apr 01-30 | 7.9265 | Apr 01-30 | 3648 |
| May 01-31 | 11.4585 | May 01-31 | 4608 |
| Jun 01-30 | 14.0964 | Jun 01-30 | 5776 |
| Jul 01-31 | 15.2558 | Jul 01-31 | 6343 |
| Aug 01-31 | 16.104 | Aug 01-31 | 6520 |
| Sep 01-30 | 13.8825 | Sep 01-30 | 5986 |
| Oct 01-31 | 9.901 | Oct 01-31 | 4366 |
| Nov 01-30 | 6.2288 | Nov 01-30 | 3303 |
| Dec 01-31 | 2.1311 | Dec 01-31 | 2101 |
| Summed total | 102.9726 | Summed total | 48602 |

| | | | Ap Sys heat rej | | | |
|--------------|-----------------------|----------------|-----------------|--------------|-------------------|--------------|
| | А | p Sys chillers | fans/pumps | Total system | Total electricity | Total energy |
| | Chillers energy (MV e | nergy (MWh) | energy (MWh) | energy (MWh) | (MWh) | (MWh) |
| | | | | | | |
| Date | | | | | | |
| Jan 01-31 | 0.3196 | 0.3196 | 0.0959 | 1.2328 | 3.0543 | 3.0552 |
| Feb 01-28 | 0.5949 | 0.5949 | 0.1785 | 1.6017 | 3.2796 | 3.3305 |
| Mar 01-31 | 1.7629 | 1.7629 | 0.5289 | 3.186 | 5.1611 | 5.1611 |
| Apr 01-30 | 3.2959 | 3.2959 | 0.9888 | 5.1446 | 7.0537 | 7.0583 |
| May 01-31 | 4.8116 | 4.8116 | 1.4435 | 7.0831 | 8.9082 | 8.9199 |
| Jun 01-30 | 6.4388 | 6.4388 | 1.9316 | 9.2307 | 11.1703 | 11.1752 |
| Jul 01-31 | 7.3225 | 7.3225 | 2.1967 | 10.3745 | 12.2681 | 12.2681 |
| Aug 01-31 | 7.5921 | 7.5921 | 2.2776 | 10.725 | 12.6108 | 12.6108 |
| Sep 01-30 | 6.7687 | 6.7687 | 2.0306 | 9.6605 | 11.5762 | 11.5821 |
| Oct 01-31 | 4.4549 | 4.4549 | 1.3365 | 6.6077 | 8.444 | 8.444 |
| Nov 01-30 | 2.7791 | 2.7791 | 0.8337 | 4.4682 | 6.3885 | 6.3885 |
| Dec 01-31 | 0.8955 | 0.8955 | 0.2685 | 2.0602 | 4.0628 | 4.0648 |
| Summed total | 47.0364 | 47.0364 | 14.1109 | 71.3749 | 93.9775 | 94.0586 |

Table E 7 IES Monthly Results for Cooling Loads, Energy and Carbon for Typical Floor for 2 Pearl Combined Scenario

| Pearl 2 Combined Room cooling | | Total CE (kgCO2) | | |
|-------------------------------|----------|------------------|-------|--|
| plant sens. lo | ad (MWh) | D-1-1 | | |
| Date | | Date | | |
| Jan 01-31 | 0.6001 | Jan 01-31 | 1544 | |
| Feb 01-28 | 1.252 | Feb 01-28 | 1654 | |
| Mar 01-31 | 3.5373 | Mar 01-31 | 2594 | |
| Apr 01-30 | 7.6138 | Apr 01-30 | 3563 | |
| May 01-31 | 11.1075 | May 01-31 | 4512 | |
| Jun 01-30 | 13.7149 | Jun 01-30 | 5672 | |
| Jul 01-31 | 14.8636 | Jul 01-31 | 6236 | |
| Aug 01-31 | 15.7025 | Aug 01-31 | 6411 | |
| Sep 01-30 | 13.5086 | Sep 01-30 | 5884 | |
| Oct 01-31 | 9.5823 | Oct 01-31 | 4279 | |
| Nov 01-30 | 5.9424 | Nov 01-30 | 3225 | |
| Dec 01-31 | 1.9258 | Dec 01-31 | 2045 | |
| Summed total | 99.3509 | Summed total | 47619 | |

| | | | Ap Sys heat rej | | | |
|--------------|--------------------------|---------------------------------|----------------------------|------------------------------|----------------------------|-----------------------|
| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
| Date | | | | | | |
| Jan 01-31 | 0.2671 | 0.2671 | 0.0801 | 1.1645 | 2.9851 | 2.987 |
| Feb 01-28 | 0.5188 | 0.5188 | 0.1556 | 1.5023 | 3.1807 | 3.231 |
| Mar 01-31 | 1.6526 | 1.6526 | 0.4958 | 3.0425 | 5.0176 | 5.0176 |
| Apr 01-30 | 3.1693 | 3.1693 | 0.9508 | 4.9801 | 6.8891 | 6.8938 |
| May 01-31 | 4.6695 | 4.6695 | 1.4009 | 6.8984 | 8.7235 | 8.7352 |
| Jun 01-30 | 6.2844 | 6.2844 | 1.8853 | 9.03 | 10.9695 | 10.9745 |
| Jul 01-31 | 7.1637 | 7.1637 | 2.1491 | 10.1681 | 12.0617 | 12.0617 |
| Aug 01-31 | 7.4295 | 7.4295 | 2.2289 | 10.5137 | 12.3995 | 12.3995 |
| Sep 01-30 | 6.6173 | 6.6173 | 1.9852 | 9.4637 | 11.3794 | 11.3853 |
| Oct 01-31 | 4.3259 | 4.3259 | 1.2978 | 6.44 | 8.2763 | 8.2763 |
| Nov 01-30 | 2.6632 | 2.6632 | 0.799 | 4.3174 | 6.2378 | 6.2378 |
| Dec 01-31 | 0.8125 | 0.8125 | 0.2438 | 1.9523 | 3.955 | 3.9569 |
| Summed total | 45.5739 | 45.5739 | 13.6722 | 69.4731 | 92.0763 | 92.1567 |

| PW Room cool | ling plant sens. load | | Total CE | (kgCO2) | | |
|--------------|-----------------------|-----------------|-----------------|--------------|-------------------|--------------|
| (1 | MWh) | | Data | | | |
| Date | | | Date | | | |
| Jan 01-31 | 1.167 | | Jan 01-31 | 1692 | | |
| Feb 01-28 | 2.3083 | | Feb 01-28 | 1938 | | |
| Mar 01-31 | 5.3366 | | Mar 01-31 | 3082 | | |
| Apr 01-30 | 9.9375 | | Apr 01-30 | 4195 | | |
| May 01-31 | 14.0887 | | May 01-31 | 5324 | | |
| Jun 01-30 | 17.1648 | | Jun 01-30 | 6611 | | |
| Jul 01-31 | 18.4735 | | Jul 01-31 | 7218 | | |
| Aug 01-31 | 19.3478 | | Aug 01-31 | 7402 | | |
| Sep 01-30 | 16.7773 | | Sep 01-30 | 6774 | | |
| Oct 01-31 | 12.0334 | | Oct 01-31 | 4946 | | |
| Nov 01-30 | 7.7868 | | Nov 01-30 | 3727 | | |
| Dec 01-31 | 2.9138 | | Dec 01-31 | 2313 | | |
| Summed total | 127.3355 | | Summed total | 55222 | | |
| | | | | | | |
| | Chillers energy | Ap Sys chillers | Ap Sys heat rei | Total system | Total electricity | Total energy |
| | (MWh) | energy (MWh) | fans/pumps | energy (MWh) | (MWh) | (MWh) |
| | (, | 5, (111) | | one (), (, | (| (|
| Date | | | | | | |
| Jan 01-31 | 0.4876 | 0.4876 | 0.1463 | 1.4516 | 3.2728 | 3 |
| Feb 01-28 | 0.9403 | 0.9403 | 0.2821 | 2.0538 | 3.7286 | 3 |
| Mar 01-31 | 2.3791 | 2.3791 | 0.7137 | 3.9869 | 5.962 | |
| Apr 01-30 | 4.11 | 4.11 | 1.233 | 6.203 | 8.1121 | 8 |
| May 01-31 | 5.8764 | 5.8764 | 1.7629 | 8.4674 | 10.2925 | 10 |
| Jun 01-30 | 7.681 | 7.681 | 2.3043 | 10.8455 | 12.785 | |
| Jul 01-31 | 8.6249 | 8.6249 | 2,5875 | 12.0676 | 13.9612 | 13 |
| Aug 01-31 | 8.9052 | 8.9052 | 2.6715 | 12.432 | 14.3178 | 14 |
| Sep 01-30 | 7.9404 | 7.9404 | 2.3821 | 11.1837 | 13.0994 | 13 |
| | | | | | | |

5.3181

3.4099

1.2116

56.8844

1.5954

1.023

0.3635

17.0653

7.73

5.2882

2.4714

84.1811

9.5662

7.2085

4.4738

106.78

Oct 01-31

Nov 01-30

Dec 01-31

Summed total

5.3181

3.4099

1.2116

56.8844

3.2741 3.7825 5.962 8.1167 10.3042 12.79 13.9612 14.3178 13.1053

9.5662 7.2085

4.476

106.8647

Table E 9 IES Monthly Results for Cooling Loads, Energy and Carbon for Roof Floor for 1 Pearl Wall Scenario

| | | Total CE (kgCO2) | | |
|-------------------|--------------------|------------------|-------|--|
| Wall Room cooling | plant sens. load (| | | |
| Date | | Date | | |
| Jan 01-31 | 1.3934 | Jan 01-31 | 1752 | |
| Feb 01-28 | 2.525 | Feb 01-28 | 1996 | |
| Mar 01-31 | 5.3094 | Mar 01-31 | 3075 | |
| Apr 01-30 | 9.4332 | Apr 01-30 | 4058 | |
| May 01-31 | 13.1231 | May 01-31 | 5061 | |
| Jun 01-30 | 15.8496 | Jun 01-30 | 6253 | |
| Jul 01-31 | 16.9862 | Jul 01-31 | 6813 | |
| Aug 01-31 | 17.7932 | Aug 01-31 | 6979 | |
| Sep 01-30 | 15.4897 | Sep 01-30 | 6423 | |
| Oct 01-31 | 11.2562 | Oct 01-31 | 4734 | |
| Nov 01-30 | 7.4945 | Nov 01-30 | 3647 | |
| Dec 01-31 | 3.1132 | Dec 01-31 | 2368 | |
| Summed total | 119.7668 | Summed total | 53160 | |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 0.5757 | 0.5757 | 0.1727 | 1.5664 | 3.3873 | 3.3889 |
| Feb 01-28 | 1.0266 | 1.0265 | 0.308 | 2.1655 | 3.8408 | 3.8953 |
| Mar 01-31 | 2.3679 | 2.3679 | 0.7104 | 3.9724 | 5.9475 | 5.9475 |
| Apr 01-30 | 3.9059 | 3.9059 | 1.1718 | 5.9376 | 7.8467 | 7.8513 |
| May 01-31 | 5.4855 | 5.4855 | 1.6456 | 7.9592 | 9.7843 | 9.796 |
| Jun 01-30 | 7.1486 | 7.1486 | 2.1445 | 10.1534 | 12.0929 | 12.0979 |
| Jul 01-31 | 8.0229 | 8.0229 | 2.4069 | 11.285 | 13.1787 | 13.1787 |
| Aug 01-31 | 8.2758 | 8.2758 | 2.4828 | 11.6139 | 13.4997 | 13.4997 |
| Sep 01-30 | 7.4193 | 7.4193 | 2.2258 | 10.5052 | 12.4219 | 12.4278 |
| Oct 01-31 | 5.0035 | 5.0035 | 1.5011 | 7.321 | 9.1572 | 9.1572 |
| Nov 01-30 | 3.2916 | 3.2916 | 0.9875 | 5.1343 | 7.0547 | 7.0547 |
| Dec 01-31 | 1.2923 | 1.2923 | 0.3877 | 2.5766 | 4.5787 | 4.5812 |
| Summed total | 53.8155 | 53.8155 | 16.1447 | 80.1926 | 102.7904 | 102.8762 |

Table E 10 IES Monthly Results for Cooling Loads, Energy and Carbon for Roof Floor for 2 Pearl Wall Scenario

| Pearl 2 - Wall Room cooling plant | | Total CE (kgCO2) | |
|-----------------------------------|----------|------------------|-------|
| sens. load | d (MWh) | | |
| Date | | Date | |
| Jan 01-31 | 1.3978 | Jan 01-31 | 1753 |
| Feb 01-28 | 2.5293 | Feb 01-28 | 1998 |
| Mar 01-31 | 5.3089 | Mar 01-31 | 3075 |
| Apr 01-30 | 9.4209 | Apr 01-30 | 4054 |
| May 01-31 | 13.1012 | May 01-31 | 5055 |
| Jun 01-30 | 15.8192 | Jun 01-30 | 6245 |
| Jul 01-31 | 16.952 | Jul 01-31 | 6804 |
| Aug 01-31 | 17.757 | Aug 01-31 | 6969 |
| Sep 01-30 | 15.4593 | Sep 01-30 | 6415 |
| Oct 01-31 | 11.2372 | Oct 01-31 | 4729 |
| Nov 01-30 | 7.4866 | Nov 01-30 | 3645 |
| Dec 01-31 | 3.1168 | Dec 01-31 | 2369 |
| Summed total | 119.5863 | Summed total | 53110 |

| | | | Ap Sys heat rej | | | |
|--------------|-----------------|-----------------|-----------------|--------------|-------------------|--------------|
| | Chillers energy | Ap Sys chillers | fans/pumps | Total system | Total electricity | Total energy |
| | (MWh) | energy (MWh) | energy (MWh) | energy (MWh) | (MWh) | (MWh) |
| Data | | | | | | |
| Date | | | | | | |
| Jan 01-31 | 0.5774 | 0.5774 | 0.1732 | 1.5686 | 3.3895 | 3.3911 |
| Feb 01-28 | 1.0284 | 1.0284 | 0.3085 | 2.1689 | 3.8431 | 3.8976 |
| Mar 01-31 | 2.3677 | 2.3677 | 0.7103 | 3.9721 | 5.9472 | 5.9472 |
| Apr 01-30 | 3.9009 | 3.9009 | 1.1703 | 5.9312 | 7.8402 | 7.8449 |
| May 01-31 | 5.4766 | 5.4766 | 1.643 | 7.9477 | 9.7728 | 9.7845 |
| Jun 01-30 | 7.1363 | 7.1363 | 2.1409 | 10.1374 | 12.0769 | 12.0819 |
| Jul 01-31 | 8.009 | 8.009 | 2.4027 | 11.267 | 13.1606 | 13.1606 |
| Aug 01-31 | 8.2612 | 8.2612 | 2.4784 | 11.5948 | 13.4806 | 13.4806 |
| Sep 01-30 | 7.4069 | 7.4069 | 2.2221 | 10.4902 | 12.4059 | 12.4118 |
| Oct 01-31 | 4.9958 | 4.9958 | 1.4987 | 7.3109 | 9.1472 | 9.1472 |
| Nov 01-30 | 3.2884 | 3.2884 | 0.9865 | 5.1301 | 7.0505 | 7.0505 |
| Dec 01-31 | 1.2937 | 1.2937 | 0.3881 | 2.5785 | 4.5806 | 4.5831 |
| Summed total | 53.7423 | 53.7423 | 16.1227 | 80.0975 | 102.6952 | 102.781 |

Table E 11 IES Monthly Results for Cooling Loads, Energy and Carbon for Roof Floor for 1 Pearl Glazing Scenario

| Pearl 1 - Glazing Room cooling plant | | Total CE (kgCO2) | |
|--------------------------------------|-----------|------------------|-------|
| Date | | Date | |
| lan 01-31 | 0.8382 | an 01-31 | 1604 |
| Feb 01-28 | 1 7601 | Feb 01-28 | 1790 |
| Mar 01-31 | 4 4 3 9 5 | Mar 01-31 | 2838 |
| Anr 01-30 | 8 719 | Apr 01-30 | 3863 |
| May 01-31 | 12 4942 | May 01-31 | 4890 |
| Jun 01-30 | 15.3592 | Jun 01-30 | 6120 |
| Jul 01-31 | 16.5814 | Jul 01-31 | 6703 |
| Aug 01-31 | 17.4201 | Aug 01-31 | 6878 |
| Sep 01-30 | 15.0777 | Sep 01-30 | 6311 |
| Oct 01-31 | 10.7339 | Oct 01-31 | 4592 |
| Nov 01-30 | 6.8079 | Nov 01-30 | 3460 |
| Dec 01-31 | 2.376 | Dec 01-31 | 2167 |
| Summed total | 112.6073 | Summed total | 51216 |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 0.3559 | 0.3559 | 0.1068 | 1.2802 | 3.1016 | 3.1027 |
| Feb 01-28 | 0.7193 | 0.7193 | 0.2158 | 1.7657 | 3.4414 | 3.4945 |
| Mar 01-31 | 2.0161 | 2.0161 | 0.6048 | 3.5151 | 5.4902 | 5.4902 |
| Apr 01-30 | 3.6168 | 3.6168 | 1.085 | 5.5617 | 7.4708 | 7.4755 |
| May 01-31 | 5.2309 | 5.2309 | 1.5693 | 7.6282 | 9.4533 | 9.465 |
| Jun 01-30 | 6.95 | 6.95 | 2.085 | 9.8953 | 11.8348 | 11.8398 |
| Jul 01-31 | 7.859 | 7.859 | 2.3577 | 11.072 | 12.9656 | 12.9656 |
| Aug 01-31 | 8.1248 | 8.1248 | 2.4375 | 11.4176 | 13.3034 | 13.3034 |
| Sep 01-30 | 7.2524 | 7.2524 | 2.1757 | 10.2894 | 12.205 | 12.211 |
| Oct 01-31 | 4.792 | 4.792 | 1.4376 | 7.0451 | 8.8823 | 8.8823 |
| Nov 01-30 | 3.0136 | 3.0136 | 0.9041 | 4.7729 | 6.6933 | 6.6933 |
| Dec 01-31 | 0.9941 | 0.9941 | 0.2982 | 2.1884 | 4.191 | 4.193 |
| Summed total | 50.925 | 50.925 | 15.2775 | 76.4326 | 99.0327 | 99.1162 |

Table E 12 IES Monthly Results for Cooling Loads, Energy and Carbon for Roof Floor for 2 Pearl Glazing Scenario

| Pearl 2 - Glazing Room cooling plant | | Total CE (kgCO2) | |
|--------------------------------------|----------|------------------|-------|
| sens. Ioa | | D. L. | |
| Date | | Date | |
| Jan 01-31 | 0.6995 | Jan 01-31 | 1567 |
| Feb 01-28 | 1.5615 | Feb 01-28 | 1736 |
| Mar 01-31 | 4.1722 | Mar 01-31 | 2766 |
| Apr 01-30 | 8.4287 | Apr 01-30 | 3784 |
| May 01-31 | 12.1762 | May 01-31 | 4803 |
| Jun 01-30 | 15.0194 | Jun 01-30 | 6027 |
| Jul 01-31 | 16.2347 | Jul 01-31 | 6609 |
| Aug 01-31 | 17.0655 | Aug 01-31 | 6781 |
| Sep 01-30 | 14.744 | Sep 01-30 | 6220 |
| Oct 01-31 | 10.4425 | Oct 01-31 | 4513 |
| Nov 01-30 | 6.5377 | Nov 01-30 | 3387 |
| Dec 01-31 | 2.1702 | Dec 01-31 | 2111 |
| Summed total | 109.2521 | Summed total | 50305 |

| | | | Ap Sys heat rej | | | |
|--------------|--------------------------|---------------------------------|----------------------------|------------------------------|----------------------------|-----------------------|
| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
| Data | | | | | | |
| Date | | | | | | |
| Jan 01-31 | 0.3013 | 0.3013 | 0.0904 | 1.2092 | 3.0306 | 3.0317 |
| Feb 01-28 | 0.6396 | 0.6396 | 0.1919 | 1.6617 | 3.3378 | 3.3905 |
| Mar 01-31 | 1.908 | 1.908 | 0.5724 | 3.3745 | 5.3496 | 5.3496 |
| Apr 01-30 | 3.4992 | 3.4992 | 1.0498 | 5.4089 | 7.318 | 7.3227 |
| May 01-31 | 5.1021 | 5.1021 | 1.5306 | 7.4609 | 9.286 | 9.2977 |
| Jun 01-30 | 6.8125 | 6.8125 | 2.0437 | 9.7165 | 11.656 | 11.661 |
| Jul 01-31 | 7.7187 | 7.7187 | 2.3156 | 10.8895 | 12.7832 | 12.7832 |
| Aug 01-31 | 7.9813 | 7.9813 | 2.3944 | 11.231 | 13.1168 | 13.1168 |
| Sep 01-30 | 7.1174 | 7.1174 | 2.1352 | 10.1138 | 12.0295 | 12.0354 |
| Oct 01-31 | 4.6741 | 4.6741 | 1.4022 | 6.8927 | 8.729 | 8.729 |
| Nov 01-30 | 2.9042 | 2.9042 | 0.8713 | 4.6307 | 6.5511 | 6.5511 |
| Dec 01-31 | 0.9108 | 0.9108 | 0.2732 | 2.0802 | 4.0828 | 4.0847 |
| Summed total | 49.5692 | 49.5692 | 14.8708 | 74.6696 | 97.2702 | 97.3532 |

Table E 13 IES Monthly Results for Cooling Loads, Energy and Carbon for Roof Floor for 1 Pearl Roof Scenario

| Pearl 1 - Roof Room cooling plant | | Total CE (kgCC | 02) |
|-----------------------------------|----------|----------------|-------|
| sens. loa | d (MWh) | | |
| Date | | Date | |
| Jan 01-31 | 1.2513 | Jan 01-31 | 1714 |
| Feb 01-28 | 2.3366 | Feb 01-28 | 1946 |
| Mar 01-31 | 5.2117 | Mar 01-31 | 3048 |
| Apr 01-30 | 9.6118 | Apr 01-30 | 4106 |
| May 01-31 | 13.5508 | May 01-31 | 5177 |
| Jun 01-30 | 16.4546 | Jun 01-30 | 6418 |
| Jul 01-31 | 17.6706 | Jul 01-31 | 7000 |
| Aug 01-31 | 18.535 | Aug 01-31 | 7181 |
| Sep 01-30 | 16.0898 | Sep 01-30 | 6587 |
| Oct 01-31 | 11.6279 | Oct 01-31 | 4835 |
| Nov 01-30 | 7.6285 | Nov 01-30 | 3684 |
| Dec 01-31 | 2.9838 | Dec 01-31 | 2332 |
| Summed total | 122.9523 | Summed total | 54029 |

| | | | Ap Sys heat rej | | | |
|--------------|--------------------------|---------------------------------|----------------------------|------------------------------|----------------------------|-----------------------|
| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
| Date | | | | | | |
| lan 01 21 | 0 5004 | 0 5004 | 0.1561 | 1 4042 | 2 2454 | 2 2100 |
| Jan 01-31 | 0.5204 | 0.5204 | 0.1561 | 1.4943 | 3.3154 | 3.3108 |
| Feb 01-28 | 0.9515 | 0.9515 | 0.2855 | 2.0684 | 3.7432 | 3.7971 |
| Mar 01-31 | 2.3285 | 2.3285 | 0.6985 | 3.9212 | 5.8963 | 5.8963 |
| Apr 01-30 | 3.9782 | 3.9782 | 1.1935 | 6.0316 | 7.9407 | 7.9453 |
| May 01-31 | 5.6587 | 5.6587 | 1.6976 | 8.1843 | 10.0094 | 10.0211 |
| Jun 01-30 | 7.3935 | 7.3935 | 2.218 | 10.4718 | 12.4113 | 12.4163 |
| Jul 01-31 | 8.3 | 8.3 | 2.49 | 11.6452 | 13.5388 | 13.5388 |
| Aug 01-31 | 8.5762 | 8.5762 | 2.5729 | 12.0043 | 13.8901 | 13.8901 |
| Sep 01-30 | 7.6622 | 7.6622 | 2.2986 | 10.822 | 12.7377 | 12.7436 |
| Oct 01-31 | 5.154 | 5.154 | 1.5462 | 7.5166 | 9.3528 | 9.3528 |
| Nov 01-30 | 3.3458 | 3.3458 | 1.0037 | 5.2049 | 7.1252 | 7.1252 |
| Dec 01-31 | 1.24 | 1.24 | 0.372 | 2.5084 | 4.5107 | 4.5129 |
| Summed total | 55.1088 | 55.1088 | 16.5326 | 81.8729 | 104.4717 | 104.5565 |

Table E 14 IES Monthly Results for Cooling Loads, Energy and Carbon for Roof Floor for 2 Pearl Roof Scenario

| Pearl 2 - Roof Room cooling plant | | т | otal CE (kgCO2) |
|-----------------------------------|------------|------------|-----------------|
| sens. | load (MWh) | | |
| Date | | Date | |
| Jan 01-31 | 1.2564 | Jan 01-31 | 1716 |
| Feb 01-28 | 2.3385 | Feb 01-28 | 1946 |
| Mar 01-31 | 5.2049 | Mar 01-31 | 3047 |
| Apr 01-30 | 9.5933 | Apr 01-30 | 4101 |
| May 01-31 | 13.5202 | May 01-31 | 5169 |
| Jun 01-30 | 16.414 | Jun 01-30 | 6407 |
| Jul 01-31 | 17.6247 | Jul 01-31 | 6987 |
| Aug 01-31 | 18.4884 | Aug 01-31 | 7169 |
| Sep 01-30 | 16.0504 | Sep 01-30 | 6576 |
| Oct 01-31 | 11.6047 | Oct 01-31 | 4829 |
| Nov 01-30 | 7.6196 | Nov 01-30 | 3681 |
| Dec 01-31 | 2.988 | Dec 01-31 | 2334 |
| Summed total | 122.7032 | Summed tot | al 53961 |

| | | | Ap Sys heat rej | | | |
|--------------|--------------------------|---------------------------------|----------------------------|------------------------------|----------------------------|-----------------------|
| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
| Date | | | | | | |
| Jan 01-31 | 0.5224 | 0.5224 | 0.1567 | 1.4969 | 3.318 | 3.3194 |
| Feb 01-28 | 0.9523 | 0.9523 | 0.2857 | 2.0694 | 3.7442 | 3.7981 |
| Mar 01-31 | 2.3257 | 2.3257 | 0.6977 | 3.9176 | 5.8927 | 5.8927 |
| Apr 01-30 | 3.9707 | 3.9707 | 1.1912 | 6.0219 | 7.931 | 7.9356 |
| May 01-31 | 5.6463 | 5.6463 | 1.6939 | 8.1682 | 9.9933 | 10.005 |
| Jun 01-30 | 7.3771 | 7.3771 | 2.2131 | 10.4504 | 12.3899 | 12.3949 |
| Jul 01-31 | 8.2814 | 8.2814 | 2.4844 | 11.6211 | 13.5147 | 13.5147 |
| Aug 01-31 | 8.5573 | 8.5573 | 2.5672 | 11.9798 | 13.8656 | 13.8656 |
| Sep 01-30 | 7.6462 | 7.6462 | 2.2939 | 10.8013 | 12.7169 | 12.7229 |
| Oct 01-31 | 5.1446 | 5.1446 | 1.5434 | 7.5044 | 9.3406 | 9.3406 |
| Nov 01-30 | 3.3422 | 3.3422 | 1.0027 | 5.2001 | 7.1205 | 7.1205 |
| Dec 01-31 | 1.2417 | 1.2417 | 0.3725 | 2.5106 | 4.5129 | 4.5152 |
| Summed total | 55.0079 | 55.0079 | 16.5024 | 81.7417 | 104.3404 | 104.4252 |

Table E 15 IES Monthly Results for Cooling Loads, Energy and Carbon for Roof Floor for 1 Pearl Combined Scenario

| Pearl 1 Combined Room cooling | | Total CE (kgCO2) | |
|-------------------------------|---------|------------------|-------|
| Date | | Date | |
| Jan 01-31 | 1.1086 | Jan 01-31 | 1674 |
| Feb 01-28 | 1.9213 | Feb 01-28 | 1832 |
| Mar 01-31 | 4.127 | Mar 01-31 | 2753 |
| Apr 01-30 | 7.6222 | Apr 01-30 | 3565 |
| May 01-31 | 10.621 | May 01-31 | 4380 |
| Jun 01-30 | 12.8833 | Jun 01-30 | 5446 |
| Jul 01-31 | 13.8119 | Jul 01-31 | 5950 |
| Aug 01-31 | 14.5427 | Aug 01-31 | 6095 |
| Sep 01-30 | 12.6582 | Sep 01-30 | 5653 |
| Oct 01-31 | 9.2372 | Oct 01-31 | 4185 |
| Nov 01-30 | 6.1532 | Nov 01-30 | 3282 |
| Dec 01-31 | 2.5666 | Dec 01-31 | 2219 |
| Summed total | 97.2532 | Summed total | 47034 |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 0.4597 | 0.4597 | 0.1379 | 1.4154 | 3.2365 | 3.2379 |
| Feb 01-28 | 0.7826 | 0.7825 | 0.2348 | 1.8488 | 3.5236 | 3.5775 |
| Mar 01-31 | 1.8894 | 1.8894 | 0.5668 | 3.3504 | 5.3255 | 5.3255 |
| Apr 01-30 | 3.1727 | 3.1727 | 0.9518 | 4.9844 | 6.8935 | 6.8982 |
| May 01-31 | 4.4726 | 4.4726 | 1.3418 | 6.6424 | 8.4675 | 8.4792 |
| Jun 01-30 | 5.9478 | 5.9478 | 1.7843 | 8.5924 | 10.5319 | 10.5369 |
| Jul 01-31 | 6.7379 | 6.7379 | 2.0214 | 9.6146 | 11.5082 | 11.5082 |
| Aug 01-31 | 6.9597 | 6.9597 | 2.0879 | 9.9028 | 11.7887 | 11.7887 |
| Sep 01-30 | 6.273 | 6.273 | 1.8819 | 9.0161 | 10.9317 | 10.9377 |
| Oct 01-31 | 4.1862 | 4.1862 | 1.2559 | 6.2584 | 8.0947 | 8.0947 |
| Nov 01-30 | 2.7485 | 2.7485 | 0.8245 | 4.4284 | 6.3488 | 6.3488 |
| Dec 01-31 | 1.0711 | 1.0711 | 0.3213 | 2.2891 | 4.2912 | 4.2937 |
| Summed total | 44.7012 | 44.7012 | 13.4104 | 68.3432 | 90.9418 | 91.0268 |

Table E 16 IES Monthly Results for Cooling Loads, Energy and Carbon for Roof Floor for 2 Pearl Combined Scenario

| Pearl 2 Combined Room cooling | | Total CE (kgCO2) | |
|-------------------------------|-----------|------------------|-------|
| plant sens. I | oad (MWh) | | |
| Date | | Date | |
| Jan 01-31 | 0.9447 | Jan 01-31 | 1630 |
| Feb 01-28 | 1.6936 | Feb 01-28 | 1771 |
| Mar 01-31 | 3.8046 | Mar 01-31 | 2655 |
| Apr 01-30 | 7.2414 | Apr 01-30 | 3461 |
| May 01-31 | 10.1765 | May 01-31 | 4259 |
| Jun 01-30 | 12.3865 | Jun 01-30 | 5311 |
| Jul 01-31 | 13.2956 | Jul 01-31 | 5809 |
| Aug 01-31 | 14.0105 | Aug 01-31 | 5950 |
| Sep 01-30 | 12.1697 | Sep 01-30 | 5520 |
| Oct 01-31 | 8.8378 | Oct 01-31 | 4076 |
| Nov 01-30 | 5.8148 | Nov 01-30 | 3190 |
| Dec 01-31 | 2.333 | Dec 01-31 | 2156 |
| Summed total | 92.7087 | Summed total | 45798 |

| | | | Ap Sys heat rej | | | |
|--------------|-----------------|-----------------|-----------------|--------------|-------------------|--------------|
| | Chillers energy | Ap Sys chillers | fans/pumps | Total system | Total electricity | Total energy |
| | (MWh) | energy (MWh) | energy (MWh) | energy (MWh) | (MWh) | (MWh) |
| Date | | | | | | |
| Jan 01-31 | 0.3943 | 0.3943 | 0.1183 | 1.3303 | 3.1515 | 3.1528 |
| Feb 01-28 | 0.6909 | 0.6909 | 0.2073 | 1.7293 | 3.4044 | 3.458 |
| Mar 01-31 | 1.759 | 1.759 | 0.5277 | 3.1809 | 5.156 | 5.156 |
| Apr 01-30 | 3.0185 | 3.0185 | 0.9056 | 4.784 | 6.6931 | 6.6978 |
| May 01-31 | 4.2926 | 4.2926 | 1.2878 | 6.4084 | 8.2335 | 8.2452 |
| Jun 01-30 | 5.7467 | 5.7467 | 1.724 | 8.331 | 10.2705 | 10.2755 |
| Jul 01-31 | 6.5289 | 6.5289 | 1.9587 | 9.3429 | 11.2365 | 11.2365 |
| Aug 01-31 | 6.7441 | 6.7441 | 2.0232 | 9.6226 | 11.5084 | 11.5084 |
| Sep 01-30 | 6.0751 | 6.0751 | 1.8225 | 8.7589 | 10.6745 | 10.6805 |
| Oct 01-31 | 4.0245 | 4.0245 | 1.2074 | 6.0483 | 7.8845 | 7.8845 |
| Nov 01-30 | 2.6116 | 2.6116 | 0.7835 | 4.2503 | 6.1707 | 6.1707 |
| Dec 01-31 | 0.9766 | 0.9765 | 0.293 | 2.1652 | 4.1683 | 4.1708 |
| Summed total | 42.8629 | 42.8629 | 12.8589 | 65.9531 | 88.552 | 88.6367 |

| PW Room cooling plant sens. load | | Total CE (kgCO2) | | |
|----------------------------------|----------|------------------|--------|--|
| (M) | Wh) | | | |
| Date | | Date | | |
| Jan 01-31 | 4.8277 | Jan 01-31 | 3745 | |
| Feb 01-28 | 7.1878 | Feb 01-28 | 4283 | |
| Mar 01-31 | 12.3987 | Mar 01-31 | 6256 | |
| Apr 01-30 | 19.5385 | Apr 01-30 | 7945 | |
| May 01-31 | 26.0515 | May 01-31 | 9696 | |
| Jun 01-30 | 30.8737 | Jun 01-30 | 11719 | |
| Jul 01-31 | 32.9321 | Jul 01-31 | 12720 | |
| Aug 01-31 | 34.3809 | Aug 01-31 | 13036 | |
| Sep 01-30 | 30.1718 | Sep 01-30 | 11973 | |
| Oct 01-31 | 22.7376 | Oct 01-31 | 9083 | |
| Nov 01-30 | 16.3251 | Nov 01-30 | 7249 | |
| Dec 01-31 | 8.2974 | Dec 01-31 | 4944 | |
| Summed total | 245.7228 | Summed total | 102649 | |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|-------------------------------|------------------------------|----------------------------|-----------------------|
| | | 0, () | | 0, () | . , | |
| Date | | | | | | |
| Jan 01-31 | 1.969 | 1.969 | 0.5907 | 3.7585 | 7.2432 | 7.2457 |
| Feb 01-28 | 2.9151 | 2.9151 | 0.8745 | 5.0179 | 8.2502 | 8.339 |
| Mar 01-31 | 5.3629 | 5.3629 | 1.6089 | 8.282 | 12.1014 | 12.1014 |
| Apr 01-30 | 8.0453 | 8.0453 | 2.4136 | 11.7196 | 15.3654 | 15.3729 |
| May 01-31 | 10.8182 | 10.8182 | 3.2455 | 15.2792 | 18.7473 | 18.7664 |
| Jun 01-30 | 13.6593 | 13.6593 | 4.0978 | 19.0186 | 22.6637 | 22.6718 |
| Jul 01-31 | 15.1512 | 15.1512 | 4.5453 | 20.9498 | 24.6031 | 24.6031 |
| Aug 01-31 | 15.6213 | 15.6213 | 4.6864 | 21.5609 | 25.2142 | 25.2142 |
| Sep 01-30 | 14.0371 | 14.0371 | 4.2111 | 19.5113 | 23.1548 | 23.1646 |
| Oct 01-31 | 9.9111 | 9.9111 | 2.9733 | 14.0808 | 17.568 | 17.568 |
| Nov 01-30 | 7.0113 | 7.0113 | 2.1034 | 10.3681 | 14.0213 | 14.0213 |
| Dec 01-31 | 3.4085 | 3.4085 | 1.0226 | 5.7451 | 9.5607 | 9.5644 |
| Summed total | 107.9103 | 107.9103 | 32.3731 | 155.2918 | 198.4932 | 198.6329 |

Table E 18 IES Monthly Results for Cooling Loads, Energy and Carbon for GF + Mezz Floor for 1 Pearl Wall Scenario

| Pearl 1 - Wall Room cooling plant | | Total CE (kgCO2) | | |
|-----------------------------------|----------|------------------|--------|--|
| sens. load | l (MWh) | | | |
| Date | | Date | | |
| Jan 01-31 | 5.3563 | Jan 01-31 | 3886 | |
| Feb 01-28 | 7.6822 | Feb 01-28 | 4417 | |
| Mar 01-31 | 12.5156 | Mar 01-31 | 6288 | |
| Apr 01-30 | 18.9078 | Apr 01-30 | 7774 | |
| May 01-31 | 24.7172 | May 01-31 | 9333 | |
| Jun 01-30 | 29.0255 | Jun 01-30 | 11216 | |
| Jul 01-31 | 30.8381 | Jul 01-31 | 12150 | |
| Aug 01-31 | 32.1874 | Aug 01-31 | 12439 | |
| Sep 01-30 | 28.3966 | Sep 01-30 | 11490 | |
| Oct 01-31 | 21.7249 | Oct 01-31 | 8807 | |
| Nov 01-30 | 16.059 | Nov 01-30 | 7177 | |
| Dec 01-31 | 8.7731 | Dec 01-31 | 5073 | |
| Summed total | 236.1836 | Summed total | 100049 | |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 2.1786 | 2.1786 | 0.6536 | 4.0313 | 7.5157 | 7.5185 |
| Feb 01-28 | 3.1137 | 3.1137 | 0.9341 | 5.2769 | 8.5083 | 8.598 |
| Mar 01-31 | 5.41 | 5.41 | 1.623 | 8.3433 | 12.1626 | 12.1626 |
| Apr 01-30 | 7.7899 | 7.7899 | 2.337 | 11.3877 | 15.0334 | 15.041 |
| May 01-31 | 10.2781 | 10.2781 | 3.0834 | 14.5769 | 18.045 | 18.0641 |
| Jun 01-30 | 12.9112 | 12.9112 | 3.8733 | 18.046 | 21.6911 | 21.6993 |
| Jul 01-31 | 14.3035 | 14.3035 | 4.2911 | 19.8479 | 23.5012 | 23.5012 |
| Aug 01-31 | 14.7331 | 14.7331 | 4.4199 | 20.4063 | 24.0596 | 24.0596 |
| Sep 01-30 | 13.3184 | 13.3184 | 3.9955 | 18.577 | 22.2205 | 22.2303 |
| Oct 01-31 | 9.5012 | 9.5012 | 2.8503 | 13.5478 | 17.0351 | 17.035 |
| Nov 01-30 | 6.9036 | 6.9036 | 2.0711 | 10.228 | 13.8813 | 13.8813 |
| Dec 01-31 | 3.601 | 3.601 | 1.0803 | 5.9957 | 9.8109 | 9.815 |
| Summed total | 104.0423 | 104.0423 | 31.2127 | 150.2647 | 193.4648 | 193.6059 |

Table E 19 IES Monthly Results for Cooling Loads, Energy and Carbon for GF + Mezz Floor for 2 Pearl Wall Scenario

| Pearl 2 - Wall Room cooling plant | | Total CE (kgCO2) | | |
|-----------------------------------|----------|------------------|-------|--|
| sens. loa | d (MWh) | | | |
| Date | | Date | | |
| Jan 01-31 | 5.3686 | Jan 01-31 | 3889 | |
| Feb 01-28 | 7.6938 | Feb 01-28 | 4420 | |
| Mar 01-31 | 12.519 | Mar 01-31 | 6289 | |
| Apr 01-30 | 18.892 | Apr 01-30 | 7769 | |
| May 01-31 | 24.686 | May 01-31 | 9325 | |
| Jun 01-30 | 28.9814 | Jun 01-30 | 11204 | |
| Jul 01-31 | 30.7884 | Jul 01-31 | 12137 | |
| Aug 01-31 | 32.1343 | Aug 01-31 | 12424 | |
| Sep 01-30 | 28.3532 | Sep 01-30 | 11478 | |
| Oct 01-31 | 21.6993 | Oct 01-31 | 8800 | |
| Nov 01-30 | 16.0512 | Nov 01-30 | 7175 | |
| Dec 01-31 | 8.7834 | Dec 01-31 | 5076 | |
| Summed total | 235.9506 | Summed total | 99986 | |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 2.1835 | 2.1835 | 0.655 | 4.0376 | 7.5221 | 7.5249 |
| Feb 01-28 | 3.1183 | 3.1183 | 0.9355 | 5.2829 | 8.5144 | 8.6041 |
| Mar 01-31 | 5.4114 | 5.4114 | 1.6234 | 8.3451 | 12.1644 | 12.1644 |
| Apr 01-30 | 7.7835 | 7.7835 | 2.3351 | 11.3794 | 15.0252 | 15.0327 |
| May 01-31 | 10.2654 | 10.2654 | 3.0796 | 14.5605 | 18.0286 | 18.0477 |
| Jun 01-30 | 12.8933 | 12.8933 | 3.868 | 18.0227 | 21.6678 | 21.676 |
| Jul 01-31 | 14.2834 | 14.2834 | 4.285 | 19.8217 | 23.475 | 23.475 |
| Aug 01-31 | 14.7116 | 14.7116 | 4.4135 | 20.3784 | 24.0317 | 24.0317 |
| Sep 01-30 | 13.3008 | 13.3008 | 3.9903 | 18.5542 | 22.1977 | 22.2074 |
| Oct 01-31 | 9.4908 | 9.4908 | 2.8472 | 13.5343 | 17.0216 | 17.0216 |
| Nov 01-30 | 6.9005 | 6.9005 | 2.0701 | 10.2239 | 13.8772 | 13.8772 |
| Dec 01-31 | 3.6052 | 3.6052 | 1.0816 | 6.0011 | 9.8164 | 9.8205 |
| Summed total | 103.9478 | 103.9478 | 31.1843 | 150.142 | 193.342 | 193.4831 |

Table E 20 IES Monthly Results for Cooling Loads, Energy and Carbon for GF + Mezz Floor for 1 Pearl Glazing Scenario

| Pearl 1 - Glazing | Room cooling plant | | Fotal CE (kgCO2) |
|-------------------|--------------------|--------------|------------------|
| sens. Io | ad (ivivvn) | | |
| Date | | Date | |
| Jan 01-31 | 3.9118 | Jan 01-31 | 3496 |
| Feb 01-28 | 5.6525 | Feb 01-28 | 3865 |
| Mar 01-31 | 9.8998 | Mar 01-31 | 5577 |
| Apr 01-30 | 15.8946 | Apr 01-30 | 6954 |
| May 01-31 | 21.227 | May 01-31 | 8383 |
| Jun 01-30 | 25.2645 | Jun 01-30 | 10193 |
| Jul 01-31 | 26.9905 | Jul 01-31 | 11103 |
| Aug 01-31 | 28.3108 | Aug 01-31 | 11384 |
| Sep 01-30 | 24.8183 | Sep 01-30 | 10516 |
| Oct 01-31 | 18.6616 | Oct 01-31 | 7974 |
| Nov 01-30 | 13.3182 | Nov 01-30 | 6431 |
| Dec 01-31 | 6.7517 | Dec 01-31 | 4523 |
| Summed total | 200.7012 | Summed total | 90399 |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 1.5982 | 1.5982 | 0.4795 | 3.2763 | 6.7612 | 6.7635 |
| Feb 01-28 | 2.2939 | 2.2939 | 0.6882 | 4.2096 | 7.4426 | 7.5308 |
| Mar 01-31 | 4.3515 | 4.3515 | 1.3054 | 6.9672 | 10.7865 | 10.7865 |
| Apr 01-30 | 6.57 | 6.57 | 1.971 | 9.8018 | 13.4476 | 13.4551 |
| May 01-31 | 8.8651 | 8.8651 | 2.6595 | 12.7401 | 16.2081 | 16.2273 |
| Jun 01-30 | 11.3886 | 11.3886 | 3.4166 | 16.0666 | 19.7117 | 19.7199 |
| Jul 01-31 | 12.746 | 12.746 | 3.8238 | 17.8231 | 21.4764 | 21.4764 |
| Aug 01-31 | 13.1639 | 13.1639 | 3.9492 | 18.3664 | 22.0196 | 22.0196 |
| Sep 01-30 | 11.8699 | 11.8699 | 3.561 | 16.694 | 20.3375 | 20.3473 |
| Oct 01-31 | 8.261 | 8.261 | 2.4783 | 11.9356 | 15.4228 | 15.4228 |
| Nov 01-30 | 5.794 | 5.794 | 1.7382 | 8.7855 | 12.4387 | 12.4387 |
| Dec 01-31 | 2.7828 | 2.7828 | 0.8348 | 4.9316 | 8.7472 | 8.7509 |
| Summed total | 89.6848 | 89.6848 | 26.9054 | 131.5977 | 174.8001 | 174.9389 |

Table E 21 IES Monthly Results for Cooling Loads, Energy and Carbon for GF + Mezz Floor for 2 Pearl Glazing Scenario

| Pearl 2 - GlazingRoom cooling plant | | Total CE (kgCO2) | |
|-------------------------------------|----------|------------------|-------|
| sens. loa | ad (MWh) | | |
| Date | | Date | |
| Jan 01-31 | 3.3067 | Jan 01-31 | 3332 |
| Feb 01-28 | 4.907 | Feb 01-28 | 3663 |
| Mar 01-31 | 8.9546 | Mar 01-31 | 5320 |
| Apr 01-30 | 14.875 | Apr 01-30 | 6676 |
| May 01-31 | 20.1106 | May 01-31 | 8080 |
| Jun 01-30 | 24.0566 | Jun 01-30 | 9864 |
| Jul 01-31 | 25.7521 | Jul 01-31 | 10766 |
| Aug 01-31 | 27.0394 | Aug 01-31 | 11038 |
| Sep 01-30 | 23.6206 | Sep 01-30 | 10191 |
| Oct 01-31 | 17.607 | Oct 01-31 | 7687 |
| Nov 01-30 | 12.3339 | Nov 01-30 | 6163 |
| Dec 01-31 | 5.978 | Dec 01-31 | 4313 |
| Summed total | 188.5416 | Summed total | 87092 |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 1.3547 | 1.3547 | 0.4064 | 2.9597 | 6.4447 | 6.4469 |
| Feb 01-28 | 1.9929 | 1.9929 | 0.5979 | 3.8178 | 7.0513 | 7.1389 |
| Mar 01-31 | 3.969 | 3.969 | 1.1907 | 6.4699 | 10.2893 | 10.2893 |
| Apr 01-30 | 6.1572 | 6.1572 | 1.8472 | 9.2652 | 12.911 | 12.9185 |
| May 01-31 | 8.4131 | 8.4131 | 2.5239 | 12.1525 | 15.6206 | 15.6397 |
| Jun 01-30 | 10.8996 | 10.8996 | 3.2699 | 15.431 | 19.0761 | 19.0843 |
| Jul 01-31 | 12.2447 | 12.2447 | 3.6734 | 17.1714 | 20.8247 | 20.8247 |
| Aug 01-31 | 12.6492 | 12.6492 | 3.7948 | 17.6973 | 21.3506 | 21.3506 |
| Sep 01-30 | 11.3851 | 11.3851 | 3.4155 | 16.0637 | 19.7072 | 19.717 |
| Oct 01-31 | 7.8341 | 7.8341 | 2.3502 | 11.3806 | 14.8678 | 14.8678 |
| Nov 01-30 | 5.3955 | 5.3955 | 1.6186 | 8.2674 | 11.9207 | 11.9207 |
| Dec 01-31 | 2.4696 | 2.4696 | 0.7409 | 4.5244 | 8.3401 | 8.3437 |
| Summeditotal | 84.7648 | 84.7648 | 25,4294 | 125.201 | 168,4041 | 168.5421 |

Table E 22 IES Monthly Results for Cooling Loads, Energy and Carbon for GF + Mezz Floor for 1 Pearl Combined Scenario

| Pearl 1 Room cooling plant sens. | | Total CE (kgCO2) | | |
|----------------------------------|---------|------------------|-------|--|
| load (| MWh) | | | |
| Date | | Date | | |
| Jan 01-31 | 4.4063 | Jan 01-31 | 3627 | |
| Feb 01-28 | 6.0783 | Feb 01-28 | 3980 | |
| Mar 01-31 | 9.8843 | Mar 01-31 | 5572 | |
| Apr 01-30 | 15.0318 | Apr 01-30 | 6719 | |
| May 01-31 | 19.5664 | May 01-31 | 7932 | |
| Jun 01-30 | 23.0208 | Jun 01-30 | 9582 | |
| Jul 01-31 | 24.4762 | Jul 01-31 | 10419 | |
| Aug 01-31 | 25.6658 | Aug 01-31 | 10664 | |
| Sep 01-30 | 22.657 | Sep 01-30 | 9928 | |
| Oct 01-31 | 17.3721 | Oct 01-31 | 7623 | |
| Nov 01-30 | 12.8696 | Nov 01-30 | 6309 | |
| Dec 01-31 | 7.1506 | Dec 01-31 | 4632 | |
| Summed total | 188.179 | Summed total | 86986 | |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 1.7935 | 1.7935 | 0.538 | 3.5305 | 7.015 | 7.0177 |
| Feb 01-28 | 2.4642 | 2.4642 | 0.7393 | 4.4322 | 7.664 | 7.7534 |
| Mar 01-31 | 4.3448 | 4.3448 | 1.3035 | 6.9586 | 10.7779 | 10.7779 |
| Apr 01-30 | 6.2207 | 6.2207 | 1.8662 | 9.3477 | 12.9935 | 13.001 |
| May 01-31 | 8.1928 | 8.1928 | 2.4578 | 11.8661 | 15.3342 | 15.3533 |
| Jun 01-30 | 10.4803 | 10.4803 | 3.1441 | 14.8859 | 18.531 | 18.5392 |
| Jul 01-31 | 11.7278 | 11.7278 | 3.5183 | 16.4994 | 20.1527 | 20.1527 |
| Aug 01-31 | 12.0921 | 12.0921 | 3.6276 | 16.9731 | 20.6264 | 20.6264 |
| Sep 01-30 | 10.9944 | 10.9944 | 3.2983 | 15.5558 | 19.1993 | 19.209 |
| Oct 01-31 | 7.739 | 7.739 | 2.3217 | 11.257 | 14.7442 | 14.7442 |
| Nov 01-30 | 5.6124 | 5.6124 | 1.6837 | 8.5494 | 12.2027 | 12.2027 |
| Dec 01-31 | 2.9442 | 2.9442 | 0.8833 | 5.1418 | 8.957 | 8.9611 |
| Summed total | 84.6061 | 84.6061 | 25.3818 | 124.9974 | 168.1977 | 168.3385 |

Table E 23 IES Monthly Results for Cooling Loads, Energy and Carbon for GF + Mezz Floor for 2 Pearl Combined Scenario

| Pearl 2 Combine | d Room cooling | Total CE (kgCO2) | |
|-----------------|----------------|------------------|-------|
| plant sens. le | oad (MWh) | | |
| Date | | Date | |
| Jan 01-31 | 3.7678 | Jan 01-31 | 3454 |
| Feb 01-28 | 5.2969 | Feb 01-28 | 3768 |
| Mar 01-31 | 8.8893 | Mar 01-31 | 5301 |
| Apr 01-30 | 13.9327 | Apr 01-30 | 6420 |
| May 01-31 | 18.3389 | May 01-31 | 7598 |
| Jun 01-30 | 21.6775 | Jun 01-30 | 9217 |
| Jul 01-31 | 23.0938 | Jul 01-31 | 10043 |
| Aug 01-31 | 24.2402 | Aug 01-31 | 10276 |
| Sep 01-30 | 21.3267 | Sep 01-30 | 9566 |
| Oct 01-31 | 16.2209 | Oct 01-31 | 7310 |
| Nov 01-30 | 11.82 | Nov 01-30 | 6023 |
| Dec 01-31 | 6.3421 | Dec 01-31 | 4412 |
| Summed total | 174.9468 | Summed total | 83386 |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 1.5358 | 1.5358 | 0.4607 | 3.1954 | 6.6801 | 6.6826 |
| Feb 01-28 | 2.1482 | 2.1482 | 0.6445 | 4.0212 | 7.2532 | 7.3424 |
| Mar 01-31 | 3.9421 | 3.9421 | 1.1826 | 6.435 | 10.2543 | 10.2543 |
| Apr 01-30 | 5.7757 | 5.7757 | 1.7327 | 8.7692 | 12.415 | 12.4225 |
| May 01-31 | 7.6959 | 7.6959 | 2.3088 | 11.2201 | 14.6882 | 14.7073 |
| Jun 01-30 | 9.9366 | 9.9366 | 2.981 | 14.179 | 17.8241 | 17.8323 |
| Jul 01-31 | 11.168 | 11.168 | 3.3504 | 15.7717 | 19.4249 | 19.4249 |
| Aug 01-31 | 11.5145 | 11.5145 | 3.4544 | 16.2222 | 19.8754 | 19.8754 |
| Sep 01-30 | 10.4556 | 10.4556 | 3.1367 | 14.8554 | 18.4989 | 18.5086 |
| Oct 01-31 | 7.273 | 7.273 | 2.1819 | 10.6512 | 14.1384 | 14.1384 |
| Nov 01-30 | 5.1874 | 5.1874 | 1.5562 | 7.997 | 11.6503 | 11.6503 |
| Dec 01-31 | 2.6169 | 2.6169 | 0.7851 | 4.7162 | 8.5315 | 8.5356 |
| Summed total | 79.2497 | 79.2497 | 23.7749 | 118.0336 | 161.2344 | 161.3748 |

| | | Total CE (kgCC | 2) |
|--------------------|--------------------|----------------|--------|
| / Room cooling pla | ant sens. load (MW | | |
| Date | | Date | |
| Jan 01-31 | 18.6773 | Jan 01-31 | 28215 |
| Feb 01-28 | 35.4269 | Feb 01-28 | 31659 |
| Mar 01-31 | 85.0081 | Mar 01-31 | 50470 |
| Apr 01-30 | 164.9722 | Apr 01-30 | 69876 |
| May 01-31 | 236.5126 | May 01-31 | 89318 |
| Jun 01-30 | 288.8427 | Jun 01-30 | 111024 |
| Jul 01-31 | 311.8924 | Jul 01-31 | 121494 |
| Aug 01-31 | 327.2845 | Aug 01-31 | 124808 |
| Sep 01-30 | 282.6447 | Sep 01-30 | 113793 |
| Oct 01-31 | 202.26 | Oct 01-31 | 83007 |
| Nov 01-30 | 129.3723 | Nov 01-30 | 62132 |
| Dec 01-31 | 46.7236 | Dec 01-31 | 38211 |
| Summed total | 2129.6187 | Summed total | 923993 |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|-------------------------------|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 7.9166 | 7.9166 | 2.375 | 23.7517 | 54.5586 | 54.5764 |
| Feb 01-28 | 14.4968 | 14.4968 | 4.3486 | 32.5083 | 60.899 | 61.7599 |
| Mar 01-31 | 38.052 | 38.052 | 11.4156 | 64.1893 | 97.6352 | 97.6352 |
| Apr 01-30 | 68.2267 | 68.2267 | 20.4676 | 102.855 | 135.1373 | 135.2138 |
| May 01-31 | 98.6114 | 98.6114 | 29.584 | 141.8324 | 172.677 | 172.8716 |
| Jun 01-30 | 129.0745 | 129.0745 | 38.7225 | 181.9629 | 214.7005 | 214.7836 |
| Jul 01-31 | 145.2765 | 145.2765 | 43.5832 | 202.9424 | 234.9997 | 234.9997 |
| Aug 01-31 | 150.2857 | 150.2857 | 45.0851 | 209.4535 | 241.3952 | 241.3952 |
| Sep 01-30 | 133.4721 | 133.4721 | 40.042 | 187.6952 | 220.0728 | 220.1725 |
| Oct 01-31 | 89.2878 | 89.2878 | 26.7867 | 129.5156 | 160.5472 | 160.5472 |
| Nov 01-30 | 56.6394 | 56.6394 | 16.992 | 87.7143 | 120.1734 | 120.1734 |
| Dec 01-31 | 19.4503 | 19.4503 | 5.8353 | 40.0399 | 73.8957 | 73.9282 |
| Summed total | 950.7911 | 950.7911 | 285.2376 | 1404.4605 | 1786.6916 | 1788.0556 |

Table E 25 IES Monthly Results for Cooling Loads, Energy and Carbon for All Building for 1 Pearl Wall Scenario

| Pearl 1 - WallR | oom cooling plant | | Total CE | (kgCO2) | | |
|-----------------|-------------------|-----------------|-----------------|-----------------|-------------------|--------------|
| sens. lo | ad (MWh) | | | | | |
| Date | | | Date | | | |
| Jan 01-31 | 21.7175 | | Jan 01-31 | 29000 | | |
| Feb 01-28 | 38.2285 | | Feb 01-28 | 32409 | | |
| Mar 01-31 | 84.4698 | | Mar 01-31 | 50334 | | |
| Apr 01-30 | 157.7489 | | Apr 01-30 | 67913 | | |
| May 01-31 | 222.5069 | | May 01-31 | 85497 | | |
| Jun 01-30 | 269.8389 | | Jun 01-30 | 105845 | | |
| Jul 01-31 | 290.4042 | | Jul 01-31 | 115646 | | |
| Aug 01-31 | 304.9506 | | Aug 01-31 | 118723 | | |
| Sep 01-30 | 264.2543 | | Sep 01-30 | 108802 | | |
| Oct 01-31 | 191.3227 | | Oct 01-31 | 80029 | | |
| Nov 01-30 | 125.455 | | Nov 01-30 | 61066 | | |
| Dec 01-31 | 49.5611 | | Dec 01-31 | 38984 | | |
| Summed total | 2020.4583 | | Summed total | 894233 | | |
| | | | | | | |
| | | | An Suchast rai | | | |
| | Chillers operat | An Sus shillors | Ap sys near rej | Total system | Total electricity | Total aparau |
| | (MM/b) | apergy (MM/b) | anarov (MW/b) | epergy (MM/b) | (MM/b) | (MM/b) |
| | (101001) | chergy (wwwh) | chergy (wwwh) | chergy (within) | (1010011) | (1010011) |
| Date | | | | | | |
| Jan 01-31 | 9.1775 | 9.1775 | 2,7541 | 25.3951 | 56,1986 | 56 |
| Feb 01-28 | 15.6945 | 15.6945 | 4.7085 | 34.0799 | 62.4565 | 63 |
| Mar 01-31 | 37.8177 | 37.8177 | 11.3452 | 63.8861 | 97.3319 | 97 |
| Apr 01-30 | 65.0988 | 65.0988 | 19.529 | 98.7871 | 131.0693 | 131 |
| May 01-31 | 92.5508 | 92.5508 | 27.7646 | 133.9523 | 164.7983 | 164 |
| Jun 01-30 | 120.85 | 120.85 | 36.2551 | 171.2696 | 204.0072 | 204 |
| Jul 01-31 | 135.977 | 135.977 | 40.7936 | 190.8519 | 222.9107 | 222 |
| Aug 01-31 | 140.6159 | 140.6159 | 42.1841 | 196.8828 | 228.8231 | 228 |
| Sep 01-30 | 125.5067 | 125.5067 | 37.6527 | 177.3404 | 209.7194 | 209 |
| Oct 01-31 | 84.5453 | 84.5453 | 25.364 | 123.3502 | 154.3819 | 154 |

Nov 01-30

Dec 01-31

Summed total

54.9364

20.6783

903.4474

54.9364

20.6783

903.4474

16.4804

6.2042

271.034

85.4995

41.6403

1342.9365

117.9588

1725.1456

75.4926

56.2198 63.3315 97.3319 131.1473 164.9915 204.0904 222.9107 228.8231 209.8177 154.3818

117.9588

75.5286

1726.5317

Table E 26 IES Monthly Results for Cooling Loads, Energy and Carbon for All Building for 2 Pearl Wall Scenario

| Pearl 2- Wall Room cooling plant | | Total CE (kgCO2) | |
|----------------------------------|-----------|------------------|--------|
| sens. lo | ad (MWh) | | |
| Date | | Date | |
| Jan 01-31 | 22.0012 | Jan 01-31 | 29078 |
| Feb 01-28 | 38.4961 | Feb 01-28 | 32472 |
| Mar 01-31 | 84.4273 | Mar 01-31 | 50314 |
| Apr 01-30 | 157.0569 | Apr 01-30 | 67725 |
| May 01-31 | 221.2068 | May 01-31 | 85150 |
| Jun 01-30 | 268.0628 | Jun 01-30 | 105369 |
| Jul 01-31 | 288.3976 | Jul 01-31 | 115107 |
| Aug 01-31 | 302.8531 | Aug 01-31 | 118149 |
| Sep 01-30 | 262.5107 | Sep 01-30 | 108319 |
| Oct 01-31 | 190.2629 | Oct 01-31 | 79735 |
| Nov 01-30 | 125.0476 | Nov 01-30 | 60954 |
| Dec 01-31 | 49.808 | Dec 01-31 | 39043 |
| Summed total | 2010.1325 | Summed total | 891428 |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 9.1995 | 9.1995 | 2.7602 | 25.4232 | 56.2268 | 56.248 |
| Feb 01-28 | 15.7149 | 15.7149 | 4.7146 | 34.1064 | 62.4831 | 63.3581 |
| Mar 01-31 | 37.8105 | 37.8105 | 11.3427 | 63.8764 | 97.3222 | 97.3222 |
| Apr 01-30 | 65.023 | 65.023 | 19.5074 | 98.6898 | 130.9706 | 131.0486 |
| May 01-31 | 92.4158 | 92.4158 | 27.7246 | 133.7774 | 164.622 | 164.8166 |
| Jun 01-30 | 120.663 | 120.663 | 36.1985 | 171.0273 | 203.7649 | 203.8481 |
| Jul 01-31 | 135.7666 | 135.7666 | 40.7301 | 190.5795 | 222.6368 | 222.6368 |
| Aug 01-31 | 140.3964 | 140.3964 | 42.1187 | 196.5964 | 228.5381 | 228.5381 |
| Sep 01-30 | 125.3227 | 125.3227 | 37.5962 | 177.1014 | 209.479 | 209.5786 |
| Oct 01-31 | 84.4306 | 84.4306 | 25.3291 | 123.202 | 154.2324 | 154.2324 |
| Nov 01-30 | 54.8895 | 54.8895 | 16.4672 | 85.438 | 117.8973 | 117.8973 |
| Dec 01-31 | 20.6979 | 20.6979 | 6.2087 | 41.6658 | 75.5168 | 75.5528 |
| Summed total | 902.3291 | 902.3291 | 270.6994 | 1341.4825 | 1723.6914 | 1725.0775 |

Table E27 IES Monthly Results for Cooling Loads, Energy and Carbon for All Building for 1 Pearl Glazing Scenario

| Pearl 1 - Glazing Room cooling plant | | Total CE (kgCO2) | | |
|--------------------------------------|-----------|------------------|--------|--|
| sens. loa | d (MWh) | | | |
| Date | | Date | | |
| Jan 01-31 | 13.2256 | Jan 01-31 | 26758 | |
| Feb 01-28 | 26.2062 | Feb 01-28 | 29161 | |
| Mar 01-31 | 69.6631 | Mar 01-31 | 46313 | |
| Apr 01-30 | 143.9286 | Apr 01-30 | 64157 | |
| May 01-31 | 209.0572 | May 01-31 | 81845 | |
| Jun 01-30 | 257.7021 | Jun 01-30 | 102539 | |
| Jul 01-31 | 279.2437 | Jul 01-31 | 112614 | |
| Aug 01-31 | 294.1357 | Aug 01-31 | 115786 | |
| Sep 01-30 | 253.3596 | Sep 01-30 | 105825 | |
| Oct 01-31 | 179.8241 | Oct 01-31 | 76896 | |
| Nov 01-30 | 112.3945 | Nov 01-30 | 57505 | |
| Dec 01-31 | 37.4777 | Dec 01-31 | 35698 | |
| Summed total | 1876.2195 | Summed total | 855097 | |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 5.7537 | 5.7537 | 1.7259 | 20.9365 | 51.7466 | 51.7598 |
| Feb 01-28 | 10.7944 | 10.7944 | 3.2378 | 27.6753 | 56.0872 | 56.9271 |
| Mar 01-31 | 31.8504 | 31.8504 | 9.5542 | 56.1265 | 89.5737 | 89.5737 |
| Apr 01-30 | 59.7076 | 59.7076 | 17.9128 | 91.7797 | 124.0606 | 124.1386 |
| May 01-31 | 87.4966 | 87.4966 | 26.2494 | 127.3829 | 158.2274 | 158.4221 |
| Jun 01-30 | 116.4688 | 116.4688 | 34.9408 | 165.5741 | 198.3117 | 198.3949 |
| Jul 01-31 | 132.0604 | 132.0604 | 39.6177 | 185.7609 | 217.8182 | 217.8182 |
| Aug 01-31 | 136.8671 | 136.8671 | 41.0605 | 192.0104 | 223.9506 | 223.9506 |
| Sep 01-30 | 121.6177 | 121.6177 | 36.4849 | 172.2852 | 204.6627 | 204.7625 |
| Oct 01-31 | 80.204 | 80.204 | 24.0619 | 117.7083 | 148.7385 | 148.7385 |
| Nov 01-30 | 49.766 | 49.766 | 14.9301 | 78.7788 | 111.238 | 111.238 |
| Dec 01-31 | 15.7133 | 15.7133 | 4.7142 | 35.1788 | 69.0376 | 69.0671 |
| Summed total | 848.3 | 848.3 | 254.4901 | 1271.1959 | 1653.4544 | 1654.7911 |

Table E 28 IES Monthly Results for Cooling Loads, Energy and Carbon for All Building for 2 Pearl Wall Scenario

| Pearl 2 Glazing Room cooling plant | | Total CE (kgCO2) | |
|------------------------------------|-----------|------------------|--------|
| sens. loa | d (MWh) | | |
| Date | | Date | |
| Jan 01-31 | 10.862 | Jan 01-31 | 26137 |
| Feb 01-28 | 22.8135 | Feb 01-28 | 28247 |
| Mar 01-31 | 64.987 | Mar 01-31 | 45046 |
| Apr 01-30 | 138.7953 | Apr 01-30 | 62764 |
| May 01-31 | 203.4536 | May 01-31 | 80321 |
| Jun 01-30 | 251.7094 | Jun 01-30 | 100913 |
| Jul 01-31 | 273.124 | Jul 01-31 | 110951 |
| Aug 01-31 | 287.8883 | Aug 01-31 | 114083 |
| Sep 01-30 | 247.4714 | Sep 01-30 | 104233 |
| Oct 01-31 | 174.6645 | Oct 01-31 | 75494 |
| Nov 01-30 | 107.5826 | Nov 01-30 | 56198 |
| Dec 01-31 | 33.8676 | Dec 01-31 | 34718 |
| Summed total | 1817.2179 | Summed total | 839077 |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 4.827 | 4.827 | 1.4488 | 19.7313 | 50.5429 | 50.556 |
| Feb 01-28 | 9.4379 | 9.4379 | 2.831 | 25.9041 | 54.3239 | 55.1572 |
| Mar 01-31 | 29.9612 | 29.9612 | 8.9885 | 53.6714 | 87.1173 | 87.1173 |
| Apr 01-30 | 57.6288 | 57.6288 | 17.289 | 89.0771 | 121.3594 | 121.4374 |
| May 01-31 | 85.2288 | 85.2288 | 25.5683 | 124.4342 | 155.2788 | 155.4734 |
| Jun 01-30 | 114.0433 | 114.0433 | 34.2124 | 162.4203 | 195.1579 | 195.2411 |
| Jul 01-31 | 129.5834 | 129.5834 | 38.875 | 182.5411 | 214.5985 | 214.5985 |
| Aug 01-31 | 134.3385 | 134.3385 | 40.3016 | 188.7215 | 220.6632 | 220.6632 |
| Sep 01-30 | 119.2353 | 119.2353 | 35.7697 | 169.1861 | 201.5651 | 201.6634 |
| Oct 01-31 | 78.115 | 78.115 | 23.435 | 114.9923 | 146.0226 | 146.0226 |
| Nov 01-30 | 47.8189 | 47.8189 | 14.3451 | 76.2467 | 108.7046 | 108.7046 |
| Dec 01-31 | 14.2542 | 14.2542 | 4.2761 | 33.2816 | 67.1405 | 67.1684 |
| Summed total | 824.471 | 824.471 | 247.342 | 1240.2078 | 1622.4759 | 1623.8029 |

Table E 29 IES Monthly Results for Cooling Loads, Energy and Carbon for All Building for 1 Pearl Roof Scenario

| Pearl 1 Roof - Room cooling plant | | Total CE (kg | CO2) |
|-----------------------------------|-----------|--------------|--------|
| sens. la | ad (MWh) | | |
| Date | | Date | |
| Jan 01-31 | 18.7616 | Jan 01-31 | 28237 |
| Feb 01-28 | 35.4552 | Feb 01-28 | 31667 |
| Mar 01-31 | 84.8832 | Mar 01-31 | 50436 |
| Apr 01-30 | 164.6465 | Apr 01-30 | 69787 |
| May 01-31 | 235.9747 | May 01-31 | 89171 |
| Jun 01-30 | 288.1325 | Jun 01-30 | 110831 |
| Jul 01-31 | 311.0895 | Jul 01-31 | 121276 |
| Aug 01-31 | 326.4717 | Aug 01-31 | 124587 |
| Sep 01-30 | 281.9572 | Sep 01-30 | 113606 |
| Oct 01-31 | 201.8545 | Oct 01-31 | 82896 |
| Nov 01-30 | 129.214 | Nov 01-30 | 62089 |
| Dec 01-31 | 46.7936 | Dec 01-31 | 38230 |
| Summed total | 2125.2355 | Summed total | 922800 |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 7.9494 | 7.9494 | 2.3848 | 23.7944 | 54.6012 | 54.6191 |
| Feb 01-28 | 14.508 | 14.508 | 4.352 | 32.5229 | 60.9136 | 61.7745 |
| Mar 01-31 | 38.0014 | 38.0014 | 11.4004 | 64.1236 | 97.5695 | 97.5695 |
| Apr 01-30 | 68.0949 | 68.0949 | 20.4281 | 102.6836 | 134.9659 | 135.0424 |
| May 01-31 | 98.3937 | 98.3937 | 29.5187 | 141.5493 | 172.3939 | 172.5885 |
| Jun 01-30 | 128.787 | 128.787 | 38.6362 | 181.5892 | 214.3268 | 214.4099 |
| Jul 01-31 | 144.9516 | 144.9516 | 43.4857 | 202.52 | 234.5773 | 234.5773 |
| Aug 01-31 | 149.9567 | 149.9567 | 44.9865 | 209.0258 | 240.9675 | 240.9675 |
| Sep 01-30 | 133.1939 | 133.1939 | 39.9585 | 187.3335 | 219.7111 | 219.8108 |
| Oct 01-31 | 89.1237 | 89.1237 | 26.7375 | 129.3022 | 160.3338 | 160.3338 |
| Nov 01-30 | 56.5753 | 56.5753 | 16.9727 | 87.631 | 120.0901 | 120.0901 |
| Dec 01-31 | 19.4787 | 19.4787 | 5.8438 | 40.0769 | 73.9326 | 73.9651 |
| Summed total | 949.0155 | 949.0155 | 284.7049 | 1402.1523 | 1784.3833 | 1785.7474 |

Table E 30 IES Monthly Results for Cooling Loads, Energy and Carbon for All Building for 2 Pearl Roof Scenario

| Pearl 2 Roof Room cooling plant | | Total CE (kgC | Total CE (kgCO2) | | |
|---------------------------------|-----------|---------------|------------------|--|--|
| sens. lo | ad (MWh) | | | | |
| Date | | Date | | | |
| Jan 01-31 | 18.7667 | Jan 01-31 | 28239 | | |
| Feb 01-28 | 35.4571 | Feb 01-28 | 31667 | | |
| Mar 01-31 | 84.8764 | Mar 01-31 | 50435 | | |
| Apr 01-30 | 164.628 | Apr 01-30 | 69782 | | |
| May 01-31 | 235.9441 | May 01-31 | 89163 | | |
| Jun 01-30 | 288.0919 | Jun 01-30 | 110820 | | |
| Jul 01-31 | 311.0436 | Jul 01-31 | 121263 | | |
| Aug 01-31 | 326.4251 | Aug 01-31 | 124575 | | |
| Sep 01-30 | 281.9178 | Sep 01-30 | 113595 | | |
| Oct 01-31 | 201.8313 | Oct 01-31 | 82890 | | |
| Nov 01-30 | 129.2051 | Nov 01-30 | 62086 | | |
| Dec 01-31 | 46.7978 | Dec 01-31 | 38232 | | |
| Summed total | 2124.9864 | Summed total | 922732 | | |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 7.9514 | 7.9514 | 2.3854 | 23.797 | 54.6038 | 54.6217 |
| Feb 01-28 | 14.5088 | 14.5088 | 4.3522 | 32.5239 | 60.9146 | 61.7755 |
| Mar 01-31 | 37.9986 | 37.9986 | 11.3996 | 64.12 | 97.5659 | 97.5659 |
| Apr 01-30 | 68.0874 | 68.0874 | 20.4258 | 102.6739 | 134.9562 | 135.0327 |
| May 01-31 | 98.3813 | 98.3813 | 29.515 | 141.5332 | 172.3778 | 172.5724 |
| Jun 01-30 | 128.7706 | 128.7706 | 38.6313 | 181.5678 | 214.3054 | 214.3885 |
| Jul 01-31 | 144.933 | 144.933 | 43.4801 | 202.4959 | 234.5532 | 234.5532 |
| Aug 01-31 | 149.9378 | 149.9378 | 44.9808 | 209.0013 | 240.943 | 240.943 |
| Sep 01-30 | 133.1779 | 133.1779 | 39.9538 | 187.3128 | 219.6903 | 219.7901 |
| Oct 01-31 | 89.1143 | 89.1143 | 26.7347 | 129.29 | 160.3216 | 160.3216 |
| Nov 01-30 | 56.5717 | 56.5717 | 16.9717 | 87.6262 | 120.0854 | 120.0854 |
| Dec 01-31 | 19.4804 | 19.4804 | 5.8443 | 40.0791 | 73.9348 | 73.9674 |
| Summed total | 948.9146 | 948.9146 | 284.6747 | 1402.0211 | 1784.252 | 1785.6161 |

Table E 31 IES Monthly Results for Cooling Loads, Energy and Carbon for All Building for 1 Pearl Combined Scenario

| Pearl 1 Combined Room cooling | | Total CE (kgCO2) | |
|-------------------------------|-----------|------------------|--------|
| plant sens. I | oad (MWh) | | |
| Date | | Date | |
| Jan 01-31 | 15.7965 | Jan 01-31 | 27407 |
| Feb 01-28 | 28.1988 | Feb 01-28 | 29696 |
| Mar 01-31 | 67.3625 | Mar 01-31 | 45677 |
| Apr 01-30 | 133.625 | Apr 01-30 | 61356 |
| May 01-31 | 190.6064 | May 01-31 | 76824 |
| Jun 01-30 | 233.2537 | Jun 01-30 | 95892 |
| Jul 01-31 | 251.8693 | Jul 01-31 | 105171 |
| Aug 01-31 | 265.6645 | Aug 01-31 | 108039 |
| Sep 01-30 | 229.6702 | Sep 01-30 | 99385 |
| Oct 01-31 | 165.2233 | Oct 01-31 | 72932 |
| Nov 01-30 | 106.226 | Nov 01-30 | 55833 |
| Dec 01-31 | 39.5526 | Dec 01-31 | 36265 |
| Summed total | 1727.0486 | Summed total | 814448 |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 6.7276 | 6.7276 | 2.0185 | 22.2051 | 53.0117 | 53.0284 |
| Feb 01-28 | 11.5754 | 11.5754 | 3.4731 | 28.7048 | 57.102 | 57.9579 |
| Mar 01-31 | 30.9148 | 30.9148 | 9.2749 | 54.913 | 88.3588 | 88.3588 |
| Apr 01-30 | 55.536 | 55.536 | 16.6612 | 86.3565 | 118.6388 | 118.7154 |
| May 01-31 | 80.0278 | 80.0278 | 24.0086 | 117.6719 | 148.5165 | 148.7111 |
| Jun 01-30 | 106.5713 | 106.5713 | 31.9708 | 152.7081 | 185.4471 | 185.5289 |
| Jul 01-31 | 120.9807 | 120.9807 | 36.2935 | 171.357 | 203.4143 | 203.4143 |
| Aug 01-31 | 125.3412 | 125.3412 | 37.6019 | 177.0259 | 208.9663 | 208.9663 |
| Sep 01-30 | 112.0292 | 112.0292 | 33.6086 | 159.8189 | 192.1978 | 192.2961 |
| Oct 01-31 | 74.2938 | 74.2938 | 22.2886 | 110.0232 | 141.0549 | 141.0549 |
| Nov 01-30 | 47.2683 | 47.2683 | 14.1801 | 75.5326 | 107.9905 | 107.9905 |
| Dec 01-31 | 16.5523 | 16.5523 | 4.965 | 36.2737 | 70.1274 | 70.162 |
| Summed total | 787.8169 | 787.8169 | 236.3448 | 1192.5892 | 1574.8245 | 1576.1857 |

Table E 32 IES Monthly Results for Cooling Loads, Energy and Carbon for All Building for 2 Pearl Combined Scenario

| Pearl 2 CombinedRoom cooling | | Total CE (kgCO2) | |
|------------------------------|------------|------------------|--------|
| plant sens. | load (MWh) | | |
| Date | | Date | |
| Jan 01-31 | 13.1139 | Jan 01-31 | 26700 |
| Feb 01-28 | 24.5185 | Feb 01-28 | 28695 |
| Mar 01-31 | 62.2161 | Mar 01-31 | 44283 |
| Apr 01-30 | 127.7673 | Apr 01-30 | 59763 |
| May 01-31 | 184.0204 | May 01-31 | 75025 |
| Jun 01-30 | 226.0726 | Jun 01-30 | 93936 |
| Jul 01-31 | 244.4798 | Jul 01-31 | 103156 |
| Aug 01-31 | 258.0857 | Aug 01-31 | 105980 |
| Sep 01-30 | 222.6168 | Sep 01-30 | 97462 |
| Oct 01-31 | 159.2109 | Oct 01-31 | 71292 |
| Nov 01-30 | 100.8284 | Nov 01-30 | 54363 |
| Dec 01-31 | 35.6363 | Dec 01-31 | 35198 |
| Summed total | 1658.5681 | Summed total | 795850 |

| | Chillers energy (MWh) | Ap Sys chillers energy (MWh) | Ap Sys heat rej fans/pumps energy (MWh) | Total system energy (MWh) | Total electricity (MWh) | Total energy (MWh) |
|--------------|--------------------------|---------------------------------|---|------------------------------|----------------------------|-----------------------|
| Date | | | | | | |
| Jan 01-31 | 5.6695 | 5.6695 | 1.7004 | 20.8287 | 51.637 | 51.6534 |
| Feb 01-28 | 10.1023 | 10.1023 | 3.0302 | 26.7827 | 55.1874 | 56.0344 |
| Mar 01-31 | 28.8375 | 28.8375 | 8.6515 | 52.2109 | 85.6567 | 85.6567 |
| Apr 01-30 | 53.1644 | 53.1644 | 15.9495 | 83.2746 | 115.5555 | 115.6335 |
| May 01-31 | 77.3615 | 77.3615 | 23.2092 | 114.2061 | 145.0507 | 145.2453 |
| Jun 01-30 | 103.6649 | 103.6649 | 31.0992 | 148.93 | 181.6676 | 181.7508 |
| Jul 01-31 | 117.9887 | 117.9887 | 35.3965 | 167.468 | 199.5252 | 199.5252 |
| Aug 01-31 | 122.2716 | 122.2716 | 36.6822 | 173.0366 | 204.9768 | 204.9768 |
| Sep 01-30 | 109.1729 | 109.1729 | 32.752 | 156.1061 | 188.485 | 188.5833 |
| Oct 01-31 | 71.8601 | 71.8601 | 21.5585 | 106.8595 | 137.8911 | 137.8911 |
| Nov 01-30 | 45.0838 | 45.0838 | 13.5257 | 72.6909 | 105.1502 | 105.1502 |
| Dec 01-31 | 14.9685 | 14.9685 | 4.4913 | 34.2146 | 68.0698 | 68.103 |
| Summed total | 760.1472 | 760.1472 | 228.0446 | 1156.6101 | 1538.8546 | 1540.2053 |